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LIGHTLY ARMORED STRUCTURE VULNERABILITY ESTIMATION METHODOLOGY --ETC(U)
JAN 79 C J LAPOINTE
AMSAA-TR-254

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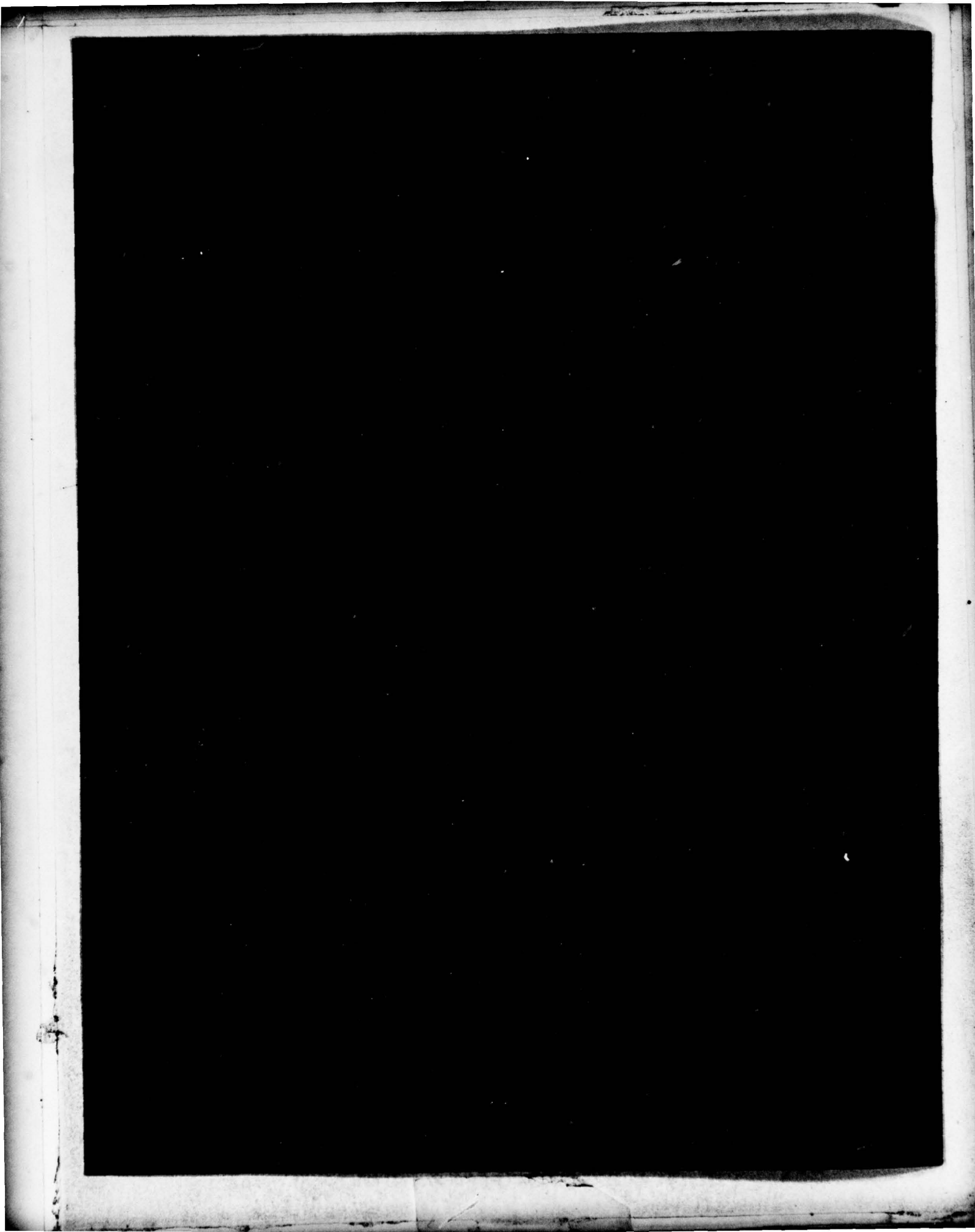
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rationale, together with a program listing, details of the input data decks, and examples of input and output.

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LIGHTLY ARMORED STRUCTURE VULNERABILITY ESTIMATION METHODOLOGY (LASVEM)

1. INTRODUCTION

The USAMSAA has developed a computer model which assists in the evaluation of lightly armored structures, such as armored personnel carriers, by computing various measures of vulnerability of those structures when subjected to indirect fire, high explosive (not ICM) field artillery projectiles. The basic concept is that the primary function of such a structure, with respect to field artillery fire, is to prevent the intrusion of fragments into an enclosure; therefore, a fundamental measure of such a structure's vulnerability to artillery fire is the number of perforations which it sustains when subjected to such fires. Such a quantity, however, may not be especially useful to decision makers at various levels. Hence, a family of statistical parameters, all based upon the expected number of perforations, has been developed to address the vulnerability of a group of structures to various volumes of tactically delivered field artillery fires.

The program was originally developed for use on the USA Ballistic Research Laboratory (USABRL) BRLESC I/II computers. The characteristics of those computers resulted in restrictions on the size of certain matrices used in the program and in the use of a magnetic tape oriented file system. As documented herein, the program has been modified to run on the new USABRL CYBER 173/76 computer. The file system is now random access, but the size of the above mentioned matrices has not been increased in the desire to minimize the changes made to an already debugged program. This is the source of certain remarks in this report concerning restraints due to machine size.

This document is intended to serve as a user's guide so that other organizations may achieve a capability in this area. It is also intended to serve as a programmer's guide for those changes to the program which may be necessary or desired.

2. OVERVIEW OF THE COMPUTATIONAL TECHNIQUE

2.1 The Program.

The program is divided into four main sections. Section I uses the methodology of Thor reports 47 and 70 (references 1 and 2) to produce a description of the damage sustained by a single plate or plate pair from the detonation of a projectile at a fixed point in space with a fixed angle of fall and terminal velocity, for all locations of the plate or plate pair. Section II combines the descriptions of damage sustained by several plates (output of Section I) to obtain a description of damage sustained by a complete structure. Section III uses the descriptions of damage sustained by a complete structure from the detonation of a projectile to obtain various statistical measures of the damage sustained by specified arrays of target structures when these arrays are subjected to tactically delivered field artillery fire.

Whereas the first three sections of the program deal with the number of perforations sustained, Section IV assesses, in a rather simplistic manner, the effect of a perforation upon people within the enclosure. Additionally, it determines, without reference to the detailed and time consuming computations of Section I, whether any of the fragments have the capability of ever penetrating (except by direct hit or very near miss of the projectile) the plate under consideration.

2.2 Damage Criteria.

The function of a lightly armored structure with respect to field artillery fire is to prevent the intrusion of fragments into an enclosure. (Protection against direct hits and very near misses seems impossible to achieve with current light armors.) Therefore, the damage criteria used herein are always of the form, "sustain at least N perforations", and the probability statements obtained are always of the form, "probability that M targets each sustain at least N perforations". For brevity, this is often expressed as, "probability that M vehicles are damaged", where the damage criterion has been specified as above.

A minor problem arises with damage criteria of this form if one wishes to differentiate between the damage (which may be major) caused by individual fragments and the truly catastrophic damage caused by direct hits or very near misses. Within this model, the problem has been eliminated by forcing a direct hit or very near miss to produce a very large expected number of perforations (currently 10^4). Thus, direct hits and very near misses are addressed within the established framework, and yet are distinguished merely by using a criterion "sustain at least N perforations", where N is large but still small with respect to 10^4 .

2.3 Measures of Vulnerability.

Sections I and II produce an expected perforations matrix for a single target subjected to the fragmentation of one projectile at a fixed point in space with a fixed angle of fall and terminal velocity. Each element of this matrix is the expected number of perforations sustained by the target when it is located at a point in the ground plane corresponding to the matrix coordinates, (i,j).

The probability of damage matrix is obtained from the expected perforations matrix. With a damage criterion of the form, "sustain at least N perforations", and the assumption that a Poisson distribution applies for each location of the target, each element of this matrix is the probability that the target sustains damage at that location. There is a one-to-one correspondence between elements of the expected perforations matrix and elements of the probability of damage matrix.

From the probability of damage matrix are obtained:

- a. The lethal area (reference 3).
- b. The average probability of damage within the area over which the probability of damage is non-zero.
- c. The area over which the probability of damage is non-zero.
- d. A damage function.

Section III uses the methodology of reference 4 to address the vulnerability of an array of targets to various volumes of artillery fire. Using damage functions (one for each HOB in the HOB distribution being considered) obtained from the probability of damage matrices, this section of the program computes the probability that each target of the array is damaged for each volume of fire, for each HOB. The probabilities can be averaged over a specified HOB distribution. Using the average probabilities (over the HOB distribution) that each target sustain damage, the probabilities that various numbers of targets sustain damage, for each specified volley size, are computed. Also, an optimum HOB can be determined, which is then treated as an HOB distribution of zero width to obtain the quantities discussed above.

Section IV identifies those fragments of the fragment distribution which are capable of perforating a specified plate assuming no air drag. For each such fragment, the mass and velocity of the most massive residual fragment are computed. For each most massive residual fragment, the probability of incapacitating a soldier, given that he is hit, is computed using the methodology of reference 5. The average probability of incapacitation over the distribution of perforating fragments is computed.

3. MAJOR ASSUMPTIONS

- a. The perforation of the specified armor plates by the specified fragments is described by the methodology of Thor reports 47 and 70 (references 1 and 2). This assumption is fairly easy to change should a better methodology become available.
- b. The lightly armored structure is described by a set of flat, rectangular armor plates. If a plate is horizontal, its edges must be parallel to the range and deflection axes. If a plate is non-horizontal, it can deviate from a congruent, but horizontal, plate by not more than a rotation downward about any one of the horizontal plate's edges.
- c. The probability of sustaining at least N perforations is a good measure of the degree to which indirect artillery fire with HE projectiles is able to defeat a lightly armored structure.

4. PROGRAM SECTION I - VULNERABILITY OF ARMOR PLATES

4.1 The Program.

The purpose of Section I is to determine, for one set of projectile fragmentation data and one set of projectile coordinates, the expected number of perforations sustained by one armor plate of given material and geometry for every location of interest of that plate in a horizontal plane. This information is placed in the expected perforations matrix file. During the computation, various outputs are generated, which are of interest in the themselves and which may, in fact, be the only reason for processing certain plates. Conceptually, the methodology of this section is straightforward.

4.1.1 Horizontal Plates. Rather than compute directly the expected number of perforations sustained by the target plate for every location of interest, we consider an infinite plate of the specified material and thickness. We establish a grid of square cells thereon, and fix the grid's location with respect to the projectile by defining its burst point (range, deflection) in terms of grid columns and rows. The geometry is shown in Figure 4-1, where:

Z is the burst point.

OZ is the vertical separation between burst point and plate.

$O'Z$ is the HOB.

ZQ is the tangent to the projectile trajectory at the burst point.

P is the point currently being considered for fragmentation damage.

ω is the angle of fall.

ψ is the supplement of the polar angle to the point P from the point Z .

\hat{n} is an outward drawn unit vector normal to the plate.

ζ is the obliquity angle and is equal to ψ .

ϕ is the azimuthal angle to the point P .

θ is the angle between the projectile axis (assumed to coincide with ZQ) and the line ZP .

The equation for the angle between any two vectors in a spherical polar coordinate system yields equation 4-1 which, in a Cartesian coordinate system, reduces to equation 4-2, which is used to determine the fragment spray within which point P lies.



$$\cos \theta = \cos \psi \sin \omega + \sin \psi \cos \omega \cos \phi \quad \text{Equation 4-1}$$

$$\cos \theta = (X^2 + Y^2 + Z^2)^{-1/2} (Z \sin \omega + X \cos \omega) \quad \text{Equation 4-2}$$

The fragment spray within which the point P lies is determined, and the entire cell within which it is embedded is considered to be covered by that spray. Hence, it is important for the grid cell at point P to subtend a solid angle at point \bar{z} which is small with respect to the fragment spray angle. On the other hand, since a computer has a limited storage capability, the grid must be limited in size. Therefore, the grid cell should be large enough to produce a quasi-infinite plane of sufficient size to encompass the entire area over which significant perforation effects may occur.

The static fragmentation data format currently used breaks the fragmentation down into various spray angles measured from the projectile nose and, for each spray, provides a fragment mass distribution and the maximum and median fragment velocities observed within that spray. References 6 and 7 provide examples of the data format and an explanation of the data collection and reduction techniques. The fragment sprays are vectored forward to account for the projectile velocity. Because the perforation capability of a fragment is not a linear function of its velocity, and also because consideration of each individual fragment velocity (to whatever extent such data are available) would have been prohibitive in terms of computer time, the following procedure was adopted as an approximation. The number of perforations sustained by the $(i,j)^{\text{th}}$ cell is computed assuming that all fragments have the appropriate maximum velocity and then recomputed assuming that all fragments have the appropriate median velocity. The expected number of perforations for cell (i,j) is approximated by the average of these two results. Should a comparison of these approximate values with experimental data indicate significant differences, other combinations of the two computed values could be used to obtain a better approximation.

Once the fragmentation data have been vectored and the spray(s) within which the point P lies have been identified (vectoring the sprays can cause them to overlap), the number of perforations sustained by the cell at point P is computed by use of equation 4-3, where

M is fragment mass.

V is fragment speed.

Q is either mass or speed.

r is a subscript identifying residual mass or residual speed of the most massive fragment particle resulting from a perforation.

$M_r \leq 0$ or $V_r \leq 0$ means no perforation occurs.

s is a subscript identifying striking mass or striking speed of an impinging fragment.

K is the fragment shape factor (reference 7); $K = m_s A^{-3/2}$ where A is the average fragment impact area.

t is the plate thickness.

ζ is the obliquity angle at impact of the fragment with the plate.

$C_Q, \alpha_Q, \beta_Q, \gamma_Q, \lambda_Q$ are empirical constants.

$$Q_r = Q_s - 10^{C_Q} t^{\alpha_Q} K^{-(2/3)\alpha_Q} M_s^{(2/3)\alpha_Q + \beta_Q} (\sec \zeta)^{\gamma_Q} V_s^{\lambda_Q} \quad \text{Equation 4-3}$$

This equation, from Thor Report 47 (reference 1), yields the residual mass and speed of a fragment after perforation. In the situation at hand, that of a horizontal plate, $\cos \zeta$ is just $\cos \psi$ which is merely the ratio of length ZO to length ZP.

Thor Report 70 (reference 2) provides equations which can be used to extend Equation 4-3 to some aluminum alloys not considered in Thor Report 47 (reference 1). These equations, after some algebraic manipulation yield

$$\frac{Q_r(AL)}{Q_s} = 1 - \frac{k_Q(AL)}{k_Q(AL\ 2024)} + \frac{k_Q(AL)}{k_Q(AL\ 2024)} \frac{Q_r(AL\ 2024)}{Q_s} \quad \text{Equation 4-4}$$

where the notation is the same as in equation 4-3 with the addition of:

k_Q is an empirical constant.

AL references some particular aluminum alloy.

AL 2024 references 2024 aluminum.

Reference 6 provides equation 4-5 which is used to compute velocity decay due to air drag:

$$V_s = V_o \exp (-AA \cdot R \cdot M_s^{-(1/3)}) \quad \text{Equation 4-5}$$

where

V_s is the velocity with which the fragment strikes the plate

V_o is the velocity with which the fragment is projected from the fragment source point.

AA is the air drag constant provided in the fragmentation data.

R is the distance from the fragment source point to the center of the plate cell being struck.

M_s is the mass of the fragment as it is projected from the fragment source point and as it strikes the plate.

When fragments capable of perforating the plate at point P (M_r and V_r both greater than zero) are identified, their densities per unit solid angle are summed and then multiplied by the solid angle subtended by the cell at point P. The solid angle, Ω , is computed using equation 4-6, where A is the surface area of the cell, ζ is the obliquity angle, and Ω must be small.

$$\Omega = A \cdot (X^2 + Y^2 + Z^2)^{-1} \cdot \cos \zeta \quad \text{Equation 4-6}$$

The preceding is done for both the maximum and median velocities of the fragments striking point P and the average of the two results is the expected number of perforations sustained by the cell at point P. This procedure is performed for each cell in the grid.

When a direct hit or very near miss occurs, the preceding computations are bypassed and a very large number of perforations (currently 10^4) is inserted into the matrix elements corresponding to the quasi-infinite plate cells sustaining a direct hit or very near miss. The direct hit problem, then, boils down to identifying the cells sustaining a direct hit or very near miss. This is done in the following manner.

A sphere with radius equal to the blast parameter is generated about the burst point. The upper hemisphere is replaced by a right circular cylinder whose directrix is the circle formed by the hemisphere edge. The intersection of the resulting solid figure with the quasi-infinite plate is a circle. On the quasi-infinite plate is constructed the smallest square which completely encompasses all cells, any parts of which were enclosed by the circle. The cells encompassed by this square are the ones considered to sustain direct hits or very near misses.

The expected perforations matrix described above is not the desired matrix; it merely shows the expected perforations sustained by a horizontal, square target of unit size (one cell) for every position of the target. To obtain the expected perforations matrix for the actual target plate, we superimpose on the actual target plate a grid having the same cell size and cell orientation as the quasi-infinite grid. The center cell of this actual target plate is defined by equations 4-7:

$$MIDX = (NX \oplus 2) + 1$$

$$MIDY = (NY \oplus 2) + 1$$

Equations 4-7

where

NX is the number of cells of the actual target plate along the range axis.

NY is the number of cells of the actual target plate along the deflection axis.

⊙ is an operation defined as divide and then truncate the fractional part.

Defining the location of the actual target plate on the quasi-infinite plate as the location of its central cell on the quasi-infinite plate, we position the central cell of the actual target plate successively over each cell of the quasi-infinite plate and, for each such position, we sum the expected perforations of every cell covered by the actual target plate. The result is the expected perforations matrix for the actual target plate. This matrix is now multiplied by a scale factor, if desired, to account for any slight mismatch in surface areas that may exist between the actual target plate and the plate being modeled.

At this point, the expected perforations matrix is stored in the expected perforations matrix file and various types of information may be output, as will be discussed in paragraph 4.2.

4.1.2 Non-Horizontal Single Plates. The plates considered here are those obtained from a congruent, but horizontal, plate by a downward rotation from the horizontal about only one of the horizontal plate's four edges. Figure 4-2 shows two such plates rotated about the deflection axis. Figure 4-3 shows two such plates rotated about the range axis. The following sign conventions and constraints hold:

- (1) $0^\circ \leq |\alpha| < 180^\circ$
- (2) $0^\circ \leq |\beta| < 180^\circ$
- (3) α is positive (negative) when a vector drawn outward and normal to the plate has a component in the direction of increasing (decreasing) range.
- (4) β is positive (negative) when a vector drawn outward and normal to the plate has a component in the direction of increasing (decreasing) deflection.
- (5) One or the other of α and β must be zero.

In this program, as in field artillery usage, deflection left is increasing and deflection right is decreasing. The treatment of such plates is similar to the treatment of the horizontal plate, but there is an increase in complexity.

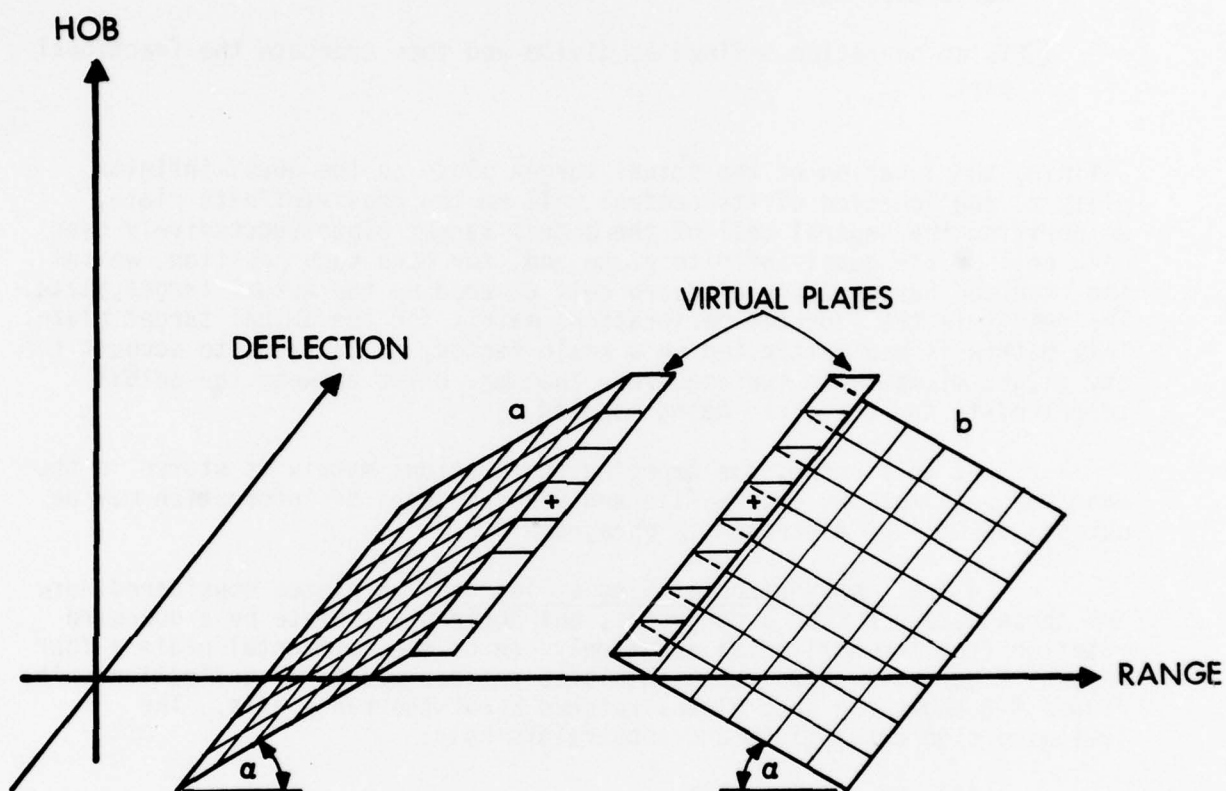


Figure 4-2. (U) Single Plates With a Rotation from the Horizontal About the Deflection Axis.

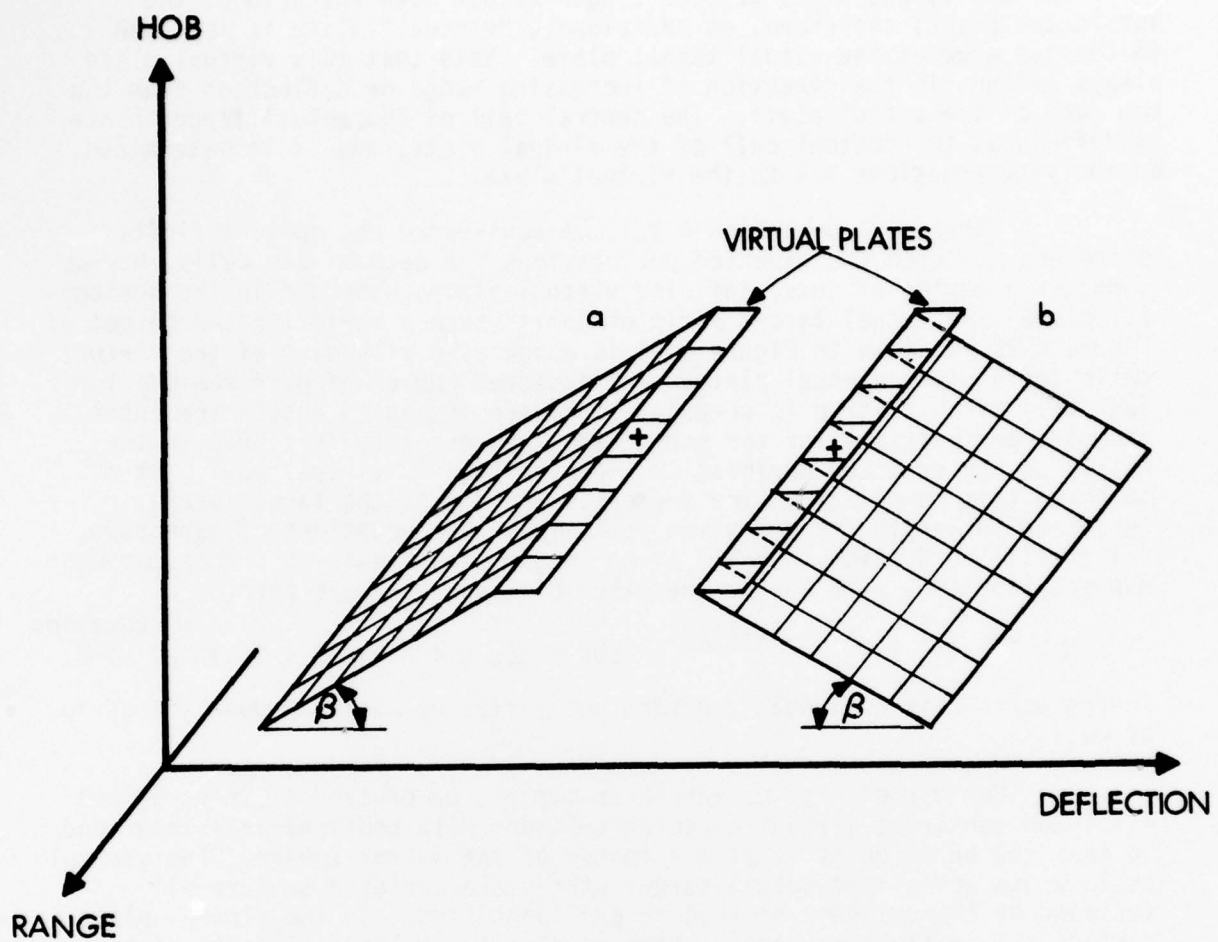


Figure 4.3 (U) Single Plates With a Rotation from the Horizontal About the Range Axis.

The target plate grid no longer meshes with the grid of the horizontal plane; therefore, an additional, "virtual" plate is appended to the top edge of the actual target plate. Note that this virtual plate always extends in the direction of increasing range or deflection from the top edge of the actual plate. The central cell of the actual target plate is defined as the central cell of the virtual plate, and it is determined by applying equations 4-7 to the virtual plate.

Whereas in paragraph 4.1.1, we considered one quasi-infinite plate and computed the expected perforations for each of its cells, now we consider a series of quasi-infinite virtual plates embedded in the horizontal plane. An actual target strip of cells (such a strip for the target of Figure 4-2a is shown in Figure 4-4) is associated with each of the virtual cells for a given virtual plate. The expected number of perforations for each cell of this strip is computed, they are summed to obtain the total expected perforations for the strip, and this quantity is stored in the matrix as the expected perforations for the $(i,j)^{th}$ virtual cell. It must be noted that computation time increases rapidly as the target strip increases in length for any given cell size. The equations of paragraph 4.1.1 still hold, except that ζ is no longer the same as ψ . Hence, we must use equation 4-8, with one or the other of α and β always zero.

$$\cos \zeta = (X^2 + Y^2 + Z^2)^{-1/2} (Z \cos \alpha \cos \beta + X \sin \alpha + Y \sin \beta) \quad \text{Equation 4-8}$$

Furthermore, Z is no longer constant but varies as we sweep down the strip of cells.

For direct hits or very near misses, we proceed as in paragraph 4.1.1 and construct a right circular cylinder with hemispherical lower end so that the burst point is at the center of the parent sphere. The virtual cells whose associated actual target strips are enclosed or partially enclosed by the cylinder-hemisphere are identified. On the virtual plate surface the smallest rectangle which completely encloses all such virtual cells is generated. The virtual cells enclosed by this rectangle are identified, and their associated actual target strips are the ones considered to sustain direct hits or very near misses.

As in paragraph 4.1.1, a sum over the virtual cells is performed to obtain the expected perforations matrix for the actual target plate. Of course, this sum is now 1-dimensional rather than 2-dimensional.

4.1.3 Non-Horizontal Plate Pairs. The concept of a non-horizontal plate pair arises from an examination of the two plates shown in Figure 4-2, or in Figure 4-3, and from the realization that if either of these plates is present in a lightly armored structure, it may well be accompanied by the other (e.g., the two sides of an APC). For this case, the two plates are considered as one plate pair and the symmetry of the situation is utilized to expedite the calculation. Except for the top spacer plate, nothing new is introduced. The utility of the concept is two-fold; it is faster on the computer than doing the two plates separately, and it expedites (for the machine) and facilitates (for the user) some of the subsequent computations of program section II.

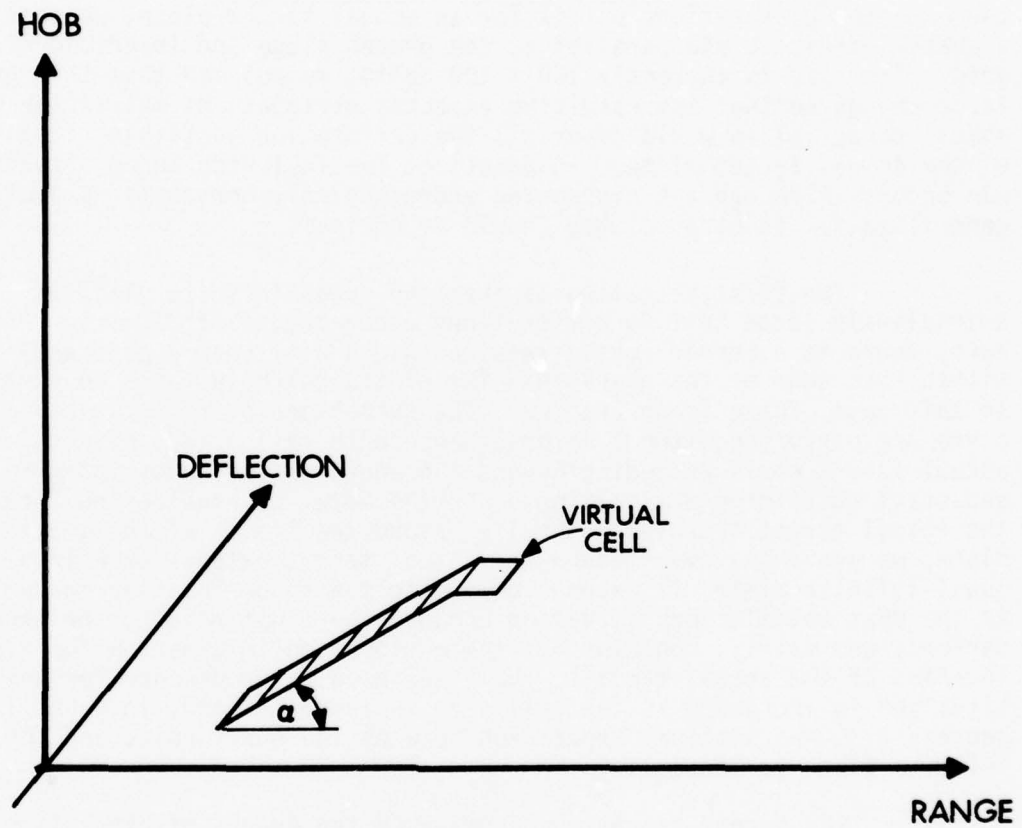


Figure 4.4. (U) A Target Strip and its Virtual Cell for the Target Plate of Figure 4.2a.

Figure 4-5 shows the two plates of Figure 4-2 combined to form a plate pair. The horizontal plate is not allowed to sustain perforations and serves merely as a spacer. The central cell of the plate pair is defined as the central cell of the top spacer and is computed from equations 4-7 applied to the top spacer. There is no longer a need for the virtual plate of paragraph 4.1.2 unless the top edges of the two non-horizontal plates are adjacent. In this case, the geometry can be visualized by letting the virtual plates of Figure 4-2 (or Figure 4-3) overlap each other completely. One of the angles, α and β , is always zero, the other is always positive and varies between 0° and 180° .

4.1.4 Problems Caused by Finite Grid Size. In order to obtain the expected perforations matrix for an actual target plate, we considered a quasi-infinite plate parallel to the ground plane and inscribed with a grid. The grid is currently 100×100 cells; we assumed that this grid was large enough so that the resulting expected perforations matrix for the actual target plate would cover all the perforation sustaining locations of the actual target plate. In practice, the following three situations can occur. Although the discussion addresses only horizontal plates, the generalization to other plates should be obvious.

The first situation is that the quasi-infinite plate is sufficiently large that no perforations occur beyond its limits. Furthermore, there is a border (whose required width will become apparent) just within each edge of the quasi-infinite plate, which sustains no perforations. In this case, there is no problem. The summations over the quasi-infinite plate are performed without errors (henceforth called edge effects) due to actual target cells extending beyond the edges of the quasi-infinite plate and still sustaining perforations. Furthermore, by considering locations of the actual target's center which lie beyond the limits of the quasi-infinite plate, we see that, even though the actual target extends back into the quasi-infinite plate, it extends only into the no perforation border. This is the most satisfactory situation because the final result, the expected perforations matrix, contains all the perforation information for every location of the actual target. The likelihood of occurrence for this situation is increased as the cell size is increased and, in general, decreased as the vertical separation between the burst point and the quasi-infinite plate is increased.

The second situation occurs when the quasi-infinite plate is sufficiently large that no perforations occur beyond its limits, but the no perforation border of the preceding situation either is absent or is not wide enough. An error called matrix truncation occurs (there are locations not represented by the expected perforations matrix for which the actual target will sustain perforations), but there are still no edge effects. This problem, if significant, can be eliminated by solving the same actual target again with a different projectile location with respect to the grid and manually piecing together the several expected perforations matrices, or by depending upon symmetry.

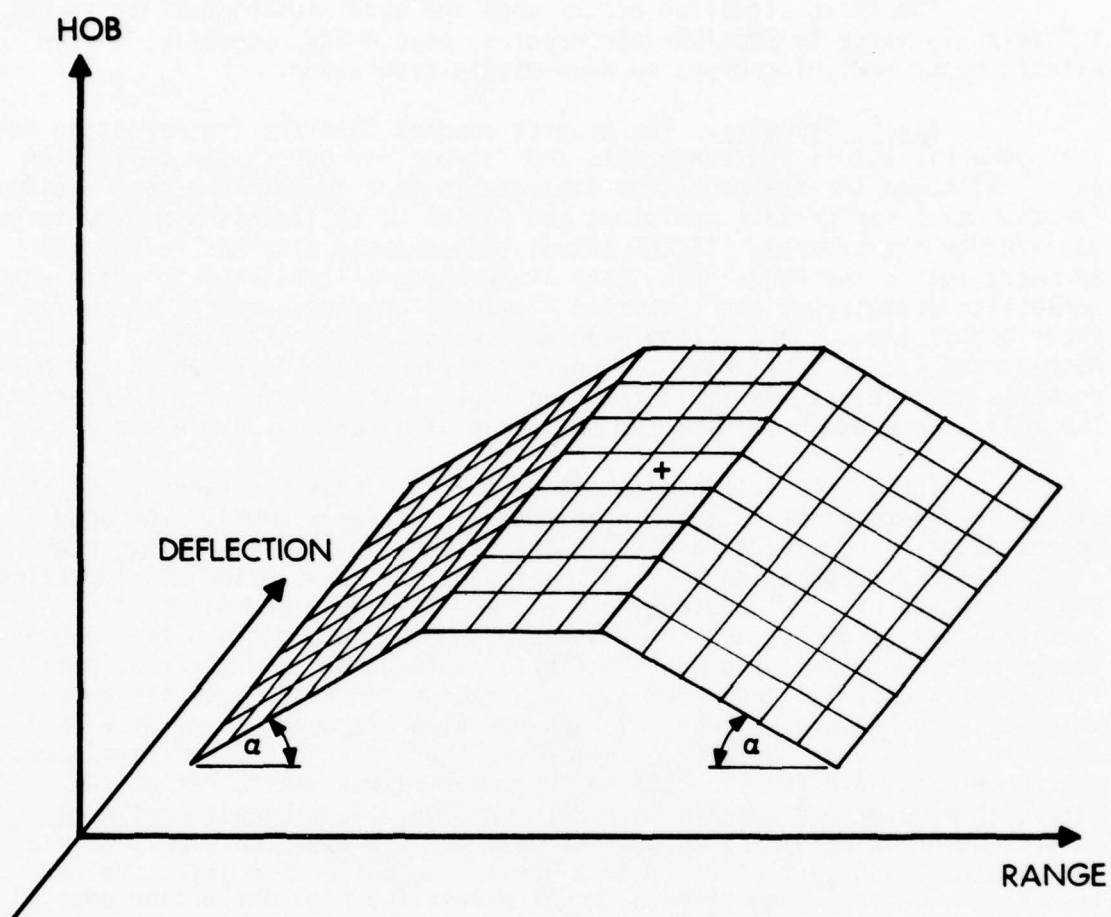


Figure 4.5. (U) A Plate Pair.

The third situation occurs when the quasi-infinite plate is not sufficiently large to preclude perforations beyond its boundaries. Edge effects occur and, of course, so does matrix truncation.

4.1.5 Symmetry. The program assumes that the fragmentation data are symmetric across the range axis and asymmetric across the deflection axis. Although the fragmentation data are in fact symmetric across the deflection axis for certain munitions and angles of fall, this symmetry is not utilized by the program. If the actual target plate also has reflection symmetry across the range axis, then the program will attempt to utilize the reflection symmetry of the system to eliminate any edge effects which may occur across the low deflection edge of the quasi-infinite plate. Thus, in such a case, it is beneficial to locate the range axis (over which the burst point is located) at the low deflection edge of the quasi-infinite plate. The following example illustrates the ideas of paragraphs 4.1.4 and 4.1.5.

The fragmentation data are symmetric across the range axis (as always) and across the deflection axis (angle of fall = 90°). The actual target plate is horizontal and so enjoys reflection symmetry across both axes. It is 36 inches long (along the range axis) and 20 inches wide (along the deflection axis). Considering the plate thickness and material, vertical separation between the plate and the burst point, and the fragmentation data, we expect the quasi-infinite plate to sustain perforations throughout a circular region of 400 inch radius centered under the burst point. We choose a four-inch cell and position the burst point at Z as shown in Figure 4-6. Because of symmetry, there are no edge effects across the range axis, and the expected perforations matrix can be reflected across this axis to eliminate matrix truncation. Very significant edge effects occur in columns 1 through 4; however, the user can simply delete these columns and reflect the matrix across the deflection axis. Matrix truncation, but not edge effects, occur across the high deflection edge of the matrix, but the error should be small because this area is at the far edge of the region in which perforations occur. Both matrix truncation and edge effects occur across the high range edge of the matrix but, again, the error should be small.

4.2 Output.

- a. The input data are printed out.
- b. The non-zero portion of the expected perforations matrix is written on the expected perforations file with a unique record number, which is the ordinal for that record. These records are sequentially and consecutively numbered for all cases within a batch (paragraph 4.3). Not more than 2500 records can be written on this file. If the entire matrix is zero, then a small zero matrix is written. If desired, the non-zero portion of the matrix can be printed. If the entire matrix is zero, its printing is suppressed. When printing occurs, each element is printed in an I6 format after being multiplied by a power of 10 (input data) and truncated.

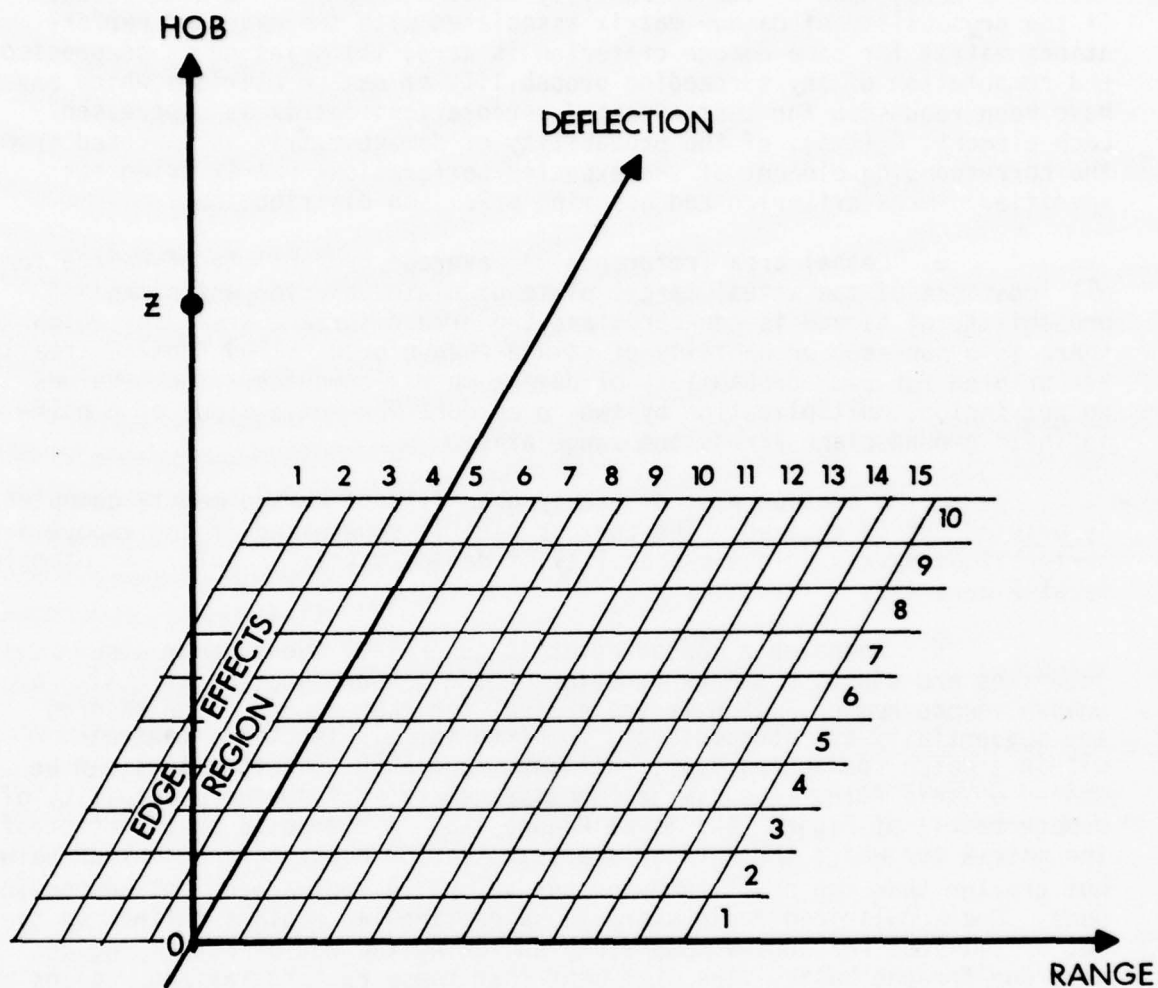


Figure 4.6. (U) A Situation Displaying Edge Effects.

c. The non-zero portion of the probability of damage matrix for each criterion is printed out if desired. If the expected perforations matrix is zero, none of its probability of damage matrices are computed. If the probability of damage matrix associated with the expected perforations matrix for some damage criterion is zero, its printing is suppressed and computation of any succeeding probability of damage matrices which may have been requested for that expected perforations matrix is suppressed. Each element, $P_d(i,j)$, of the probability of damage matrix is computed from the corresponding element of the expected perforations matrix using the specified damage criterion and assuming a Poisson distribution.

d. Lethal area (reference 3), average probability of damage for all locations of the actual target plate or plate pair for which the probability of damage is non-zero, and the ground surface area over which there is a non-zero probability of damage (henceforth called "damage area"), are printed for each probability of damage matrix computed. These values do not include multiplication by two to account for reflections of a half-infinite ground plane across the range axis.

e. A contour plot of each probability of damage matrix computed is printed out if desired. The contour plot is suppressed if the expected perforations matrix or the probability of damage matrix is null. An example is at Figure 4-7.

f. Whenever a contour plot is generated, the program also generates and stores a damage function on the damage function file with a unique record number, which is the ordinal for that record. The records are sequentially and consecutively numbered for all functions generated within a batch (paragraph 4.3). Not more than 5000 such functions can be stored on this file. The damage function generated from the probability of damage matrix of Figure 4-7 is at Figure 4-8. A region is that portion of the matrix for which the $P_d(i,j)$ are less than or equal to one contour value but greater than the next lower contour value. A region need not be continuous. Rectangularized regions are those rectangular regions defined by the set of smallest rectangles completely enclosing the set of actual regions on a one-for-one basis. The statement that these rectangularized regions are unnormalized means that lethal area and damage area are not conserved in their generation; hence, before they can be used, these damage functions must be normalized. The various regions in one damage function are written on the file from outermost to innermost. The maximum number of such regions is 11, corresponding to the regions within contour lines for $P_d = 1., .9, .8, \dots, .1$, and $.0005$.

4.3 Input Data Deck

This deck inputs a "batch", or "logical grouping", of cases. All cases within a batch have the same cell size, ground plane grid size, projectile location with respect to the grid, and fragmentation data. For the purposes of this paragraph, a "target" is one plate or one plate pair. A "case", then, is one target at one plate thickness and one projectile HOB. Each target is solved for every specified thickness at every specified HOB.

PROBABILITY OF SUSTAINING AT LEAST 1 PERFORATIONS

HOB= 4.69 METERS THICKNESS=1.00 INCHES CELL= 8.00 INCHES NX= 16 CELLS NY= 9 CELLS NZ= 0 CELLS T= 76.0 INCHES

SCALE FACTOR APPLIED TO INPUT PLATE = 1./1.000

NXX=100 CELLS NYY=100 CELLS PROJECTILE LOCATION WAS (55.5, .2)

THE EXPECTED PERFORATIONS MATRIX FOR THIS CASE IS ON THE EXPECTED PERFORATIONS FILE (PMAT348) AS RECORD NUMBER 1

LETHAL AREA= 16.500 SQUARE METERS AVERAGE PROBABILITY OF DAMAGE = .647 OVER 28.738 SQUARE METERS

OUTPUT OF THE PROBABILITY OF DAMAGE MATRIX HAS BEEN SUPPRESSED

THE PROBABILITY CONTOURS FOR THIS TARGET, HOB, AND DAMAGE CRITERION FOLLOW. THE NUMBERS ARE PD*10. (TRUNCATED), AND E=.0005, +-1.0

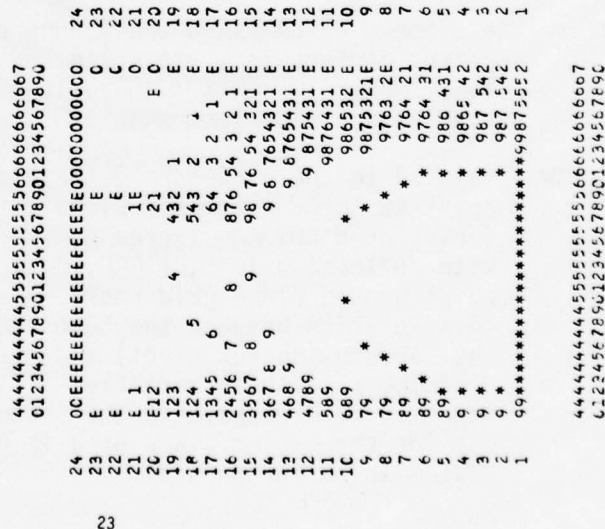


FIGURE 4-7. SAMPLE OUTPUT OF PROGRAM SECTION I

Unless otherwise stated, each data field is 10 columns wide and each numeric datum is in a real format with an explicit decimal point. Data fields not specifically addressed are ignored and may be used for any desired purpose, such as user comments within the data deck.

4.3.1 The Data Deck. The data deck for program section I is at Figure 4-9.

4.3.2 Definition of Each Input Variable

Card 1:

Columns 1-10 - the words "BASIC DATA".

FILES - the unique whole number identifying the first perforation matrix to be generated in this batch of cases. The perforation matrix file cannot contain more than 2500 records (matrices). FILES can be any whole number from 1 thru 2500. FILES is the first value of a consecutive series of numeric indices for the matrices to be generated and filed in the current batch of cases. FILES itself, however, need not be consecutive or even sequential with respect to the matrices stored in the perforation file by all preceeding batches. If FILES is not greater than the index of the highest indexed matrix placed in the file by all preceeding batches, some or all of the earlier matrices may be overlaid by matrices of the current batch. There is a default value for FILES. If FILES is blank or 0, its value is computed to be one greater than the index of the highest indexed matrix already in the file. If the file is empty, the default for FILES is 1.

CELL1 - the edge length, in inches, of the square cell which will be used to grid both the target and the ground plane.

NXX,NYY - the numbers of cells in the ground plane grid (and hence in the expected perforations matrix) along the range and deflection axes, respectively; $1. \leq NXX \leq 100.$; $1. \leq NYY \leq 100.$; in practice, these variables would be less than 100. only to save machine time.

ICOL,IROW - related to the range and deflection coordinates of the burst point in terms of ground plane grid columns and rows, respectively; grid columns increase with range and grid rows increase with deflection left; (ICOL,IROW) = (50.,0.) would yield burst point ground plane grid coordinates = (50.5,.5), corresponding to a location between the 50th and 51st grid columns and between the zeroeth (non-existent) and first grid rows; in practice, the usefulness of these variables is to shift the ground plane grid location with respect to the (fixed) burst point; a burst point outside the ground plane grid is allowed, with the exception stated in paragraph 5.3.

THESE DATA ARE ON THE DAMAGE FUNCTION FILE (DFCN548) AS RECORD NUMBER 1

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
	PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
1.000	7.143	7.143	7.143	7.143
.971	5.731	12.874	5.905	13.048
.848	1.365	14.239	1.610	14.658
.749	.866	15.105	1.156	15.814
.651	.806	15.912	1.239	17.053
.551	.774	16.685	1.404	18.457
.449	.593	17.278	1.321	19.778
.354	.467	17.746	1.321	21.099
.249	.411	18.157	1.652	22.751
.146	.259	18.416	1.775	24.527
.041	.172	18.588	4.212	28.738

RECTANGULARIZED, UNNORMALIZED RANGE DATA				RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
AVERAGE PD WITHIN EACH REGION		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION	
		METERS	CELLS			METERS	CELLS
1.000	4.267	21.0	21.0	-7.11	-3.5	2.032	10.0
.971	5.080	25.0	25.0	-7.11	-3.5	3.048	15.0
.848	5.283	26.0	26.0	-6.10	-3.0	3.251	16.0
.749	5.486	27.0	27.0	-5.08	-2.5	3.251	16.0
.651	5.486	27.0	27.0	-5.08	-2.5	2.845	14.0
.551	6.096	30.0	30.0	-2.03	-1.0	3.658	18.0
.449	6.096	30.0	30.0	-2.03	-1.0	3.658	18.0
.354	6.096	30.0	30.0	-2.03	-1.0	3.048	15.0
.249	6.299	31.0	31.0	-1.02	-.5	4.064	20.0
.146	6.299	31.0	31.0	-1.02	-.5	3.454	17.0
.041	6.299	31.0	31.0	-1.02	-.5	3.454	17.0

FIGURE 4-6. DAMAGE FUNCTION PRODUCED FROM PROBABILITY OF DAMAGE MATRICES CORRESPONDING TO FIGURE 4-7

Card 2:

NHOB - the number of HOB's to be considered in this batch of cases;
 $1. \leq \text{NHOB} \leq 25.$

HHHOB(I) - the I^{th} HOB to be considered in this batch of cases; in meters.

As many as three additional cards may occur here to input up to 25 values of HHHOB; each additional card starts with a value of HHHOB in the first data field (columns 1-10).

Card 3:

NTHCK - the number of armor plate thicknesses to be considered in this batch of cases; each thickness is considered for each HOB;
 $1. \leq \text{NTHCK} \leq 25.$

TTHCK(I) - the I^{th} thickness to be considered in this batch of cases; in inches.

As many as three additional cards may occur here to input up to 25 values of TTHCK; each additional card starts with a value of TTHCK in the first data field (columns 1-10).

Card 4:

NTRGT - the number of targets to be considered in this batch of cases;
 $1. \leq \text{NTRGT} \leq 25.$; each target is considered for each thickness, thus, the number of cases in this batch is $\text{NTRGT} * \text{NTHCK} * \text{NHOB}$; an overall constraint is $1. \leq \text{NTRGT} * \text{NTHCK} * \text{NHOB} \leq 2500.$

Card 5:

There are NTRGT cards 5; each provides information for one target in this batch of targets; all targets will be solved for the first thickness at the first HOB, then for the second thickness at the first HOB, and so on until all thicknesses have been exhausted, then for the first thickness at the second HOB, and so on until all HOB's have been exhausted.

NXTGT(I) - the number of cells along the range axis in the I^{th} plate or in the spacer of the I^{th} plate pair.

NYTGT(I) - the number of cells along the deflection axis in the I^{th} plate or in the spacer of the I^{th} plate pair.

NZTGT(I) - the number of cells along the slope in the I^{th} plate or plate pair; zero or blank for horizontal plates.

NSIDE(I) - zero or blank for horizontal plates; 1. for single non-horizontal plates; 2. for plate pairs.

- ALPHA(I) - $0. \leq |\text{ALPHA}(I)| < 180.$; the angle in degrees from the horizontal down to the outer surface of the I^{th} plate or plate pair; positive for plate pairs and plates whose outward drawn normal vector has a component in the direction of increasing range; negative otherwise; zero for plates rotated about the range axis and for horizontal plates.
- BETA(I) - $0. \leq |\text{BETA}(I)| < 180.$; the angle in degrees from the horizontal down to the outer surface of the I^{th} plate or plate pair; positive for plate pairs and plates whose outward drawn normal vector has a component in the direction of increasing deflection (deflection left); negative otherwise; zero for plates rotated about the deflection axis and for horizontal plates.
- TT(I) - the height of the top surface or top edge of the I^{th} plate or plate pair above the ground plane; in inches.
- SC(I) - 5 column field; actually SCALE(I); a scale factor used to adjust for minor mismatch between actual and model plate surface areas; has no effect on direct hit contributions; equal to the surface area of the plate being input to the program divided by the surface area of the plate being modeled; default value is 1.
- SH(I) - 5 column field; actually SHOW(I); non-negative whole number; the power to which 10. will be raised and then used to multiply each element of the expected perforations matrix prior to output of that matrix; if SH(I) = 0. or blank, the I^{th} matrix is not output; the output field for each element of the matrix is I6, including spaces between elements.

Card 6:

- NKRIT - the number of damage criteria which will be considered for each case in this batch; $1. \leq \text{NKrit} \leq 7.$
- KRIT(I) - the I^{th} damage criterion; KRIT(I) > 0; the input vector must be monotone increasing.

Card 7:

Columns 1-10 - the words THOR DATA; identifies the following two cards as providing Thor constants; from and in the same units as Thor reports 47, 70 (references 1,2); if not present, cards 8 and 9 also must be not present and Thor constants from the immediately preceding batch of cases will be used.

Card 8:

- METAL - 10 alphanumeric characters; the user's own name for the material to which the Thor constants apply.

CV, ALFAV, BETAV, GAMAV, LAMDAV, KFCTRV - Thor constants for the residual velocity equations with no particular fragment shape assumed; KFCTRV is blank or 0. if the armor is not an aluminum for which K-factors are available, as in Thor report 70 (reference 2).

Card 9:

CM, ALFAM, BETAM, GAMAM, LANDAM, KFCTRM - Thor constants for the residual mass equations with no particular fragment shape assumed; KFCTRM is blank or 0. if the armor is not an aluminum for which K-factors are available, as in Thor report 70 (reference 2).

Card 10:

- W - the projectile angle of fall in degrees.
- VTM - The projectile terminal velocity in feet per second.
- BLAST - radius in inches of the blast effects sphere, within which the probability of damage is 1.

Card 11:

Columns 1-10 - the word, FRAGMENTAT; identifies subsequent cards as providing the fragmentation distribution; if not present, cards 12 through 17 also must not be present and the fragmentation data from the immediately preceding batch of cases, or from the immediately preceding execution of program Section IV, will be used.

- SHAPE - the fragment shape factor; in grains/cubic inch.
- AA - a constant in the velocity decay equation (see equation 4-5).

Card 12:

- NSPRA - the number of fragment sprays in the fragmentation data;
 $3. \leq \text{NSPRA} \leq 46.$
- NSP(I) - the number of mass values in the Ith spray; this vector may be continued on as many as 5 additional cards, starting in column 1 of each, for NSPRA elements in NSP; $1. \leq \text{NSP}(I) \leq 40.$, all I.

Card 13:

There may be as many as 46 sets of as many as 11 cards each to input as many as 40 Q(J,K), M(J,K) pairs for each of the NSPRA fragment sprays; K runs from 1 to NSPRA; J runs from 1 to NSP(K).

- K - the spray number.

- Q(J,K) - the fraction of all fragments in the K^{th} spray residing in the J^{th} mass interval.
- M(J,K) - the mass assigned to fragments residing in the J^{th} mass interval of the K^{th} fragment spray; in grains; for any given K, the M(J,K) must be monotone increasing.

Card 14:

There may be as many as 46 cards #14 to define NSPRA fragment sprays.

- K - the spray number.

SPRBS(K), SPRBS(K+1) - the leading and trailing edges of the K^{th} fragment spray; in degrees; the leading (trailing) edge of the first (last) spray must be $0.^{\circ}$ ($180.^{\circ}$); the sprays must be continuous from 0° through 180° .

VSTMN(K) - the median fragment velocity at the midpoint of the K^{th} fragment spray; in feet per second; the midpoints of the first and last sprays are defined as $0.^{\circ}$ and $180.^{\circ}$, respectively.

VSTMX(K) - the maximum fragment velocity at the midpoint of the K^{th} fragment spray; in feet per second; the midpoints of the first and last sprays are defined as $0.^{\circ}$ and $180.^{\circ}$, respectively.

NUM(K) - the number of fragments in the K^{th} fragment spray; if 0. or blank, will be computed from SGST(K).

SGST(K) - the density of fragments (number per steradian) in the K^{th} fragment spray; if 0. or blank, will be computed from NUM(K).

Card 15:

An optional card which may use either of two formats.
The first format is:

Columns 1-10 - the word CONTOUR; causes a contour map of the probability of of damage matrix to be output for each case and damage criterion of the current batch; also causes generation of a damage function, storage thereof on the damage function file, and printed output thereof.

NSTAPE - the unique whole number identifying the first damage function to be generated in this batch of cases. The damage function file cannot contain more than 5000 records (functions). NSTAPE can be any whole number from 1. thru 5000. NSTAPE is the first value of a consecutive series of numeric indices for the functions to be generated and filed in the current batch of cases. NSTAPE itself,

however, need not be consecutive or even sequential with respect to the functions stored in the damage function file by all preceeding batches. If NSTAPE is not greater than the index of the highest indexed function placed in the file by all preceeding batches, some or all of the earlier functions may be overlaid by functions of the current batch. There is a default value for NSTAPE. If NSTAPE is blank or 0., its value is computed to be one greater than the index of the highest indexed function already in the file. If the file is empty, the default for NSTAPE is 1.

Columns 21-30 - the words NO PROBABI; causes suppression of the printing of all the probability of damage matrices for this batch.

The alternate format is:

Columns 1-10 - the words NO PROBABI, as above.

Columns 31-40 - the word CONTOUR, as above.

Columns 41-50 - the variable NSTAPE, as above.

5. PROGRAM SECTION II - VULNERABILITY OF ARMORED STRUCTURE

5.1 The Program.

The function of program Section II is to assemble the expected perforations matrices (generated by Section I and retrievable from the perforation matrix file) for as many as seven plates or plate pairs to obtain the expected perforations matrix, probability of damage matrices, and damage functions for one complete target. All the matrices which are combined for any one case must be for the same cell size and projectile HOB, angle of fall, and terminal velocity. There can be up to 25 cases in one batch. The manner in which the expected perforations matrices associated with several plates are combined to form the expected perforations matrix for a complete target is best described through the use of an example.

5.1.1 Assembling a Complete Target. Consider the target shown in Figure 5-1, which shows a side view with elevation, a side view, and a front view. Plates seen on edge have tick marks to indicate cell boundaries. The extent of plates seen on edge is indicated. The scale and coordinate system are common to all three views. Data for each plate or plate pair are shown in Table 5-1.

Plate A is embedded in the spacer BB which can sustain no perforations. Between the edges of plate A and the top edges of sides B is a region which could correspond to heavily armored parts of an actual structure. The shaded region is the virtual plate associated with plate C. Reflection symmetry exists across the range axis.

Figures 5-2, 5-3, and 5-4 provide examples of additional plates which could be part of the complete structure, but which are not considered in the current example. Partial data are given in Table 5-1. These plates are shown to indicate how reasonably complex structures can be built up and to show various possible values of ALPHA, BETA, AND TT. The points Q, R, and S of Figures 5-2, 5-3, and 5-4 correspond to those same points in Figure 5-1.

Consider plate A with central cell D and plate pair B with central cell E. We define plate A as the reference plate for the structure; its central cell will become the central cell for the entire structure.

Using the ground plane grid of Figure 4-6, element (I,J) of the appropriate expected perforations matrix is the expected number of perforations sustained by plate A when its central cell (D) is positioned over cell (I,J) of the ground plane. Similarly, element (I+1,J) of another expected perforations matrix is the expected number of perforations sustained by plate pair B when its central cell (E) is positioned over cell (I+1,J) of the ground plane. Thus, for all rows J and all columns I:

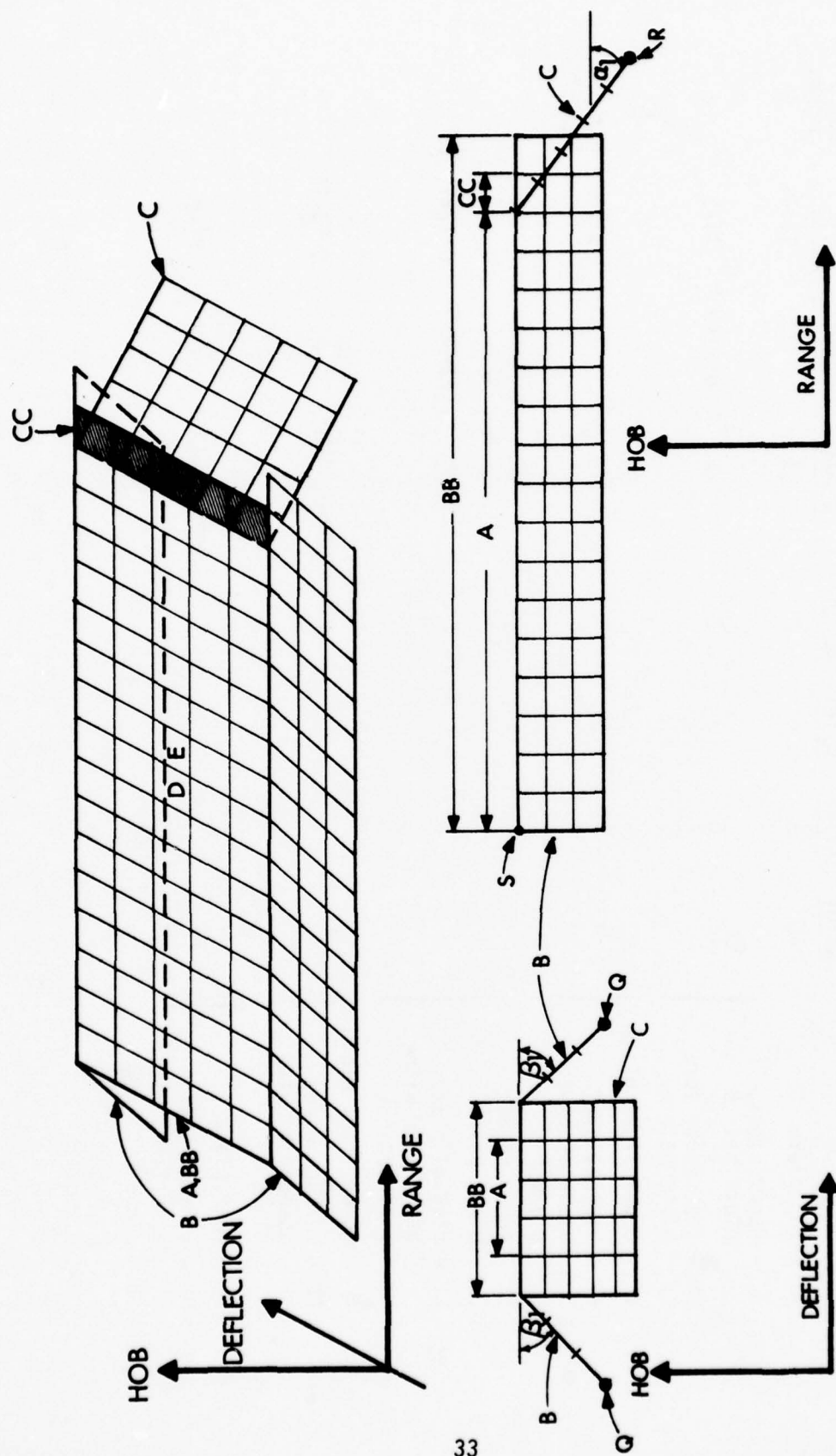


Figure 5.1 (U) Model of a Complete Target.

TABLE 5-1. DATA FOR PLATES OF FIGURES 5-1 THROUGH 5-4

	NXTGT	NYTBT	NZTGT	NSIDE	ALPHA	BETA	TT	CENTRAL CELL
A - top plate	16	3	0	0	0	0	T1>0	D
B - upper sides, plate pair B	18	5	3	2	0	0< α 1<90°	T1>0	E
BB - top spacer for plate pair B								
C - upper front plate	0	5	5	1	0< α 1<90°	0	T1>0	F
CC - virtual plate associated with plate C								
L - lower sides, plate pair				2	0	β 2=90°	0<T2<T1	
LL - virtual plate associated with plate pair L								
M - lower front plate	0			1	90°< α 2<180°	0	0<T3<T1	
MM - virtual plate associated with plate M								
N - rear plate	0			1	-90°> α 3>-180°	0	T1>0	
NN - virtual plate associated with plate N								

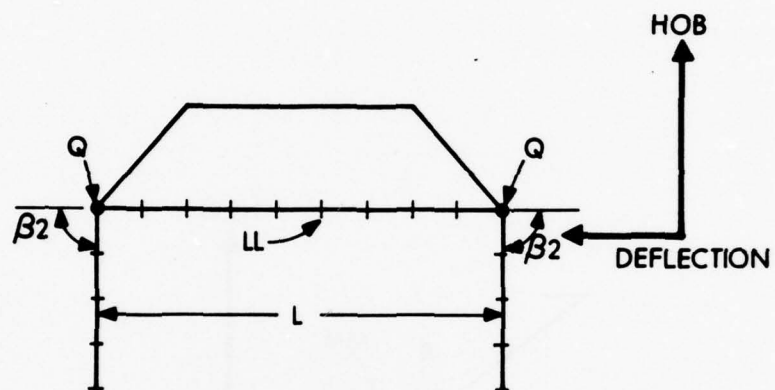


Figure 5.2 (U) Lower Sides Which Could be Added to the Model of Figure 5.1.

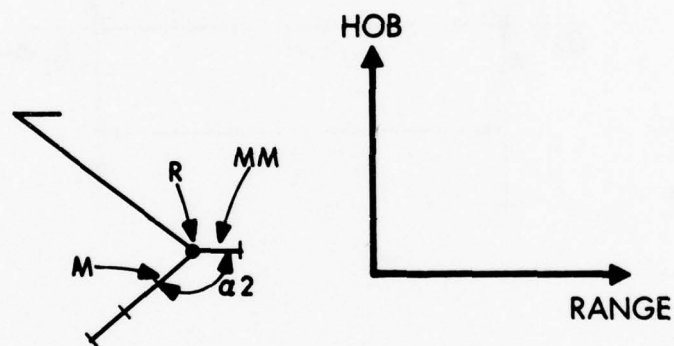


Figure 5.3 (U) Lower Front Plate Which Could be Added to the Model of Figure 5.1.

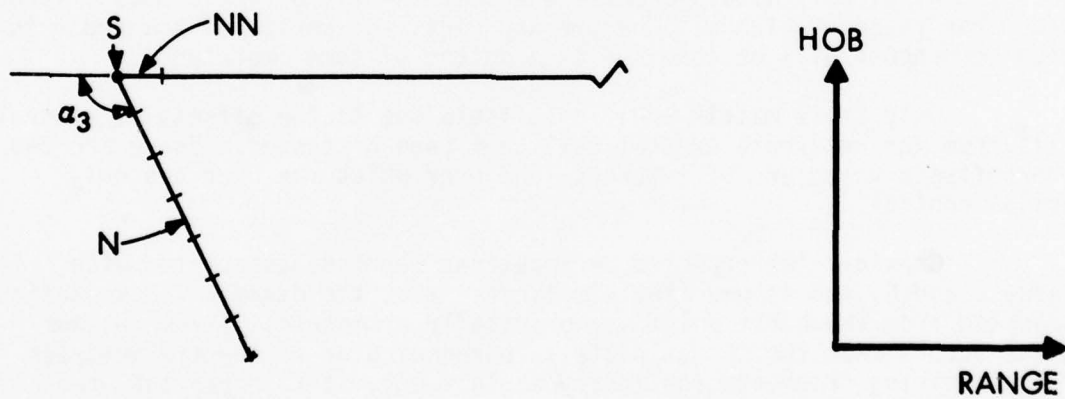


Figure 5.4. (U) Rear Plate Which Could be Added to the Model of Figure 5.1.

$$EPM_{A,B}(I,J) = EPM_A(I,J) + EPM_B(I+1,J) \quad \text{Equation 5-1}$$

where $EPM_{A,B}(I,J)$ means element (I,J) of the expected perforations matrix for the structure made up of plate A and plate pair B. Similarly,

$$EPM_{A,B,C}(I,J) = EPM_{A,B}(I,J) + EPM_C(I+8,J) \quad \text{Equation 5-2}$$

or

$$EPM_{A,B,C}(I,J) = EPM_A(I,J) + EPM_B(I+1,J) + EPM_C(I+8,J) \quad \text{Equation 5-3}$$

Thus, the expected perforations matrix for a complete structure is obtained by adding, with appropriate offsets, the expected perforations matrices for individual components.

It would be most efficient to first compute the offsets in range and deflection and then add all the matrices together, element by element, at once, as indicated by Equation 5-3. This, however, was beyond the storage capability of the computer for which this program was originally developed (BRLESC I/II of the USABRL); therefore, Equations 5-1 and 5-2 are used. The first two components are combined to obtain an intermediate structure which is then treated as a component with which the next component is combined, and so on. Therefore, the first component (the one identified by logical record number FILE(1)) is always used as the reference component and its central cell always becomes the central cell of the complete structure. For reasons which will become apparent, the choice of the order in which components will be combined is a matter of some importance.

Only those matrix addition offsets due to the offsets of central cells from the reference central cell have been discussed. There are two other offsets which are of interest, and over which the user has only partial control.

Consider the expected perforations matrices associated with plates A and C, and assume (for simplicity) that the dynamic fragmentation projected from the burst point is spherically symmetric. Since maximum damage occurs when the struck plate is perpendicular to the trajectories of the striking fragments (obliquity angle = 0°), it is clear that the region of maximum damage for plate C will be in lower numbered columns than it will be for plate A, for a wide range of HOB's. Hence, the user well may have positioned the projectile over different grid points when computing EPM_A and EPM_C in order to minimize matrix truncation (paragraph 4.1.1) for each of these plates. The program automatically compensates for any such offsets in projectile locations.

The following describes the second type of offset. Assume $NXX = NYY = 100$ for each expected perforations matrix. The various offsets

applied when combining these component matrices may result in an expected perforations matrix for the complete structure which extends beyond one or more sides of the $NXX \times NYY$ cell grid. Each time a component matrix is added into the result of previous additions (or into the reference matrix, if the addition is the first one to be performed), the program will attempt to minimize matrix truncation by rigidly translating the entire plates/projectile system within the grid. However, the program always gives preference to the prior matrices over the later matrices; that is, regardless of the magnitudes of the matrix elements being lost, and regardless of the number of such elements, the program will never shift any part of a prior matrix or matrix sum out of the grid in order to accommodate the matrix currently being added in. Therefore, consideration must be given to the order in which the component matrices are presented to the program (i.e.: the order of the NFILE elements of the set {FILE(I)}; see paragraph 5.4) and the dominant matrices should be presented first.

5.1.2 Symmetry and an Example. As in the case for Section I of the program, Section II can make use of symmetry across the range axis, and the user can utilize symmetry across the deflection axis. Consider the structure of Figure 5-1 as a target oriented in the direction of increasing range. Clearly, reflection symmetry exists across the range axis for each target component and also for the complete target. Therefore, the burst point for each component should be located between ground plane grid rows 0 (non-existent) and 1 so that each component's expected perforations matrix will contain maximum information. As the target is assembled, there will be no need to shift the burst point from this zero deflection location (shifts in range may occur) and the final matrix also will contain maximum information. A similar discussion applies to the same vehicle oriented in the direction of decreasing range.

Rotate the structure of Figure 5-1 clockwise by 90° and consider it as a target oriented across the range axis in the direction of decreasing deflection (Figure 5-5). (Note that the virtual plate belonging to plate C has changed its orientation with respect to plate C, and now lies on top of one end of plate A.) Since the fragmentation is symmetric across the range axis, it is clear that the solution over the entire ground plane differs from that for the same target oriented in the direction of increasing deflection only by a reflection across the range axis. Thus, we need only one of the two orientations for the target broadside to the range axis. We cannot, however, proceed (as in the preceding paragraph) to solve over the half-infinite ground plane, and depend on reflection symmetry of the target itself to obtain the complete solution, because target reflection symmetry does not exist. The problem can be overcome in either of two ways. The first is to position the burst point somewhere over the center of the ground plane grid. This is completely satisfactory so long as the user can stand the (extreme) matrix truncation which may occur. The other method will be discussed in paragraph 5.3. At this point, we present an example to illustrate the solution over the half-infinite plane of the target facing in the direction of decreasing deflection.

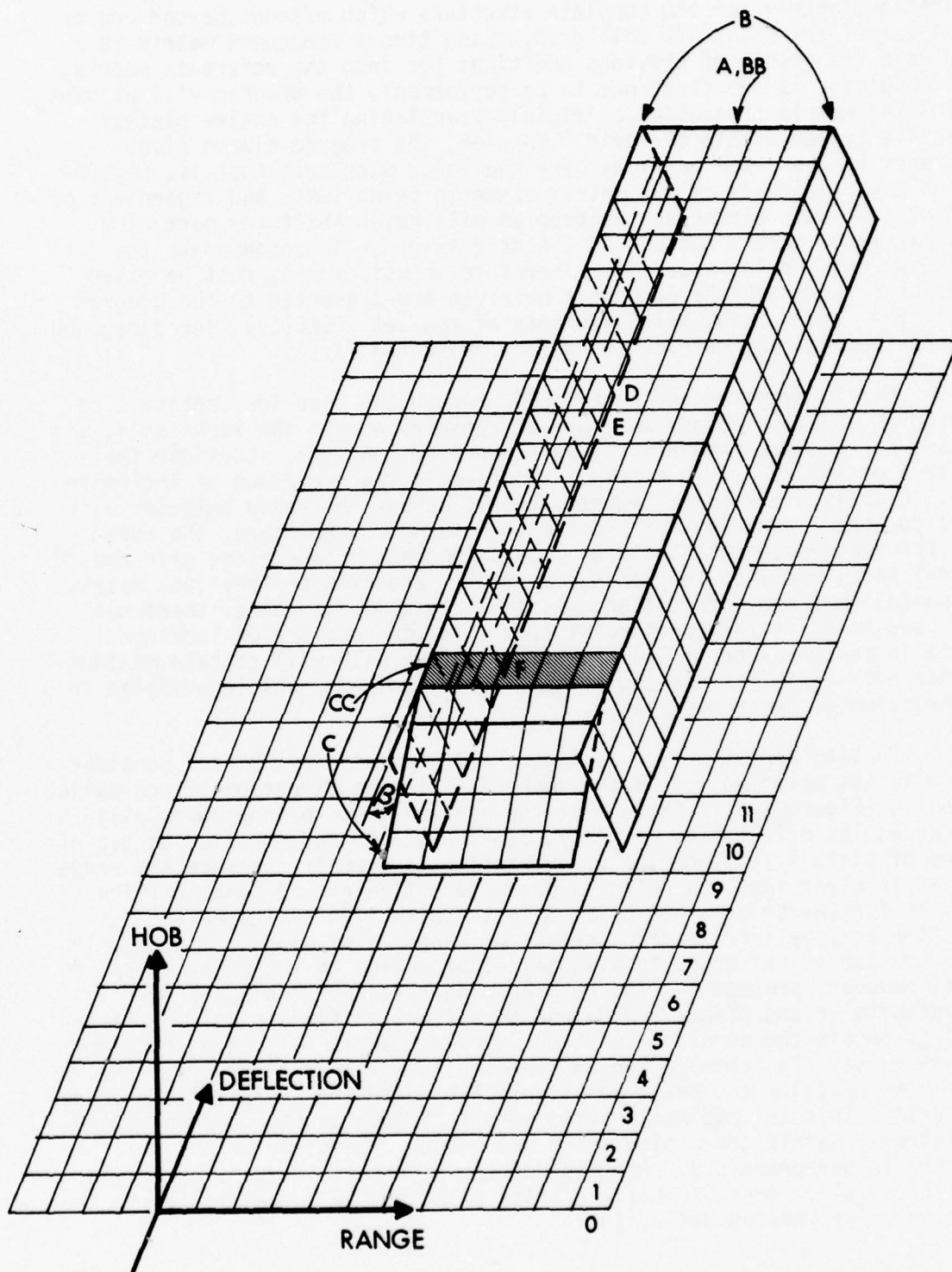


Figure 5.5 (U) The Target Model of Figure 5.1 Oriented in the Direction of Decreasing Deflection.

We have stored in a file the expected perforations matrices for each target component (plate A, plate pair B, and plate C of Figure 5-5). When these matrices were computed, we chose the projectile burst locations with some care; for components A and B, it was between grid rows 0 (non-existent) and 1, and for component C, it was between grid rows 9 and 10. Plate A is considered the reference plate and its central cell is the central cell for the entire structure. As stated previously, the perforation matrices for the several components are additive so long as the proper offsets are maintained. To determine which element of a component's perforation matrix should be added to an element of the reference plate's or reference structure's perforation matrix, we use Equation 5-4 and a similar equation for matrix columns.

(component matrix row to be added in)

$$\begin{aligned}
 &= \text{(structure matrix row under consideration)} \\
 &+ \text{(row offset of component central cell with respect to structure central cell)} \\
 &+ \text{(row offset of burst point in component matrix with respect to burst point in structure matrix)}
 \end{aligned}
 \tag{Equation 5-4}$$

For plate pair B, the last two terms of Equation 5-4 are -1 and 0, respectively. Furthermore, there are no column offsets. Therefore,

$$EPM_{A,B}(I,J) = EPM_A(I,J) + EPM_B(I,J-1) \tag{Equation 5-5}$$

We note that when cell D is in grid row 1, there is no information available for plate pair B and hence we would have an edge effect error, except for the fact that plate pair B enjoys reflection symmetry across the range axis.

A general statement is that, if matrix B has central cell row offset, K, and burst point row offset, L, then

$$EPM_{A,B}(I,J) = EPM_A(I,J) + EPM_B(I,J+K+L) \tag{Equation 5-6}$$

Furthermore, if component B enjoys reflection symmetry across the range axis and if $K < 0$ and $K + L < 0$, then, when $J \leq |K + L|$, Equation 5-6 is replaced by Equation 5-7.

$$EPM_{A,B}(I,J) = EPM_A(I,J) + EPM_B(I,1-(J+K)+L) \tag{Equation 5-7}$$

Returning to the specific case at hand, we have Equation 5-5 which holds except when cell D is in grid row 1. When cell D is in grid row 1, we use Equation 5-8, obtained from Equation 5-7.

$$EPM_{A,B}(I,J) = EPM_A(I,J) + EPM_B(I,2-J) \tag{Equation 5-8}$$

Thus far, we have obtained the expected perforations matrix for the structure of Figure 5-5, not including plate C. The structure's central cell is cell D. The range axis is still located between grid rows 0 (non-existent) and 1. The structure does not enjoy reflection symmetry across the range axis (because plate pair B sticks out in front of plate A, but not in back of it), but this is of no importance because the structure is not added into anything; rather, components are added into the structure. To add plate C into the structure, we use equation 5-9, obtained from equation 5-6 with $K = -9$ and $L = 9$

$$EPM_{A,B,C}(I,J) = EPM_{A,B}(I,J) + EPM_C(I,J) \quad \text{Equation 5-9}$$

It should now be clear that the entire purpose for locating the range axis for plate C between grid rows 9 and 10 was to avoid edge effects due to plate C when the central cell of the structure is near the burst point. Equation 5-7 could not have been used because plate C does not enjoy reflection symmetry across the range axis.

5.2 Output.

Program status at this point is very similar to its status after computations for a target component have been completed by Section I. The output is the same as in paragraph 4.2 with the following exceptions:

- a. The expected perforations matrix for the complete structure is not stored on the perforation matrix file.
- b. There is no suppression of probability of damage matrices or of the contour plots and damage functions due to null matrices.

5.3 An Additional Capability for Targets Displaying Asymmetry Across the Range Axis.

Consider the target of Figure 5-5 and allow it to assume both orientations perpendicular to the range axis in both half-infinite parts of the ground plane. Figure 5-6 illustrates the four possibilities. For each case, the target is symmetric across the deflection axis and asymmetric across the range axis. The fragmentation is symmetric across the range axis and asymmetric across the deflection axis. The expected perforations matrices for A and D are reflections of each other, and similarly for B and C. Furthermore, the matrices representing the complete solutions (A,C and B,D) are reflections of each other. Hence, the solutions for A and B contain all the information required for a solution of either orientation over the entire ground plane. The program has the capability of performing the symmetry operations, required to piece together the matrices A and for B, thereby obtaining the complete solution for both orientations. The output, including lethal area, average probability of damage, and damage area, will pertain to the complete ground plane. To use this capability, we must have $0 \leq IROW < NXX$ (see paragraph 4.3.2, card 1 for IROW) for both of the complete structure matrices, A and B. Furthermore,

both values of IROW should be small because the portions of the two matrices A and B in rows numbered less than or equal to the corresponding IROW value are lost as the two matrices are pieced together. For a similar reason, ICOL should be approximately the same for both matrices.

Note that this treatment depends upon the reflection symmetry of the structure across the deflection axis. If the structure suffers asymmetry across that axis, a very similar treatment applies, but the result has a different interpretation. In this event, structures B, D are not actual structures with orientation opposite to A, C. Rather, they are hypothetical structures which are reflections of A, C across the range axis. Furthermore, after the matrices for A and B are pieced together at the range axis, the resulting matrix A, B represents only A and C. If orientation B and D is desired, then the solution for a second set of conditions (structure B, reflected structure A) must be obtained.

5.4 Input Data Deck.

This deck inputs a batch of cases. A case is one target (usually consisting of more than one component), projectile, burst point combination. A batch may contain as many as 25 cases and, although there is usually some relationship among the cases within a batch, there need not be. If the capability of paragraph 5.3 is used, the cases must come in pairs, and there can be 25 such pairs. In this situation, the comments previously made pertaining to a case pertain to a case pair.

Unless otherwise stated, each data field is 10 columns wide and each numeric datum is in a real format with an explicit decimal point. Data fields not specifically addressed are ignored and may be used for any desired purpose.

5.4.1 The Data Deck. The data deck for program Section II is at Figure 5-7.

5.4.2 Definition of Each Input Variable.

Card 1:

Columns 1-10 - the word ASSEMBLE.

- | | |
|-------|--|
| KSYM | - KSYM = 2. causes the union of 2 expected perforations matrices at their range axes to represent, over the entire ground plane, a complete target; otherwise ignored. |
| NPNTS | - has two somewhat different interpretations; if KSYM \neq 2., NPNTS is the number of cases in this batch, a case being one complete target at one set of projectile conditions; if KSYM = 2., NPNTS is the number of case pairs in the batch; in either case, $1 \leq \text{NPNTS} \leq 25$. |

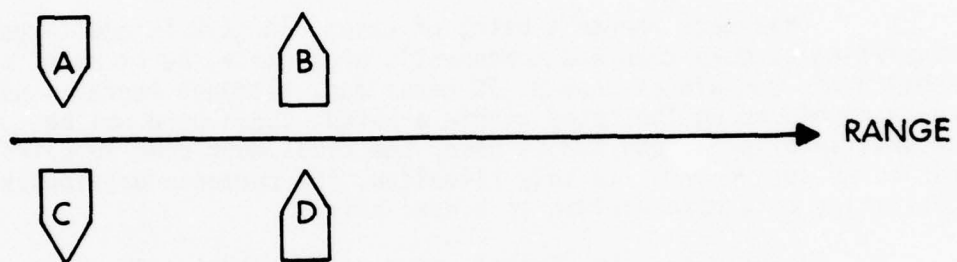


Figure 5-6. (U) Possible Target Orientations.

COLUMN	111111111222222222233333333334444444445555555556666666667777777778
NUMBER	1234567890123456789012345678901234567890123456789012345678901234567890
CARD	
NUMBER	

1	ASSEMBLE	KSYM	NPNTS	CONTOUR	NSTAPE	NO PROBABILITY MATRIX
2	EXPECTED PERFORATIONS ALL					
3	SHOW(1)	SHOW(2)	SHOW(3)	...		
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF SHOW ***					
4	MKRIT	KRIT(1)	KRIT(2)	KRIT(3)	...	
5	NFILE	FILE(1)	FILE(2)	FILE(3)	...	
6	SHIFT X		SHFTX(2)	SHFTX(3)	...	
7	SHIFT Y		SHFTY(2)	SHFTY(3)	...	
	*** UP TO 24 MORE SETS OF THE ABOVE 3					
	CARDS, AS NEEDED, FOR UP TO 25 CASES ***					

FIGURE 5-7. DATA DECK FOR PROGRAM SECTION II

Columns 21-30 - the word CONTOUR; causes a contour map of the probability of damage matrix to be output for each case and damage criterion of the current batch; also causes generation of a damage function, storage thereof on the damage function file, and printed output thereof; otherwise, ignored.

NSTAPE - the unique whole number identifying the first damage function to be generated in this batch of cases. The damage function file cannot contain more than 5000 records (functions). NSTAPE can be any whole number from 1. thru 5000. NSTAPE is the first value of a consecutive series of numeric indices for the functions to be generated and filed in the current batch of cases. NSTAPE itself, however, need not be consecutive or even sequential with respect to the functions stored in the damage function file by all preceding batches. If NSTAPE is not greater than the index of the highest indexed function placed in the file by all preceding batches, some or all of the earlier functions may be overlaid by functions of the current batch. There is a default value for NSTAPE. If NSTAPE is blank or 0., its value is computed to be one greater than the index of the highest indexed function already in the file. If the file is empty, the default for NSTAPE is 1.

Columns 51-60 - the words NO PROBABI; causes suppression of the printing of the probability of damage matrices for this batch; otherwise, ignored.

Card 2:

This is an optional card.

Columns 1-10 - the words EXPECTED P; causes output of the expected perforations matrices for individual cases of this batch as indicated below:

Columns 23-30 - in columns 23-26, ALL= and in columns 27-30, a whole number > 0., which number is the power to which 10. will be raised and then used to multiply each element of the expected perforations matrix; the fractional part of each element will be truncated and the matrix will be output in I6 format.

Card 3:

This card is present only if card 2 is present and columns 23-26 thereof are not as described above. There must be NPNTS values of SHOW(I), where SHOW(I) is defined in paragraph 4.3.b., card 5; any Ith matrix for which SHOW(I) = 0. will not be output.

Card 4:

- NKRIT - the number of damage criteria which will be considered for each case in this batch; $1 \leq \text{NKRIT} \leq 7$.
- KRIT(I) - the I^{th} damage criterion; $\text{KRIT}(I) > 0$.

Card 5:

Cards 5, 6, and 7 form a set which completely defines one case in this batch of cases. Either or both of cards 6 and 7 may be omitted for any card 5, in which case the values from the immediately preceding card 6 or 7 are used. If cards 6 or 7 or both are missing for the first case of the batch, the values are taken to be zero. If $\text{KSYM} = 2$, a special rule applies. There must be 2 sets of cards 5,6,7 to define a case; the first triplet defines the first half of the case pair and the second triplet, the second half. Both cards 5 must be present for the case, even if they are identical to each other. Cards 6, 7 may be present or absent with the same effect between the halves of a case and between cases as occurred between cases for $\text{KSYM} \neq 2$.

- NFILE - the number of logical records (expected perforations matrices for individual plates or plate pairs) required to obtain the expected perforations matrix for the complete target specified by this set of cards 5, 6, and 7; $1 \leq \text{NFILE} \leq 7$.
- FILE(I) - the unique logical record number associated with the expected perforations matrix stored on the expected perforations file for the I^{th} plate (or plate pair) of the current target.

Card 6:

Columns 1-10 - the words SHIFT X =

- SHFTX(I) - the number of cells by which the central cell of the I^{th} component plate (or plate pair) of this complete target is offset from the central cell of the first component of this complete target along the range axis; I must run from 2 to NPNTS.

Card 7:

Columns 1-10 - the words SHIFT Y =

- SHFTY(I) - same as SHFTX(I), but along the deflection axis; recall that deflection left is positive and right, negative.

6. PROGRAM SECTION III - EFFECTIVENESS SUBMODEL

6.1 The DAMAGE FUNCTION.

The damage functions generated by program sections I and II are not suitable for use by this program section because they are not normalized, because their various regions may not be nested in a manner which can be handled by this program section, and because they may represent only one half of a damage function. They are, however, a very convenient point of departure for the construction of usable damage functions.

There are three types of geometry which are allowed for the regions of the damage functions. They are identified as fully nested, unnested, and partially nested, and are exemplified in Figures 6-1, 6-2, and 6-3, respectively. With respect to Figure 6.3, note that the damage function must be considered as having seven regions rather than five. The .9 and .1 regions each must be divided into two regions at the range axis so that they can be represented by rectangles. There are no restrictions concerning how the probability of damage may vary from one region to the next; however, there is a rule concerning geometrical arrangement of regions. The rule is that any rectangular contour which causes nesting to occur must fully enclose all preceding contours, and each subsequent region of that damage function must completely enclose all regions preceding it. Once the geometry of the final damage function has been determined, it must be normalized. That is, the lethal area and damage area for any region of the rectangularized, normalized damage function must be the same as the sums of the lethal and damage areas, respectively, over the elements of the probability of damage matrix which were combined to obtain that region. It should be clear that a probability of damage matrix or, more conveniently, an unnormalized damage function from program section I or II, can result in more than one damage function as used by section III. Furthermore, the choice of the damage function's final form is a matter of judgement.

To illustrate the generation of fully nested damage functions, we first obtain from the unnormalized damage function of Figure 4-8 what is commonly called a "cookie cutter" damage function. Such a damage function consists of one region with some constant probability of damage, and the entire exterior region has zero probability of damage. The total lethal and damage areas are 18.588 and 28.738 square meters, respectively, so the average probability of damage (abbreviated PD) is .65. The only quantities remaining to be defined are the deflection to range ratio of the rectangle and the location of the rectangle's center with respect to the burst location. We choose the deflection to range ratio to be the same as it is for the PD = .354 region ($3.048/6.096 = .500$) and we choose the range coordinate of the cookie cutter's center to be the same as for the PD = .971 rectangle (.711 meters closer to the cannon than is the burst point). Because the target plate was horizontal and rectangular, the probability of damage matrix (Figure 4-7 shows the contour map) corresponds to a target enjoying reflection symmetry across the range axis, and so the lethal area, damage area, and deflection to range ratio must be doubled and the deflection coordinate of the cookie cutter's center must be set to zero.

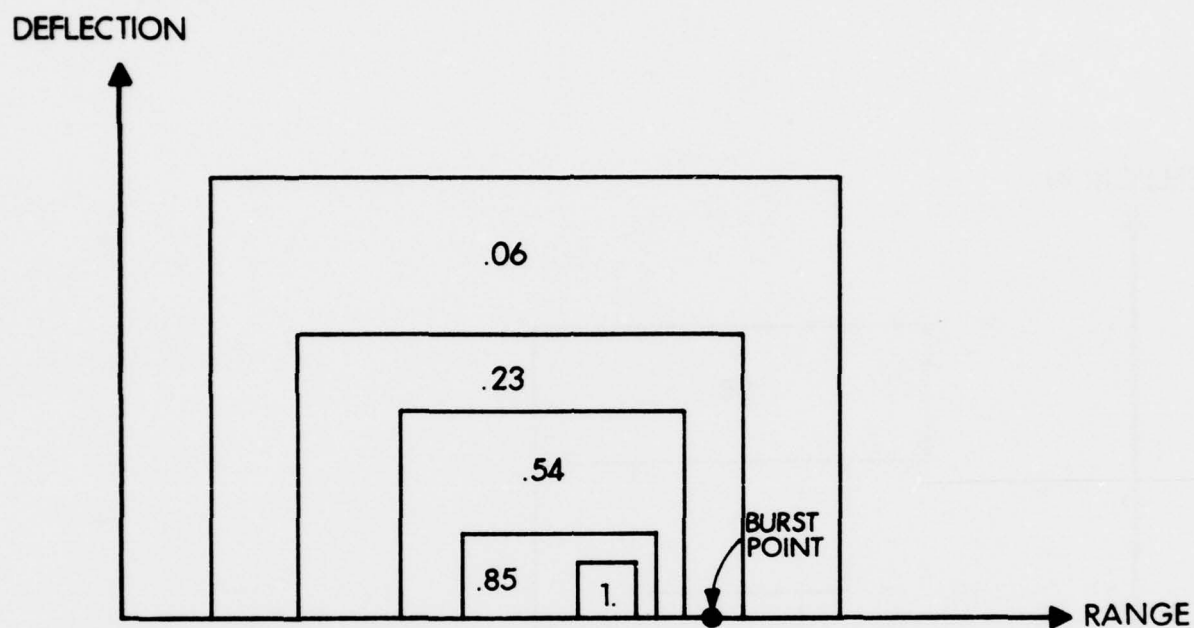


Figure 6-1. (U) One Half of a Fully Nested Normalized Damage Function Enjoying Reflection Symmetry Across the Range Axis.

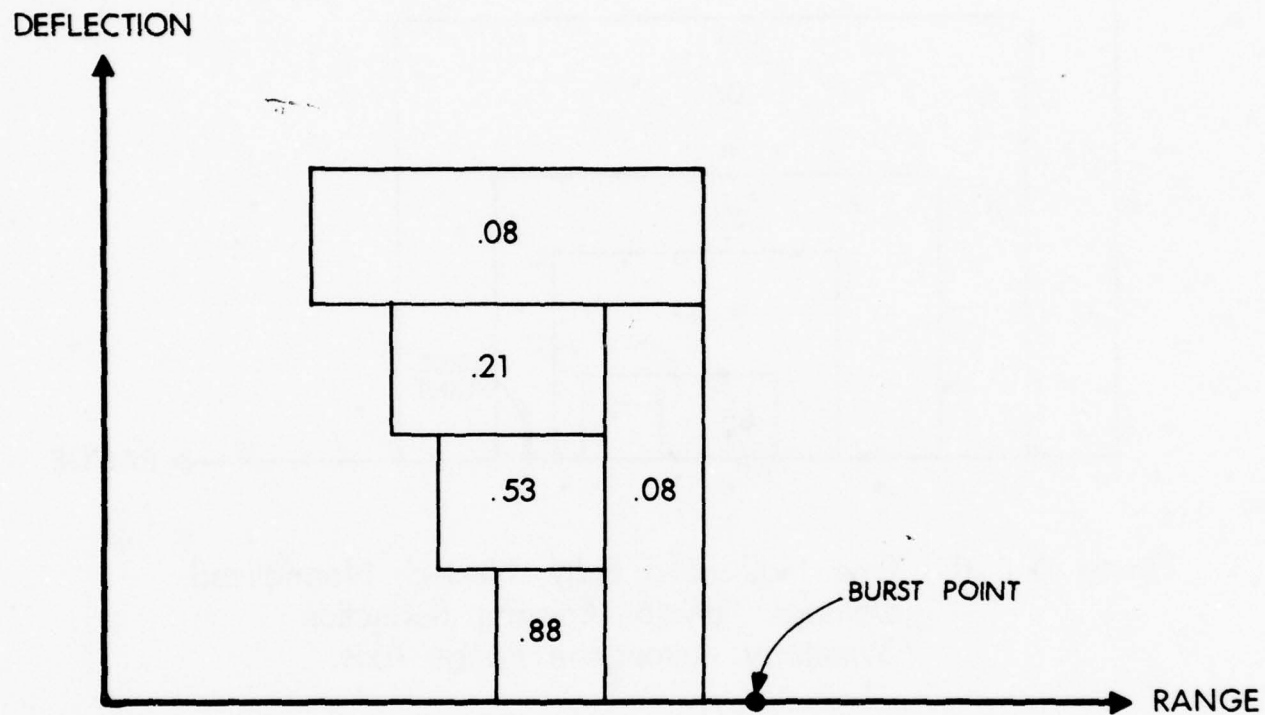


Figure 6-2. (U) One Half of an Unnested Normalized Damage Function Enjoying Reflection Symmetry Across the Range Axis.

DEFLECTION

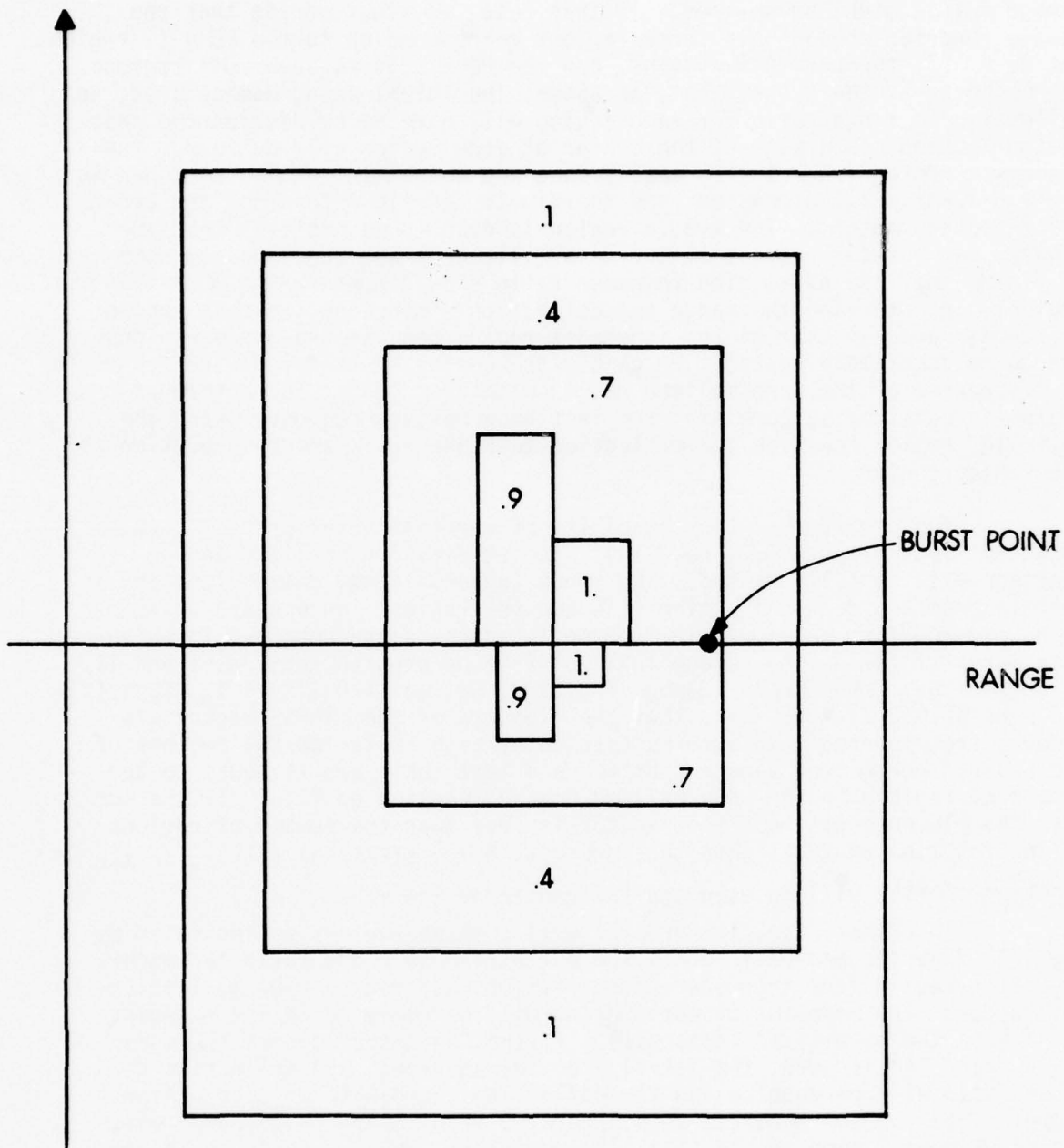


Figure 6-3. (U) A Complete Partially Nested Normalized Damage Function, Assymmetric Across the Range Axis.

A damage function more closely approximating the probability of damage matrix might be desired. In this case, we might decide that the damage function should have three regions corresponding to the PD = 1. region, the PD = .971 through .449 regions, and the PD = .354 through .041 regions. We recognize at the outset that, as above, the lethal area, damage area, and deflection to range ratio for each region will have to be doubled and that the deflection coordinate of the center of each region will be zero. The innermost region (PD = 1.) is easily done and we obtain results as shown in Table 6-1, where all dimensions and coordinates are in meters and the areas are in square meters. The middle region is done in essentially the same manner, but now six regions of the unnormalized damage function are combined. We decide that the deflection to range ratio should be from the PD = .551 region. In obtaining the range and deflection dimensions, we must augment the damage area by that of the innermost region because the three regions are to be completely nested. We choose the center of the middle region to be at the center of the unnormalized region with PD = .848. The outermost region is obtained by combining the last unnormalized regions, using the PD = .146 region for both the deflection to range ratio and the location of the region center.

The program has the capability of performing the preceding computations (paragraph 6.4.2, card 14). The resulting normalized damage function will be fully nested. The input (unnormalized) damage function is read in from the damage function file and the regions thereon are assumed to be ordered from outermost to innermost, which is the sequence in which they were written on the damage function file by program sections I and II. To obtain the three region damage function, we use STEPS2(1) = 1., STEPS2(2) = 6., and STEPS2(3) = 4. Note that the elements of the STEPS2 vector are ordered from innermost to outermost (usually high PD to low PD) regions of the desired normalized damage function and that their sum is equal to the number of regions in the unnormalized damage function on file. If the sum over the elements of the STEPS2 vector is less than the number of regions in the function on file, then the innermost $N = \sum J \text{ STEPS2}(J)$ regions in the function on file will be used and the remainder ignored.

In either case, the program will combine regions as indicated by the STEPS2 vector and will obtain the deflection to range ratio for each resulting region from the outer boundaries of that region. Normalization will occur. The midpoint of each region will be computed as the midpoint of each of the normalized rectangles. If the "symmetry" option (paragraph 6.4.2, card 14) is used, the lethal area, damage area, and deflection to range ratio will be doubled and the deflection coordinate of each region's midpoint will be set equal to zero. Working from innermost to outermost, the program will compare the $(i + 1)^{\text{th}}$ region to the i^{th} region to insure that all regions are nested. If the $(i + 1)^{\text{th}}$ rectangle cannot enclose the i^{th} rectangle because of shape, the shape of the $(i + 1)^{\text{th}}$ rectangle will be altered just enough, maintaining normalization, to allow it to enclose the i^{th} rectangle. Also, if the $(i + 1)^{\text{th}}$ rectangle must be shifted to enclose the i^{th} rectangle, the $(i + 1)^{\text{th}}$ midpoint will be shifted just enough for nesting to occur.

TABLE 6-1. A FULLY NESTED DAMAGE FUNCTION

Region	Lethal Area	Damage Area	Cumulative Damage Area	Prob of Damage	Deflection to Range Ratio	Normalized Range Dimension	Normalized Deflection Dimension	Coordinates of Region Center With Respect to Projectile
Innermost	14.286	14.286	14.286	1.000	.952	3.874	3.688	(-.711,0.)
Middle	20.270	25.270	39.556	.802	1.200	5.741	6.890	(-.610,0.)
Outermost	2.620	17.920	57.476	.146	1.096	7.242	7.936	(-.102,0.)

For unnested damage functions, and for the unnested part of a partially nested damage function, the procedure is similar, but less complicated simply because we need not be concerned about nesting. However, the program has no capability to generate such damage functions.

In any event, the program reflects the complete damage function in its final form through the projectile burst point. This transforms the function from one describing the damage sustained by a target for every location of that target about the burst point into a function describing the damage sustained by a target due to a projectile burst at any point about that target, with constant HOB.

6.2 The Program.

This section of the program uses the methodology of reference 4, with some changes in the computer program to increase flexibility and delete unneeded portions, to compute the probability that each target in a group of several similar targets is damaged. This probability is stored internally as an element of a 3-dimensional matrix, henceforth called the S matrix. The three subscripts of these matrix elements identify the target element sustaining damage, the size of the volley which caused the damage, and the HOB of all projectiles in the volley.

Essentially, the S matrix is computed as follows. The specified number of projectiles is fired at the selected aim points; proper launch is assumed. Round-to-round and occasion-to-occasion error (assumed normal) and projectile functioning reliability (binomial) distributions are applied to the projectiles. HOB is constant. A distribution of burst points over the specified target array is obtained. The burst point distribution and the damage function representing the target element are combined and integrated over the ground plane. The result is one element of the S matrix. Results are obtained for each volley size, each target in the target array, and each HOB (each HOB has its own damage function) to obtain all elements of the S matrix.

Elements of the S matrix can be averaged over any specified HOB distribution (so long as the distribution includes only HOB's for which there are elements) to obtain a two-dimensional S' matrix. The two subscripts of these matrix elements identify the target element sustaining damage and the size of the volley causing the damage.

Optimization can be performed upon the S matrix for a specified volley size to determine which HOB causes the most damage. This HOB is then treated as an HOB distribution with standard deviation equal to zero to obtain an S' matrix. The optimization consists of summing the S matrix elements over the various targets for each HOB at the specified volley size. The HOB yielding the largest sum is defined as optimum for that volley size.

From the S' matrix are obtained, for each volley size specified, the probabilities that various numbers of targets in the target array sustain damage, the average probability (averaged over the target elements)

that some target element sustains damage, and the most and least damageable target elements with the probability that they sustain damage.

Consider the plane of elements in the S matrix corresponding to one target element. Each such plane is generated by a machine computation which can be time consuming. Under certain conditions, the number of such planes to be computed can be halved and the remainder obtained through an appeal to reflection symmetry. The conditions are that the damage functions for all specified HOB's, the aim point array, and the target array enjoy reflection symmetry across the range axis. Note that, apart from being common to both the aim points and the target elements, the Cartesian coordinate system used is arbitrary and its origin may be chosen in any convenient manner.

When these conditions are satisfied, the complete aim point array is input, but only one of the two symmetric halves of the target array is input, and the SYMMETRIC ARRAY option of input data cards 16 and 19 through 21 (Figure 6-4) is used. This allows the use of a target array containing twice as many target elements (50) as can be input (25), and results in some economy of machine time.

6.3 Output.

The input data are printed out. The S and S' matrices are printed out. Depending upon the number of targets in the target array, such of the following as apply are printed out for all specified volley sizes at the specified HOB distribution (the optimum HOB, if computed, being considered as an HOB distribution with zero standard deviation). These and the S' matrix are printed out only when requested by the appropriate cards 16 through 21 (see paragraph 6.4.2), whereas the S matrix is always printed out.

- a. Probability that no targets are damaged.
- b. Probability that exactly one target is damaged.
- c. Probability that exactly two targets are damaged.
- d. Probability that at least one target is damaged.
- e. Probability that at least two targets are damaged.
- f. Probability that at least three targets are damaged.
- g. Probability that less than two targets are damaged.
- h. Probability that less than three targets are damaged.
- i. Average probability that a target is damaged.
- j. Probability that the most vulnerable target is damaged.
- k. Probability that the least vulnerable target is damaged.

6.4 Input Data Deck.

This deck inputs a batch of cases. Data cards 1 through 15 provide data used by all cases in the batch. These data include the number of cannon and their aim points, the number of targets in the target array and their locations, the number of rounds fired by each cannon for each of the volley sizes, ballistic data, functioning reliability, and damage functions for each of as many as 25 HOB's. Data cards 16 through 18 or cards 19 or 20 or 21 define a specific case within the batch. As many cases as desired may be run within one batch. A case now means a specific HOB distribution consisting of some or all of the HOB's for which damage functions were input.

Unless otherwise stated, each data field is 10 columns wide, and each numeric datum is in a real format with an explicit decimal point. Data fields not specifically addressed are ignored and may be used for any desired purpose.

6.4.1 The Data Deck. The data deck for program section III is at Figure 6-4.

6.4.2 Definition of Each Input Variable.

Card 1:

Columns 1-10 - the word ENCOUNTER

- N - the number of cannon to fire; $1. \leq N \leq 100$.
- NVEH - the number of targets in the target array to be fired upon; $1. \leq NVEH \leq 25$; see card 16, columns 31-40.
- NVS - the number of volley sizes to be solved; $1. \leq NVS \leq 25$.
- NHTS - the number of HOB's, and hence, the number of damage functions to be solved; $1. \leq NHTS \leq 25$.
- U1 - the number of increments for the range and deflection integrals over a quarter of the integration plane; usually, $U1 \geq 8$.

Cards 2 and 3:

A(I), B(I) - the range and deflection coordinates, respectively, of the aiming point for the Ith cannon; in meters; recall that deflection left is positive and right, negative.

There may be as many as 13 cards for the A's and the same number for the B's to allow the input of N values of A and B.

Card 4:

An optional card; has the words SAME CANNO in columns 1-10. If present, cards 2 and 3 must be absent. Causes the aiming points of the immediately preceding section III data deck to be used.

COLUMN	11111111112222222222333333333344444444445555556666667777777778
NUMBER	123456789012345678901234567890123456789012345678901234567890
CARD	
NUMBER	
1	ENCOUNTER N NVEH NVS NHTS U1
2	A(1) A(2) A(3) ...
	*** UP TO 12 MORE CARDS, AS NEEDED, FOR UP TO 100 VALUES OF A ***
3	B(1) B(2) B(3) ...
	*** UP TO 12 MORE CARDS, AS NEEDED, FOR UP TO 100 VALUES OF B ***
4	SAME CANNON
5	VOSR(1) VOSR(2) VOSR(3) ...
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF VOSR ***
6	VOSD(1) VOSD(2) VOSD(3) ...
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF VOSD ***
7	SAME TARGETS
8	NN(1) NN(2) NN(3) ...
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF NN ***
9	SAME VOLLEYS
10	S2 T1 T2 R
11	SAME ERRORS
12	HT(1) NUMB(1) NUMN(1)
13	XSSP(I,J) X8B3(I,J) X8B4(I,J) XROSE(I,J)XDOSE(I,J)
	*** AS MANY AS 12 MORE CARDS, AS NEEDED, FOR UP TO
	13 SETS OF THE ABOVE 5 VARIABLES, INDEXED ON J ***
14	*** THE ABOVE 2 TO 14 CARDS FORM A SET DEFINING 1 DAMAGE FUNCTION ***
	*****SYMMETRY FILE2ST(1)ST(2)ST(3)...
	*** THE ABOVE CARD DEFINES A DAMAGE FUNCTION TO
	BE EXTRACTED FROM THE DAMAGE FUNCTION FILE ***
	*** ADDITIONAL CARDS AND/OR CARD SETS, AS NEEDED, TO DEFINE A TOTAL
	OF AS MANY AS 25 DAMAGE FUNCTIONS, EACH FOR A DIFFERENT HT(I) ***
15	SAME DAMAGE FUNCTION
16	HOB DISTRIBUTION NHOB SYMMETRIC ARRAY OPTIMIZE L
17	HOB(1) HOB(2) HOB(3) ...
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF HOB ***
18	DF(1) DF(2) DF(3) ...
	*** UP TO 3 MORE CARDS, AS NEEDED, FOR UP TO 25 VALUES OF DF ***
19	ALL HOB
20	SAME HOB DISTRIBUTION SYMMETRIC ARRAY OPTIMIZE L
21	OPTIMIZE L SYMMETRIC ARRAY OPTIMIZE L

FIGURE 6-4. DATA DECK FOR PROGRAM SECTION III

Cards 5 and 6:

VOSR(I), VOSD(I) - the range and deflection coordinates, respectively, of the Ith target in the target array; in meters; recall that deflection left is positive and right, negative.

There may be as many as four cards for the VOSR's and the same number for the VOSD's to allow for the input of NVEH values of VOSR and VOSD. See card 16, columns 31-40.

Card 7:

An optional card; has the words SAME TARGE in columns 1-10. If present, cards 5 and 6 must be absent. Causes the target locations of the immediately preceding section III data deck to be used.

Card 8:

NN(I) - the number of rounds to be fired by each cannon in the Ith volley size to be solved.

There may be as many as four cards for the NN's to allow for the input of NVS volley sizes.

Card 9:

An optional card; has the words SAME VOLLE in columns 1-10; if present, card 8 must be absent. Causes the volley sizes of the immediately preceding section III data deck to be used.

Card 10:

S1, S2 - precision errors; the range and deflection standard deviations of the distribution of one cannon's burst points at one HOB on one occasion about their own mean; in meters.

T1, T2 - mean point of impact (MPI) errors; the range and deflection standard deviations of the distribution of one cannon's single occasion mean burst points at one HOB about their own mean; in meters.

R - the complete round functioning reliability, given proper launch.

Card 11:

An optional card. If present, card 10 must be absent; has the words SAME ERROR in columns 1-10. Causes S1, S2, T1, T2 and R from the immediately preceding section III data deck to be used.

Card 12:

Cards 12 and 13 define one damage function in final form. There must be NHTS sets of cards 12 and 13. These sets need not be in any particular order.

- HT(I) - the HOB to which the I^{th} damage function applies; any two elements must differ from each other by at least .1% of their sum; in meters.
- NUMB(I) - the number of regions in the I^{th} damage function; $1 \leq \text{NUMB}(I) \leq 13$.
- NUMNN(I) - the number of unnested regions in the I^{th} damage function; $0 \leq \text{NUMNN}(I) \leq \text{NUMB}(I)$.

Card 13:

- XSSP(I,J) - the average probability of damage over the J^{th} region of the I^{th} damage function.
- XBB3(I,J), XBB4(I,J) - the range and deflection dimensions, respectively, of the J^{th} region of the I^{th} damage function; in meters.
- XROSE(I,J), XDOSE(I,J) - actually XROSET(I,J), XDOSET(I,J); the range and deflection offsets, respectively, of the center of the J^{th} region of the I^{th} damage function with respect to the target location; in meters.

There must be NUMB(I) cards 13 in the I^{th} set of cards 12 and 13. Their order must be from innermost to outermost damage function region. The order among themselves of those cards defining unnested regions is unimportant, but all such unnested cards must occur before any cards defining nested regions in the I^{th} set.

Card 14:

One card 14 replaces one set of cards 12 and 13. Any and any number of those card sets may be so replaced. Causes input of data from the damage function file, from which data the program will generate a fully nested damage function.

- Columns 1-10 - any alphanumeric character string which cannot be interpreted as a number.

- Columns 11-20 - if columns 11-20 contain the word SYMMETRY, the generated damage function will be assumed to be half of a damage function enjoying reflection symmetry across the range axis and it will be reflected across the range axis to produce a complete function. Lethal area and damage area will double. Otherwise, ignored.

- FILE2 - 5 column whole number; the unique logical record number identifying the desired data on the damage function file.
- ST(J) - 5 column whole number; actually STEPS2(J); one value for each region desired in the normalized fully nested damage function to be generated; each value indicates the adjacent regions of the unnormalized damage function on file which will be combined to arrive at the Jth region of the desired normalized damage function; the elements of this set must be ordered from innermost to outermost regions of the desired function; the sum of all the STEPS2(J) must not be greater than the number of regions in the function on file (not more than 11 regions); if the sum of all the STEPS2(J) is less than the number of regions in the function on file, then only the innermost $N = \sum J \text{ STEPS2}(J)$ regions of the damage function on file will be used; the first STEPS2(J) = 0. or blank terminates the vector. There is one exception to the preceding rules: if all the STEPS2(J) are 0. (or blank) then no regions on file will be combined: that is, the result is identical with the STEPS2 vector being all 1.'s and having as many elements as there are regions in the damage function on file.

Card 15:

An optional card. If present, all cards 12, 13, and 14 must be absent. The words SAME DAMAGE in columns 1-10 cause the entire set of normalized damage functions from the immediately preceding section III data deck to be used.

Card 16:

Cards 16, 17, 18 form a set defining one HOB distribution. There may be as many or as few such sets as desired, or none.

- Columns 1-10 - the words HOB DISTRI.
- NHOB - the number of HOB's in the distribution; $1. \leq \text{NHOB} \leq 25$.
- Columns 31-40 - the word SYMMETRIC; causes the target array to be reflected across the range axis, thus producing a new target array enjoying reflection symmetry across the range axis and having twice as many target elements as the array which was input; can be used only when the aim-points and the damage function are symmetric across the range axis; does not carry over from one case to the next or from one batch to the next; otherwise, ignored.

Columns 51-60 - the word OPTIMIZE; causes HOB optimization without prior use of an HOB distribution.

L - the number of rounds fired per cannon at which optimization will be performed; if L is not a member of the NN(I) vector, NN(1) will be used; ignored if columns 51-60 are ignored.

Cards 17 and 18:

HOB(I), DF(I) - the Ith HOB, and its weighting factor, respectively, for the current HOB distribution function; each HOB must be within .1% of an element of the HT(I) vector.

There may be as many as four cards 17 and four cards 18 to allow the input of NHOB values of HOB and corresponding values of DF.

Card 19:

Cards 19, 20, and 21 each perform a function equivalent to that of the set of cards 16, 17, and 18. As many or as few as desired may be used and they may be intermingled with each other and with the set of cards 16, 17, and 18, in any order desired (but not inside the set 16, 17, and 18), with the obvious restriction on card 20, that there must have been an immediately preceding case.

Columns 1-10 - the words, ALL HOB'S; causes the current HOB distribution to be a uniform distribution consisting of all HOB's in the set {HT}.

Columns 31-80 - same as card 16.

Card 20:

Columns 1-10 - the words, SAME HOB D; causes the current HOB distribution to be the same as in the immediately preceding case; the immediately preceding case can be the last case of the immediately preceding batch.

Columns 31-80 - same as card 16.

Card 21:

Columns 1-10 - the word, OPTIMIZE; causes HOB optimization without prior use of an HOB distribution.

L - same as card 16.

Columns 31-50 - same as card 16.

7. PROGRAM SECTION IV - PERFORATIONS; POSSIBILITY AND SIGNIFICANCE

7.1 The Program.

This program section provides two functions not directly related to those of program sections I, II, and III. It predicts, for an armor plate and a fragment distribution, whether perforations can ever occur except for direct hits and very near misses. If perforations can occur, it computes the average probability of incapacitation of a soldier protected against the fragment distribution by the armor plate, assuming that the soldier will be hit by the distribution of residual fragments. Once again, the methodology is that of Thor Reports 47 and 70 (references 1 and 2). Air drag is neglected. For those fragments which perforate, the residual mass and velocity are computed. For each perforating fragment, the methodology of reference 5 is used to obtain the probability of incapacitation of a soldier, given that he is hit by the residual fragment. This methodology is augmented by the computation of a V_{50} using the equations of reference 8. Correspondence of the naked soldier and the soldier wearing a helmet and winter uniform in reference 5 to the soldier wearing a summer uniform and the soldier wearing a winter uniform in reference 8, respectively, is assumed. These $P_{I/H}$'s are averaged over the distribution of perforating fragments to obtain the average $P_{I/H}$ per fragment for the soldier protected by the armor plate.

7.2 Output.

The input data are printed out. Computed output is shown in Figure 7-1.

7.3 Input Data Deck.

This data deck is identified by its first card which contains the words SECTION IV in columns 1-10. After this card are input any number of "batches" of cases. One batch is terminated by a card with the word COMPUTE in columns 1-10. One case is one armor plate or plate assembly at one obliquity angle. For any given batch, the input data are divided into six data card subsets, which are the fragmentation data, terminal velocity, Thor constants, angles, armor, and incapacitation constants subsets. These subsets may be presented in any order.

All six subsets must be present for the first batch, except that, if the desired fragmentation data are currently in storage from program section I (see paragraph 8), then the fragmentation data subset need not be present. For subsequent batches, only those data card subsets whose input data are to be changed need be present.

Unless otherwise stated, each data field is 10 columns wide, and each numeric datum is in a real format with an explicit decimal point. Data fields not specifically addressed are ignored and may be used for any desired purpose.

7.3.1 The Data Deck. The data deck for program section IV is at Figure 7-2.

AL 7039 1.25 INCHES THICK THETA = 0.0 DEGREES PROJECTILE VELOCITY = 915.00 FEET PER SECOND

SPRAY	V IMPACT	M IMPACT	V RESIDUAL	M RESIDUAL	PI/H
6	.4592E+04 (MAX)	.6370E+03	.9798E+02	.4415E+03	0.0000
8	.4594E+04 (MAX)	.1649E+04	.1481E+04	.1212E+04	.9991
8	.4055E+04 (MED)	.1649E+04	.8879E+03	.1304E+04	.9930
9	.4745E+04 (MAX)	.1352E+04	.1400E+04	.9588E+03	.9974
9	.4207E+04 (MED)	.1352E+04	.8043E+03	.1039E+04	.9840
9	.4745E+04 (MAX)	.9690E+03	.9405E+03	.6723E+03	.9765
9	.4207E+04 (MED)	.9690E+03	.3375E+03	.7331E+03	.8416
9	.4745E+04 (MAX)	.6605E+03	.3492E+03	.4503E+03	.7739
10	.4788E+04 (MAX)	.1535E+04	.1606E+04	.1090E+04	.9991
10	.4299E+04 (MED)	.1535E+04	.1069E+04	.1172E+04	.9955
10	.4788E+04 (MAX)	.9520E+03	.9622E+03	.6547E+03	.9768
10	.4299E+04 (MED)	.9520E+03	.4147E+03	.7098E+03	.8788
10	.4788E+04 (MAX)	.5437E+03	.3856E+02	.3565E+03	0.0000
11	.4385E+04 (MAX)	.3050E+04	.1914E+04	.2377E+04	1.0000
11	.3124E+04 (MED)	.3050E+04	.5336E+03	.2697E+04	.9924
11	.4385E+04 (MAX)	.2634E+04	.1770E+04	.2039E+04	1.0000
11	.3124E+04 (MED)	.2634E+04	.3828E+03	.2322E+04	.9714
11	.4385E+04 (MAX)	.2135E+04	.1549E+04	.1637E+04	.9998
11	.3124E+04 (MED)	.2135E+04	.1513E+03	.1874E+04	0.0000
11	.4385E+04 (MAX)	.1634E+04	.1241E+04	.1237E+04	.9979
11	.4385E+04 (MAX)	.1525E+04	.1156E+04	.1150E+04	.9965
11	.4385E+04 (MAX)	.8444E+03	.2266E+03	.6171E+03	.8095

MEAN PI/H = .7698E+00

FIGURE 7-1. SAMPLE OUTPUT OF PROGRAM SECTION IV

COLUMN NUMBER	11111111112222222222333333333344444444445555555555666666666677777777778
CARD NUMBER	1234567890123456789012345678901234567890123456789012345678901234567890


```

SECTION IV
*** THE FOLLOWING CARDS DEFINE ONE BATCH OF CASES
THE VARIOUS CARD SETS MAY OCCUR IN ANY ORDER ***
*** CARD SET A ***
*** THIS SET OF CARDS IS IDENTICAL WITH CARLS .1 THRU 14 OF FIGURE 4-9 ***
*** CARD SET B ***
TERMINAL VELOCITY VTERM *** CARD SET C ***
THOR DATA NTHOR
METAL(I) CV(I) ALFAV(I) BETAV(I) GAMAV(I) LAMDAV(I) KFCTRV(I)
CM(I) ALFAM(I) BETAM(I) GAMAM(I) LAMDAM(I) KFCTRM(I)
*** UP TO 19 MORE PAIRS OF CARDS C2 AND C3, AS
NEEDED, FOR AS MANY AS 20 SETS OF THOR DATA ***
*** CARD SET D ***
D ANGLES NTHETA THETA(1) THETA(2) ***
*** UP TO 2 MORE CARDS, AS NEEDED, FOR AS MANY AS 20 VALUES OF THETA ***
*** CARD SET E ***
E1 ARMOR NPLATE
E2 PLATE(1) T(1) PLATE(2) T(2) ***
*** UP TO 4 MORE CARDS, AS NEEDED, FOR UP TO 20 PLATES ***
*** CARD SET F ***
F INCAPACITATION PARAMETERS SUMMER COEF1 COEF2 COEF3
*** LAST CARD OF THE BATCH ***
LAST COMPUTE

```

FIGURE 7-2. DATA DECK FOR PROGRAM SECTION IV

7.3.2 Definition of Each Input Variable.

Card 1:

Columns 1-10 - the words SECTION IV.

The following card sets define a batch of cases. The card sets may appear in any order. The batch is terminated by a COMPUTE card. As many batches as desired may follow the SECTION IV card.

Card set A:

This card set inputs the fragmentation data and is identical with cards 11 through 14 of paragraph 4.3.2.

Card set B:

Columns 1-10 - the words TERMINAL V.

VTERM - the projectile terminal velocity in feet per second.

Card set C:

This card set inputs as many as 20 sets of Thor constants from which are drawn the appropriate sets for the various armor plates or armor plate assemblies in this batch.

Card C1:

Columns 1-10 - the words THOR DATA.

NTHOR - the number of sets of Thor constants; $1. \leq \text{NTHOR} \leq 20$.

Cards C2 and C3:

This card pair defines one set of Thor constants. The cards are identical with cards 8 and 9 of paragraph 4.3.2. There must be NTHOR such card pairs.

Card set D:

Columns 1-10 - the word ANGLES.

NTHETA - the number of obliquity angles to be considered for each armor plate or plate assembly; $1. \leq \text{NTHETA} \leq 20$.

THETA(I) - the I^{th} obliquity angle to be considered for each armor plate or plate assembly; in degrees; there must be NTHETA such angles; $0.^\circ \leq \text{THETA} \leq 90^\circ$.

Card set E:

This card set defines the armor plates processed in this batch.

Card E1:

Columns 1-10 - the word ARMOR.

NPLATE - the number of plates.

Card E2:

This card defines an armor plate. Exactly NPLATE such plates must be defined.

PLATE(I) - 10 alphanumeric characters; specifies the material of which the I^{th} plate is made; must match, character by character, one of the variables METAL(K) from card set C.

T(I) - the thickness, in inches, of the I^{th} plate.

Card set F:

This card set defines the incapacitation parameters used in computing $P_{I/H}$.

Columns 1-10 - the word INCAPACITA.

Columns 31-40 - the word SUMMER or the word WINTER; describes the type of uniform being worn.

COEF1, COEF2, COEF3 - three constants used to compute $P_{I/H}$ for the selected kill criterion (see reference 5 and appendix B).

Last card of any batch:

Columns 1-10 - the word COMPUTE.

8. THE COMPLETE JOB DECK

8.1 The Data Deck.

Thus far, the four sections of the program and their data decks (herein called subdecks) have been discussed separately. In an actual machine run, any number of each of the four types of data subdecks may be stacked in any order desired, so long as one insures that, when a subdeck is processed, it will not demand information produced by some later subdeck.

Each type of subdeck has certain options allowing the use of data read in from a preceding subdeck of the same type. An important constraint upon the complete data deck is that each of the four program sections destroys the input data belonging to any previous different program section, with one exception, which is discussed below.

Program sections I and IV do not destroy each other's static fragmentation data. That is, either of these program sections can use static fragmentation data read in by itself or by the other and will leave that data ready to be used again by itself or by the other. Any time either of these program sections reads in such data, it replaces the fragmentation data previously read in by either section.

A complete data deck must contain at its end either of two cards not heretofore discussed.

One of these is a card with the words END OF DAT in columns 1 through 10. This card terminates the data deck. Succeeding cards are ignored.

The other card can have any of the forms shown in Figure 8-1. Only columns 1-10 and 41-50 are read; other columns are ignored. These cards cause termination of the run immediately after completion of the specified operations.

EXPECTED P causes an index of the expected perforations matrix file to be printed. An example is at Figure C-13. The column headings have the following meanings:

FILES is the unique integer identifying an expected perforations matrix; used as an element of the set FILE (paragraph 5.4.2, card 5).

NXX, NYY are as in paragraph 4.3.2, card 1.

CELL is the edge length of the cell with which the ground plane is gridded, in inches.

HOB is the height of burst above the ground, in meters.

IROW, ICOL are as in paragraph 4.3.2, card 1.

```

EXPECTED PERFORATIONS FILE      DAMAGE FUNCTION FILE
DAMAGE FUNCTION FILE            EXPECTED PERFORATIONS FILE
EXPECTED PERFORATIONS FILE      DAMAGE FUNCTION FILE
DAMAGE FUNCTION FILE            EXPECTED PERFORATIONS FILE

```

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LYMYB, LYMYT, LYMXL, LYMXR are the row and column numbers which define the minimum and maximum deflection and range limits, respectively, of the non-zero portion of the expected perforations matrix. If the matrix is all zeroes, then these numbers merely define a small region about the projectile.

A, B, NSIDE, NX, NY, NZ, T are elements of the sets ALPHA, BETA, NSIDE, NXTGT, NYTGT, NZTGT, and TT, respectively (paragraph 4.3.2, card 5).

THCK is an element of the set TTHCK (paragraph 4.3.2, card 3).

DAMAGE FUN causes the contents of the damage function file to be printed. An example is at Figure C-14. The column headings have the following meanings:

FILE NUMBER is the unique integer identifying a damage function; used as FILE2 (paragraph 6.4.2, card 14).

POINT NUMBER identifies the I^{th} case of a batch of cases from program section II.

SYMMETRY CHARACTER is KSYM (paragraph 6.4.2, card 1).

DAMAGE CRITERION is the number of perforations defined as the damage criterion.

LYMXL, LYMXR, LYMYB, LYMYT are as above.

PROJECTILE LOCATION is the range, deflection coordinate pair of the burst point with respect to the probability of damage function.

HOB is the height of burst above the ground, in meters.

CELL is as above.

NUMBER OF REGIONS is the number of different valued probability of damage regions in the probability of damage function.

THE DAMAGE FUNCTION REGIONS data completely defines the unnormalized damage function.

8.2 The Control Deck.

Certain control cards are needed to cause problem loading and execution and to insure availability and permanence of files. Depending on the situation, these functions can be accomplished in any number of

ways, and hence will not be discussed in detail. The control decks used to produce the example of Appendix C are presented and explained in Appendix D. One point, however, is worthy of note. On several figures providing examples of output in the body of the report and in Appendix C, the names assigned by the user to his perforation matrix and damage function files appear. These names are made available to the program by the control deck. Note from Appendix A that the first FORTRAN statement in the program is:

```
PROGRAM LASVEM (INPUT, OUTPUT, TAPE1, TAPE2,...)
```

where:

```
INPUT is the system input file.  
OUTPUT is the system output file.  
TAPE1 is the perforation matrix file.  
TAPE2 is the damage function file.
```

The user's local file names for the perforation matrix file and the damage function file must be equivalenced, by appropriate commands, to TAPE1 and TAPE2, respectively.

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APPENDIX A
PROGRAM TABULATION

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```

C AND DIMY ARE PROGRAMMER ORIENTED AND SERVE AS ACHIEVABLE UPPER
C BOUNDS FOR NXX AND NYX.
C
C TAPE=1
C TAPE=2
C TAPE=10
C TAPE IS THE PERFORATION MATRIX FILE.
C TAPE IS A SCRATCH FILE.
C PTAPE1 IS A SCRATCH FILE.
C PROGRAM LOGIC ORIGINALLY ASSUMED SEQUENTIAL FILES ON TAPE. MINIMAL LASV121
C LOGIC CHANGES HAVE BEEN MADE TO GET ON THE CDC MACHINE. THEREFORE, LASV122
C RECORDS WITHIN A LOGICAL INPUT DATA SET ARE STILL GENERATED LASV123
C SEQUENTIALLY, EVEN THOUGH THEY ARE STORED AND ACCESSED RANDOMLY. LASV124
C THAT SET OF RECORDS CAN BE LOCATED, AS A SET, ANYWHERE WITHIN THE LASV125
C FILE. WITHIN THE SET, LOGICAL RECORDS ARE IN SEQUENCE. THIS LASV126
C APPLIES TO BOTH DAMAGE FUNCTIONS AND PERFORATION MATRICES. PTAPE1 LASV127
C IS STILL A SEQUENTIAL FILE. LASV128
C CALL OPENMS (TAPE,PLIST,2502,0) LASV129
C CALL OPENMS (TAPE,SLIST,5002,0) LASV130
C DO 10 I=1,2502 LASV131
C IF (PLIST(I),1,NE.0) GO TO 20 LASV132
C 10 CONTINUE LASV133
C GO TO 30 LASV134
C 20 CALL READMS (TAPE,PLIST(I,2),2501,2501) LASV135
C 30 DO 40 I=1,5002 LASV136
C IF (SLIST(I),1,NE.0) GO TO 50 LASV137
C 40 CONTINUE LASV138
C GO TO 60 LASV139
C 50 CALL READMS (TAPE,SLIST(I,2),5001,5001) LASV140
C 60 CALL FILNAM (TNAME,SNAME) LASV141
C
C PI=3.1415926536 LASV142
C TWOPI=2.*PI LASV143
C HALFPI=PI/2. LASV144
C MTOT=3.28083 LASV145
C FTOT=1./MTOT LASV146
C RTODG=37.2957795131 LASV147
C DGTOR=1./RTODG LASV148
C ENAT=2.71828182846 LASV149
C VCID2=0 LASV150
C
C 70 READ (5,1090) (AAA(I),I=1,e) LASV151
C IF (AAA(1).EQ.1)CHASSEMBLE .OR.AAA(1).EQ.1CH ASSEMBLE .OR.AAA(1).EQ.1CH LASV152
C 10.1CH ASSEMBLE) GO TO 520 LASV153
C 80 IF (AAA(1).EQ.1)CHEXPECTED P.OR.AAA(1).EQ.1CHDAMAGE FUN) CALL INDEXLASV154
C 1 (0) LASV155
C IF (AAA(1).NE.1)CHENCOUNTER .AND.AAA(1).NE.1CH ENCOUNTER) GO TO 90 LASV156
C CALL SNOW LASV157
C GO TO 70 LASV158
C 90 IF (AAA(1).NE.1)CHSECTION IV) GO TO 100 LASV159
C CALL SEXUN4 LASV160
C GO TO 70 LASV161
C 100 IF (AAA(1).EQ.1)CHEND OF DAT) GO TO 110 LASV162
C IF (AAA(1).EQ.1)CHBASIC DATA) GO TO 120 LASV163
C WRITE (6,1350) (AAA(I),I=1,8) LASV164
C 110 CALL WRITMS (TAPE,PLIST(I,2),2501,2501,-1,0) LASV165
C CALL WRITMS (TAPE,SLIST(I,2),5001,5001,-1,0) LASV166
C CALL CLCDSMS (TAPE) LASV167
C CALL CLCDSMS (TAPE) LASV168
C WRITE (6,1360) LASV169
C STOP LASV170

```

```

C THIS PART OF MAIN COMPUTES THE PERFORATIONS SUSTAINED BY COMPONENTS
C PLATES OF THE TARGET
C
C 120 KSYM=0
C METPHODOLOGY DATA
C THIS LOGICAL DATA DECK GENERATES SEQUENTIALLY A SET OF PERFORATION TABLES
C MATRICES WHICH WILL BE STORED SEQUENTIALLY IN A RANDOM ACCESS FILE
C (TAPE=TAPE1-1). THE INPUT VALUE OF FILES IS THE KEY FOR THE 1ST
C LOGICAL RECORD (MATRIX) IN THE SET. THE FILE INFORMATION TABLE
C (PLIST) ALLOWS NOT MORE THAN 2500 LOGICAL RECORDS WITH KEYS 1 THRU 5000.
C 2500. SIMILARLY, DAMAGE FUNCTIONS ARE GENERATED SEQUENTIALLY
C WITHIN A SET RANDOMLY LOCATED ON A RANDOM ACCESS FILE (STAPE=TAPE2LASV193
C *2). THE FILE INFORMATION TABLE (SLIST) ALLOWS NOT MORE THAN 5000
C LOGICAL RECORDS WITH KEYS 1 THRU 5000. THE INPUT VALUE OF NSTAPE
C IS THE KEY FOR THE 1ST LOGICAL RECORD (DAMAGE FUNCTION) IN THE SET
C DECODE (6C,110,AAA(2)) FILES,CELL,FNXX,FNY,FICOL,FIROM
C FILES=FILES+.1
C NX=FNXX+.1
C NY=FNY+.1
C ICOL=FICOL+SIGN(.1,FICOL)
C FIROM=FIROM+SIGN(.1,FIROM)
C IRGW=IRGW
C ICOL=ICOL
C IF (FILES.GT.0) GO TO 150
C DO 130 I=1,2500
C J=2501-I
C IF (PLIST(J,2).NE.0) GO TO 140
C 130 CONTINUE
C J=0
C 140 FILES=J+.1
C TARGET DATA
C 150 READ (5,111C) FNHOB,(HHHOB(I),I=1,7)
C FNHOB=FNHOB+.1
C IF (FNHOB.GT.7) READ (5,111C) (HHHOB(I),I=6,NHCS)
C READ (5,111C) FNTHCK,(TTTHCK(I),I=1,7)
C FNTHCK=FNTHCK+.1
C IF (FNTHCK.GT.7) READ (5,111C) (TTTHCK(I),I=6,NTHCK)
C READ (5,111C) FNTRGT
C FNTRGT=FNTRGT+.1
C READ (5,111C) (FNXTGT(I),FNXTGT(I),FNXTGT(I),FNXTGT(I),ALPHA(I),
C 1 BETA(I),TT(I),SCALE(I),FSHOW(I),I=1,NTRGT)
C DO 160 I=1,NTRGT
C NATGT(I)=FNXTGT(I)+.1
C NYTGT(I)=FNXTGT(I)+.1
C NZTGT(I)=FNXTGT(I)+.1
C NSIDE(I)=FNXTGT(I)+.1
C 160 SHOW(I)=FSHOW(I)+.1
C SCALE IS A FACTOR USED TO ADJUST FOR SLIGHT MISMATCH IN SURFACE
C AREA BETWEEN THE ACTUAL AND MODEL PLATES. EFFECTIVE ONLY ON THE
C FRAGMENT CONTRIBUTIONS TO THE PERFORATION MATRICES.
C SCALE1 = INPUT PLATE SURFACE AREA / TRUE PLATE SURFACE AREA
C READ (5,111C) FNKRIT,(FNKRIT(I),I=1,NKRIT)
C FNKRIT=FNKRIT+.1
C 170 I=1,NKRIT
C FNKRIT(I)=FNKRIT(I)+.1
C THE FNKRIT ARRAY MUST BE MONOTONE INCREASING
C READ (5,111C) (ZAA(I),I=1,6)
C PHYSICAL CONSTANTS OF THE PLATE
C IF (ZAA(I).NE.1)CTHUR DATA .AND. AAA(I).NE.1CM THCK DATA) GO TO 18CLASV240

```

```

LASV161 00190C
LASV182 00191C
LASV183 00192C
LASV184 00193C
LASV185 00194C
LASV186 00195C
LASV187 00196C
LASV188 00197C
LASV189 00198C
LASV190 00199C
LASV191 00200C
LASV192 00201C
LASV193 00202C
LASV194 00203C
LASV195 00204C
LASV196 00205C
LASV197* 00206C
LASV198 00207C
LASV199 00208C
LASV200 00209C
LASV201 00210C
LASV202 00211C
LASV203 00212C
LASV204 00213C
LASV205 00214C
LASV206 00215C
LASV207 00216C
LASV208 00217C
LASV209 00218C
LASV210 00219C
LASV211 00220C
LASV212 00221C
LASV213 00222C
LASV214 00223C
LASV215 00224C
LASV216 00225C
LASV217 00226C
LASV218 00227C
LASV219 00228C
LASV220 00229C
LASV221 00230C
LASV222 00231C
LASV223 00232C
LASV224 00233C
LASV225 00234C
LASV226 00235C
LASV227 00236C
LASV228 00237C
LASV229 00238C
LASV230 00239C
LASV231 00240C
LASV232 00241C
LASV233 00242C
LASV234 00243C
LASV235 00244C
LASV236 00245C
LASV237 00246C
LASV238 00247C
LASV239 00248C
LASV240 00249C

```

```

C
READ (5,1120) METAL,CV,ALFAM,BETAV,GAMAV,LAMDAV,KFCTRV
READ (5,1110) CM,CH,ALFAM,BETAM,GAMAM,LAMDAM,KFCTRM
FROM THUR 76, KFCTRM(2024)=.964 AND KFCTRV(2024)=.965
RATIOH=0.
RATIOV=C.
IF (KFCTRM.NE.0.) RATIOH=ALOG10(KFCTRM/.964)
IF (KFCTRV.NE.0.) RATIOV=ALOG10(KFCTRV/.965)
SAVE1=GAMAM
SAVE2=GAMAV
SAVE3=LAMDAM
READ (5,1090) (AAA(I),I=1,8)
GO TO 190

180 GAMAM=SAVE1
GAMAV=SAVE2
LAMDAM=SAVE3
PROJECTILE LOCATION IS SHELX, SHELX
190 SHELX=FLOAT(ICOL)+.5
SHELX=FLOAT(IRGW)+.5
CELL=CELL/12.
PROJECTILE DATA
DECODE (30,1110,AAA(1))M,VTERM,BLAST
READ (5,1090) (AAA(I),I=1,8)
IF (AAA(1).NE.10HFRAGMENTAT) GO TO 200
FRGFLG=0
CALL FRAG1 (1H1)
EPSLN=2.*BLAST/CELL1
EPSLN IS IN HALF-CELLS
CNST1=-AA*CELL/2.*ALOG10(ENAT)
TEMP3=2.*ALOG10(SHAPE1/3.
CNST2=CV-ALFAM*TEMP3
CNST2M=CM-ALFAM*TEMP3
CNST3V=12.*ALFAM/3.*BETAV/(1.-LAMDAM)
CNST3M=2.*ALFAM/3.*BETAM
WRAID=W*DGTRC
COSW=COS(WRAD)
SINW=SIN(WRAD)
OUTPUT THE INPUT
WRITE (6,1340) METAL,CV,ALFAM,BETAV,GAMAV,LAMDAV,KFCTRV,CM,ALFAM,
1 BETAM,GAMAM,LAMDAM,KFCTRM,W,VTERM,BLAST,SHAPE,AA
GAMAV=GAMAV/(1.-LAMDAM)
LAMDAM=LAMDAM/(1.-CNST3M)
GAMAM=GAMAM/(1.-CNST3M)
C
IF (AAA(1).NE.10HFRAGMENTAT) GO TO 210
CALL FRAG2 (1H1)
GO TO 220
210 WRITE (6,1340)
C
220 CALL VECTR
C
DO 260 K2=K22,K222
IF (SGST(K2).EQ.0.) GO TO 260
IF (AAA(1).EQ.10HFRAGMENTAT) GO TO 230
IF (FRGFLG.EQ.0) GO TO 250
230 NNSP=NSP(K2)
DO 240 K1=1,NNSP
240 M(K1,K2)=ALOG10(M(K1,K2))
250 VDYN(K2)=ALOG10(VDYN(K2))
VDYN(K2+46)=ALOG10(VDYN(K2+46))
260 CONTINUE

```

LASV241R 002500
 LASV242R 002510
 LASV243 002520
 LASV244 002530
 LASV245 002540
 LASV246 002550
 LASV247 002560
 LASV248 002570
 LASV249 002580
 LASV250 002590
 LASV251R 002600
 LASV252 002610
 LASV253 002620
 LASV254 002630
 LASV255 002640
 LASV256 002650
 LASV257 002660
 LASV258 002670
 LASV259 002680
 LASV260 002690
 LASV261* 002700
 LASV262R 002710
 LASV263 002720
 LASV264 002730
 LASV265 002740
 LASV266 002750
 LASV267 002760
 LASV268 002770
 LASV269 002780
 LASV270 002790
 LASV271 002800
 LASV272 002810
 LASV273 002820
 LASV274 002830
 LASV275 002840
 LASV276 002850
 LASV277 002860
 LASV278W 002870
 LASV279W 002880
 LASV280 002890
 LASV281 002900
 LASV282 002910
 LASV283 002920
 LASV284 002930
 LASV285 002940
 LASV286 002950
 LASV287W 002960
 LASV288 002970
 LASV289 002980
 LASV290 002990
 LASV291 003000
 LASV292 003010
 LASV293 003020
 LASV294 003030
 LASV295 003040
 LASV296 003050
 LASV297 003060
 LASV298 003070
 LASV299 003080
 LASV300 003090


```

VOID2=0
IF (NZ.EQ.0) CALL FLAT
IF (A.NE.0..AND.NSID.EQ.2) CALL A2SID
IF (A.NE.0..AND.NSID.EQ.1) CALL A1SID
IF (B.NE.0..AND.NSID.EQ.2) CALL B2SID
IF (B.NE.0..AND.NSID.EQ.1) CALL B1SID
SCALE2=SCALE1(ITRGT)
IF (ABS(SCALE2)-1..LT..00001) SCALE2=1.
IF (ABS(SCALE2-1)..LT..00001) GO TO 330
SCALE3=1./SCALE2
DO 320 I=LYMXL,LYMYR
DO 320 J=LYMYB,LYMYT
320 LAMDA2(I,J)=LAMDA2(I,J)*SCALE3
C
330 BUFFER(1)=FILES
  BUFFER(2)=NXX
  BUFFER(3)=NYY
  ABUFFER(4)=CELL
  ABUFFER(5)=HOB
  BUFFER(6)=IRDM
  BUFFER(7)=ICOL
  BUFFER(8)=LYMYB
  BUFFER(9)=LYMYT
  BUFFER(10)=LYMXL
  BUFFER(11)=LYMYR
  ABUFFER(12)=A
  ABUFFER(13)=B
  BUFFER(14)=NSID
  BUFFER(15)=NX
  BUFFER(16)=NY
  BUFFER(17)=NZ
  ABUFFER(18)=TT(ITRGT)
  ABUFFER(19)=THCK
  K=19
DO 340 I=LYMXL,LYMYR
DO 340 J=LYMYB,LYMYT
  K=K+1
340 ABUFFER(K)=LAMDA2(I,J)
CALL WRITMS (TAPE,BUFFER(1),K,FILES,-1,C)
PLIST(FILES,2)=K
LOOP ON THE DIFFERENT CRITERIA
DO 400 IKRIT=1,NKRIT
  WRITE (6,1150) KRIT(IKRIT),HOB,THCK,CELL,NX,NY,NZ,TT(ITRGT),
1  SCALE2
  LINES=6
  IF (NZ.EQ.0) GO TO 350
  WRITE (6,1160) A,B,NSID
  LINES=LINES+2
350 WRITE (6,1170) NX,NY,SHELX,SHELX
  LINES=LINES+2
  IF (IFLAG=8..LT.C) GO TO 360
  WRITE (6,1190) WORD(4),WORD(2),LYMYT
  LINES=LINES+2
  IFLAG=IFLAG-8
  GO TO 370
360 IF (LIMIT.NE.NY) GO TO 370
  WRITE (6,1190) WORD(3),WORD(2),LYMYT
  LINES=LINES+2
370 IF (IFLAG=4..LT.C) GO TO 380
  WRITE (6,1190) WORD(4),WORD(2),LYMYE

```

```

LASV361 00370C
LASV362 003710
LASV363 003720
LASV364 003730
LASV365 003740
LASV366 003750
LASV367 003760
LASV368 003770
LASV369 003780
LASV370 003790
LASV371 003800
LASV372 003810
LASV373 003820
LASV374 003830
LASV375 003840
LASV376 003850
LASV377 003860
LASV378 003870
LASV379 003880
LASV380 003890
LASV381 003900
LASV382 003910
LASV383 003920
LASV384 003930
LASV385 003940
LASV386 003950
LASV387 003960
LASV388 003970
LASV389 003980
LASV390 003990
LASV391 004000
LASV392 004010
LASV393 004020
LASV394 004030
LASV395 004040
LASV396 004050
LASV397 004060
LASV398 004070
LASV399 004080
LASV400 004090
LASV401 004100
LASV402 004110
LASV403 004120
LASV404 004130
LASV405 004140
LASV406 004150
LASV407 004160
LASV408 004170
LASV409 004180
LASV410 004190
LASV411 004200
LASV412 004210
LASV413 004220
LASV414 004230
LASV415 004240
LASV416 004250
LASV417 004260
LASV418 004270
LASV419 004280
LASV420 004290

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```

      LINES=LINES+2
      IF LAG=IFLAG-4
        GO TO 39C
      380 IF (LIMB.NE.1.CF.IROM.EQ.0) GO TO 390
      WRITE (6,119C) WORD(3),WORD(2),LYMYB
      LINES=LINES+2
      390 IF (IFLAG-2.LT.0) GO TO 400
      WRITE (6,119C) WORD(4),WORD(1),LYMYR
      LINES=LINES+2
      IF LAG=IFLAG-2
        GO TO 410
      400 IF (LIMR.NE.NXX) GO TO 410
      WRITE (6,119C) WORD(3),WORD(1),LYMYR
      LINES=LINES+2
      410 IF (IFLAG.NE.1) GO TO 420
      WRITE (6,119C) WORD(4),WORD(1),LYMYL
      LINES=LINES+2
      GO TO 430
      420 IF (LIML.NE.1) GO TO 430
      WRITE (6,119C) WORD(3),WORD(1),LYMYL
      LINES=LINES+2
      430 WRITE (6,120C) TNAME,FILES
      LINES=LINES+2
C
      LAPI=0
      IF (VUID2.NE.0) GO TO 44C
      GO TO 440 IF PERF MATRIX IS ZEROES
      CALL PERKAY (LAPI)
      440 CALL OUTPUT (LAPI)
      IF (VUID2.EQ.0) GO TO 450
      WRITE (6,123C)
      LINES=LINES+2
      GO TO 45C
      450 IF (CCC.EQ.1)CHCONTOUR .AND.LAPI.NE.0) CALL CONTR
      IF (IKRIT.EQ.NKRIT) GO TO 47C
C
      K=15
      DO 460 I=LYMYL,LYMYR
      DO 460 J=LYMYB,LYMYT
      K=K+1
      460 LAMDA2(I,J)=ABU*FR(K)
      470 IF (LAPI.NE.0) GO TO 480
      IF (IKRIT.EQ.NKRIT) GO TO 48C
      LAPI=NKRIT-1
      WRITE (6,1220) FILES,TNAME,LAPI
      LINES=LINES+2
      GO TO 49C
      480 CONTINUE
C
      490 IF (SHOW(ITRGT).EQ.0.OR.VOIL2.NE.0) GO TO 510
      WRITE (6,IFMT1) SHOW(ITRGT),HOB,CELL
      WRITE (6,121C) TNAME,FILES
      LINES=LINES+4
C
      RECOVER THE PERFORATION MATRIX
      K=5
      DO 500 I=LYMYL,LYMYR
      DO 500 J=LYMYB,LYMYT
      K=K+1
      500 LAMDA2(I,J)=ABU*FR(K)
      CALL SHOW (ITRGT)

```

```

LASV421 004300
LASV422 004310
LASV423 004320
LASV424 004330
LASV425W 004340
LASV426 004350
LASV427 004360
LASV428W 004370
LASV429 004380
LASV430 004390
LASV431 004400
LASV432 004410
LASV433W 004420
LASV434 004430
LASV435 004440
LASV436W 004450
LASV437 004460
LASV438 004470
LASV439 004480
LASV440W 004490
LASV441 004500
LASV442W 004510
LASV443 004520
LASV444 004530
LASV445 004540
LASV446 004550
LASV447 004560
LASV448 004570
LASV449 004580
LASV450 004590
LASV451W 004600
LASV452 004610
LASV453 004620
LASV454 004630
LASV455 004640
LASV456 004650
LASV457 004660
LASV458 004670
LASV459 004680
LASV460 004690
LASV461 004700
LASV462 004710
LASV463 004720
LASV464 004730
LASV465W 004740
LASV466 004750
LASV467 004760
LASV468 004770
LASV469 004780
LASV470 004790
LASV471W 004800
LASV472W 004810
LASV473 004820
LASV474 004830
LASV475 004840
LASV476 004850
LASV477 004860
LASV478 004870
LASV479 004880
LASV480 004890

```

```

510 FILES=FILES+1
C
C
IF (AAA(1).EQ.1CHCONTOUR .OR.AAA(1).EQ.1CHNO PROBABI.OR.AAA(1).E.LASV481 004900
1Q.1OHFRAGMENTAT) READ (5,105C) (AAA(1),I=1,8) LASV482 004910
IF (AAA(1).NE.1OHASSEMBLE .AND.AAA(1).NE.1OH ASSEMBLE .AND.AAA(1).LASV483 00492C
1.NE.1OH ASSEMBLE) GO TO 8C LASV484R 004930
LASV485R 00494C
LASV486 004950
LASV487 004960
LASV488 004970
LASV489 004980
LASV490 004990
LASV491 005000
LASV492 00501C
LASV493 005020
LASV494 005030
LASV495 005040
LASV496* 005050
LASV497 005060
LASV498 005070
LASV499 005080
LASV500 00509C
LASV501 005100
LASV502 005110
LASV503 005120
LASV504 005130
LASV505 005140
LASV506 00515C
LASV507 005160
LASV508 005170
LASV509 005180
LASV510 005190
LASV511R 005200
LASV512 005210
LASV513 005220
LASV514* 005230
LASV515 005240
LASV516 005250
LASV517 005260
LASV518 005270
LASV519R 005280
LASV520 005290
LASV521 00530C
LASV522R 005310
LASV523* 005320
LASV524 005330
LASV525 005340
LASV526 005350
LASV527 00536C
LASV528R 00537C
LASV529 005380
LASV530* 005390
LASV531 00540C
LASV532 005410
LASV533 005420
LASV534R 005430
LASV535 005440
LASV536 00545C
LASV537* 00546C
LASV538 00547C
LASV539 005480
LASV540K 00549C

```

THIS PART OF MAIN ASSEMBLES A COMPLETE TARGET FROM ITS COMPONENT PARTS

```

520 KKSVM=1
VOID2=0
530 DECODE (50,1240,AAA(2) JFKSYM,FNPNTS,CCC,FNSTAP,NOPK
KSYM=FKSYM+.1
NPNTS=FNPNTS+.1
NSTAPE=FNSTAP+.1
IF (NSTAPE.GT.0) GO TO 560
DO 540 I=1,50C0
J=5001-I
IF (SLIST(J,2).NE.0) GO TO 550
540 CONTINUE
J=0
550 NSTAPE=J+1
560 DO 570 I=1,7
SHFTX(I)=0
570 SHFTY(I)=0
IF (NPNTS.EQ.0) NPNTS=1
READ (5,1090) (AAA(I),I=1,8)
SHO=AAA(1)
IF (SHO.NE.1OHEXPECTED P) GO TO 620
DECODE (10,1100,AAA(3) JAAA(1),FSHOW(1)
IF (AAA(1).NE.1OHALL- ) GO TO 590
DO 580 I=1,NPNTS
FSHOW(I)=FSHOW(1)
GO TO 600
590 READ (5,1110) (FSHOW(I),I=1,NPNTS)
600 DO 610 I=1,NPNTS
610 SHOW(I)=FSHOW(I)+.1
READ (5,1090) (AAA(I),I=1,8)
620 DECODE (60,1110,AAA(1) JFNKRIT,(FNKRIT(I),I=1,7)
NKRIT=FNKRIT+.1
DO 630 I=1,NKRIT
KRIT(I)=FNKRIT(I)+.1
REWINC PTAPEI
READ (5,1090) (AAA(I),I=1,8)
DO 950 IPNT=1,NPNTS
640 DECODE (60,1110,AAA(1) JFNFILE,(FFILE(I),I=1,7)
NFILE=FNFILE+.1
DO 650 I=1,NFILE
650 FILE(I)=FFILE(I)+.1
READ (5,1090) (AAA(I),I=1,8)
660 IF (AAA(1).EQ.1CHSHIFT X = .OR.AAA(1).EQ.1OH SHIFT X =) GO TO 690
670 IF (AAA(1).NE.1CHSHIFT Y = .AND.AAA(1).NE.1OH SHIFT Y =) GO TO 710LASV536
DECODE (60,1110,AAA(3) J(FSHFTY(I),I=2,NFILE)
DO 680 I=2,NFILE
680 SHFTY(I)=FSHFTY(I)+SIGN(.1,FSHFTY(I))
READ (5,1090) (AAA(I),I=1,8)

```

```

GO TC 660
650 DECIDE (GO,111C,AAA(3))(FSHFTX(I),I=2,NFILE)
DO 70C I=2,NFILE
700 SHFTX(I)=FSHFTX(I)+SIGN(.1,FSHFTX(I))
HEAD (.5,109C)(AAA(I),I=1,8)
GO TO 670
710 ASSIGN 880 TO SNM1
CALL READMS (TAPE,BUFFER(1),PLIST(FILE(1),2),FILE(1))
NXX=BUFFER(2)
NYY=BUFFER(3)
CELL=ABUFFER(4)
HOB=ABUFFER(5)
IROW1=BUFFER(6)
ICOL1=BUFFER(7)
L1MYB=BUFFER(8)
L1MYT=BUFFER(9)
L1MXL=BUFFER(10)
L1MYB=BUFFER(11)
L1MYT=BUFFER(12)
L1MXR=BUFFER(13)
B1=ABUFFER(14)
NSID1=BUFFER(15)
K=19
DO 720 I=1,L1MXL,L1MYR
DO 720 J=1,L1MYB,L1MYT
K=K+1
720 PERFL(I,J)=ABUFFER(K)
C
NGSLP=IROW1
IF (61-NE.O..AND.NSID1.EQ.1) ASSIGN 690 TO SNM1
KK1=2*IROW1+1
LYMYB=L1MYB
LYMYT=L1MYT
LYMXL=L1MXL
LYMYR=L1MYR
IF (NFILE.GT.1) GO TO 740
DO 730 I=LYMXL,L1MYR
DO 730 J=LYMYB,L1MYT
730 LAMDA(I,J)=PERFL(I,J)
GO TO 920
740 DO 910 JFILE=2,NFILE
ASSIGN 850 TO SNM2
CALL READMS (TAPE,BUFFER(1),PLIST(FILE(IFILE),2),FILE(IFILE))
NXX=BUFFER(2)
NYY=BUFFER(3)
CELL=ABUFFER(4)
HOB=ABUFFER(5)
IROW2=BUFFER(6)
ICOL2=BUFFER(7)
L2MYB=BUFFER(8)
L2MYT=BUFFER(9)
L2MXL=BUFFER(10)
L2MYR=BUFFER(11)
L2MYB=BUFFER(12)
L2MYT=BUFFER(13)
NSID2=BUFFER(14)
K=19
DO 750 I=L2MXL,L2MYR
DO 750 J=L2MYB,L2MYT
K=K+1
750 PERFL(I,J)=ABUFFER(K)
C
IF (62-NE.C..AND.NSID2.EQ.1) ASSIGN 860 TO SNM2

```

```

LASV541 005500
LASV542* 005510
LASV543 005520
LASV544 005530
LASV545R 005540
LASV546 005550
LASV547 005560
LASV548 005570
LASV549 005580
LASV550 005590
LASV551 005600
LASV552 005610
LASV553 005620
LASV554 005630
LASV555 005640
LASV556 005650
LASV557 005660
LASV558 005670
LASV559 005680
LASV560 005690
LASV561 005700
LASV562 005710
LASV563 005720
LASV564 005730
LASV565 005740
LASV566 005750
LASV567 005760
LASV568 005770
LASV569 005780
LASV570 005790
LASV571 005800
LASV572 005810
LASV573 005820
LASV574 005830
LASV575 005840
LASV576 005850
LASV577 005860
LASV578 005870
LASV579 005880
LASV580 005890
LASV581 005900
LASV582 005910
LASV583 005920
LASV584 005930
LASV585 005940
LASV586 005950
LASV587 005960
LASV588 005970
LASV589 005980
LASV590 005990
LASV591 006000
LASV592 006010
LASV593 006020
LASV594 006030
LASV595 006040
LASV596 006050
LASV597 006060
LASV598 006070
LASV599 006080
LASV600 006090

```



```

C      KK2=2*IR0W2+1
C      SHFT IS THE AMOUNT BY WHICH THE GEOMETRICAL CENTER OF THIS PART OF
C      THE TARGET IS OFFSET FROM THE POINT DEFINED AS THE TARGET CENTER,
C      WHICH POINT IS ALWAYS IDENTICAL TO THE GEOMETRICAL CENTER OF THE
C      PART OF THE TARGET DEFINED BY FILE(1).
      DELX=ICOL2-ICOL1+SHFTX(IFILE)
      DELY=IR0W2-IR0W1+SHFTY(IFILE)
      SLIPX=0
      SLIPY=0
      IF (L2MXL-DELTX.LT.LYMXL) LYMXL=L2MXL-DELTX
      IF (L2MYR-DELTZ.GT.LYMYR) LYMYR=L2MYR-DELTZ
      IF (L2MYB-DELTZ.LT.LYMYB) LYMYB=L2MYB-DELTZ
      IF (L2MYT-DELTZ.GT.LYMYT) LYMYT=L2MYT-DELTZ
      IF (LYMXL.GE.1) GO TO 770
      IF (LYMYR.LT.DIMX) GO TO 760
      LYMXL=1
      GO TO 790
760 SLIPX=DIMX-LYMYR
      IF (1-LYMXL.LT.SLIPX) SLIPX=1-LYMXL
      GO TO 790
770 IF (LYMYR.LE.DIMX) GO TO 790
      IF (LYMXL.GT.1) GO TO 780
      LYMYR=DIMX
      GO TO 790
780 SLIPX=1-LYMXL
      IF (DIMX-LYMYR.GT.SLIPX) SLIPX=DIMX-LYMYR
790 IF (LYMYB.GE.1) GO TO 810
      IF (LYMYT.LT.DIMY.AND.NOSLP.NE.0) GO TO 800
      LYMYB=1
      GO TO 830
800 SLIPY=DIMY-LYMYT
      IF (1-LYMYB.LT.SLIPY) SLIPY=1-LYMYB
      GO TO 830
810 IF (LYMYT.LE.DIMY) GO TO 830
      IF (LYMYB.GT.1.AND.NOSLP.NE.0) GO TO 820
      LYMYT=DIMY
      GO TO 830
820 SLIPY=1-LYMYB
      IF (DIMY-LYMYT.GT.SLIPY) SLIPY=DIMY-LYMYT
830 LYMXL=LYMXL+SLIPX
      LYMYB=LYMYB+SLIPY
      LYMYT=LYMYT+SLIPY
      IF (LYMXL.LT.1) LYMXL=1
      IF (LYMYR.GT.DIMX) LYMYR=DIMX
      IF (LYMYB.LT.1) LYMYB=1
      IF (LYMYT.GT.DIMY) LYMYT=DIMY
      DO 890 I=LYMXL,LYMYR
      I1=1-SLIPX
      I2=1+DELTX
      DO 890 J=LYMYB,LYMYT
      J1=J-SLIPY
      J2=J1+DELTZ
      TERM1=0.
      TERM2=0.
      IF (I2.LT.L2MXL.GR.I2.GT.L2MYR) GO TO 86C
      IF (J2.LT.L2MYB.GR.J2.GT.L2MYT) GO TO 840
      TERM2=PERF2(I2,J2)
      GO TO 86C
840 GO TO SNUP2, (85C,860)

```

LASV601 006100
 LASV602 006110
 LASV603 006120
 LASV604 006130
 LASV605 006140
 LASV606 006150
 LASV607 006160
 LASV608 006170
 LASV609 006180
 LASV610 006190
 LASV611 006200
 LASV612 006210
 LASV613 006220
 LASV614 006230
 LASV615 006240
 LASV616 006250
 LASV617 006260
 LASV618 006270
 LASV619 006280
 LASV620 006290
 LASV621 006300
 LASV622 006310
 LASV623 006320
 LASV624 006330
 LASV625 006340
 LASV626 006350
 LASV627 006360
 LASV628 006370
 LASV629 006380
 LASV630 006390
 LASV631 006400
 LASV632 006410
 LASV633 006420
 LASV634 006430
 LASV635 006440
 LASV636 006450
 LASV637 006460
 LASV638 006470
 LASV639 006480
 LASV640 006490
 LASV641 006500
 LASV642 006510
 LASV643 006520
 LASV644 006530
 LASV645 006540
 LASV646 006550
 LASV647 006560
 LASV648 006570
 LASV649 006580
 LASV650 006590
 LASV651 006600
 LASV652 006610
 LASV653 006620
 LASV654 006630
 LASV655 006640
 LASV656 006650
 LASV657 006660
 LASV658 006670
 LASV659 006680
 LASV660 006690

```

850 K2=K2-J2
IF (J2.LT.1.AND.K2.LE.L2MYT.AND.K2.GE.L2MYB) TERM2=PERF2(I2,K2)
860 IF (J1.LT.1.LIMXL.CR.I1.GT.LIMXR) GO TO 890
IF (J1.LT.1.LIMYB.CR.J1.GT.LIMYT) GO TO 870
TERM1=PERF1(I1,J1)
GO TO 890
870 GO TO SNUP1, (860,890)
880 K1=K1-J1
IF (J1.LT.1.AND.K1.LE.L1MYT.AND.K1.GE.L1MYB) TERM1=PERF1(I1,K1)
890 LAMDA(I,J)=TERM1+TERM2
IRCW1=IRCW1+SLIPY
ICOL1=ICOL1+SLIPX
IF (IFILE.EQ.NFILE) GO TO 920
DO 900 I=LIMXL,LYMXR
DO 900 J=LIMYB,LYMYT
900 PERF(I,J)=LAMDA(I,J)
LIMXL=LYMXL
LIMYB=LYMYB
LIMXR=LYMXR
LIMYT=LYMYT
KK1=2*IRCW1+1
IF (82.NE.O.AND.NSID2.EQ.1.OR.SHFTY(IFILE).NE.O) ASSIGN 690 TO SNLASV682
1001
910 CONTINUE
920 IF (KSYM.NE.2) GO TO 940
IF (KSYM.EQ.2) GO TO 930
WRITE (PTAPE1) ICOL1,IRCW1,LYMXL,LYMYB,LYMYT,NFILE,((LAMDA(I,LASV6874
1 ,J)=LYMXL,LYMXR),J=LIMYB,LYMYT),(FILE(I),SHFTY(I),1=1,LASV688W
2 ,NFILE)
BACKSPACE PTAPE1
KSYM=KSYM+1
ICOL=ICOL1
IRCW=IRCW1
LIMXL=LYMXL
LIMYB=LYMYB
GO TO 640
930 CALL PAIR
GO TO 920
940 WRITE (PTAPE1) HGB,CELL,KSYM,ICOL1,IRCW1,LYMXL,LYMYB,LYMYT,
1 NFILE,((LAMDA(I,J)=LYMXL,LYMXR),J=LIMYB,LYMYT),(FILE(I),
2 SHFTY(I),SHFTY(I),1=1,NFILE)
950 KSYM=1
ENCODE (IC,120,IFMT1(13) )
IF (SHO.NE.ICHECKED P) GO TO 1050
REWIND PTAPE1
ENCODE (7C,120C,IFMT1(13) )
IF (NPNTS.GT.1) ENCODE (20,120C,IFMT1(13) )
ASSIGN 1020 TO JUMPS
IPNT=0
960 IPNT=IPNT+1
ENCODE (IC,127C,IFMT1(13) ) JPNT
READ (PTAPE1) HGB,CELL,KSYM,ICOL1,IRCW1,LYMXL,LYMYB,LYMYT,
1 NFILE,((LAMDA(I,J)=LYMXL,LYMXR),J=LIMYB,LYMYT),(FILE(I),
2 SHFTY(I),SHFTY(I),1=1,NFILE)
IF (SHOW(IPNT).EQ.C) GO TO 1030
SHLY=FLOAT(ICOL1)*.5
SHLY=FLOAT(IRCW1)*.5
CELL=CELL+12.
WRITE (6,IFMT1) SHOW(IPNT),HGB,CELL

```

LASV601 C06700
LASV602 C06710
LASV603 C06720
LASV604 C06730
LASV605 C06740
LASV606 C06750
LASV607 C06760
LASV608 C06770
LASV609 C06780
LASV610 C06790
LASV611 C06800
LASV612 C06810
LASV613 C06820
LASV614 C06830
LASV615 C06840
LASV616 C06850
LASV617 C06860
LASV618 C06870
LASV619 C06880
LASV620 C06890
LASV621 C06900
LASV622 C06910
LASV623 C06920
LASV624 C06930
LASV625 C06940
LASV626 C06950
LASV627 C06960
LASV628 C06970
LASV629 C06980
LASV630 C06990
LASV631 C07000
LASV632 C07010
LASV633 C07020
LASV634 C07030
LASV635 C07040
LASV636 C07050
LASV637 C07060
LASV638 C07070
LASV639 C07080
LASV640 C07090
LASV641 C07100
LASV642 C07110
LASV643 C07120
LASV644 C07130
LASV645 C07140
LASV646 C07150
LASV647 C07160
LASV648 C07170
LASV649 C07180
LASV650 C07190
LASV651 C07200
LASV652 C07210
LASV653 C07220
LASV654 C07230
LASV655 C07240
LASV656 C07250
LASV657 C07260
LASV658 C07270
LASV659 C07280
LASV660 C07290

```

LINES=1
970 ASSIGN 1000 TO JUMP4
980 IF (NFILE.GT.1) GO TO 990
WRITE (6,1300) FILE(1)
LINES=LINES+3
GO TO JUMP4, (1000,1010)
990 KEY=NFILE-1
ENCODE (10,1310,IFMT2(7) ,KEY1
ENCODE (10,1320,IFMT2(13) ,KEY1
WRITE (6,IFMT2) (FILE(1),I=1,NFILE),WORD(5),(SHFTX(1),I=1,NFILE),
1 WORD(6),(SHFTY(1),I=1,NFILE)
LINES=LINES+7
GO TO JUMP4, (1000,1010)
1000 WRITE (6,1170) NXX,NYY,SHELX,SHELY
LINES=LINES+2
IF (KSYM.NE.2) GO TO JUMP5, (1020,1080)
READ (PTAPE1) NFILE,(FILE(1),SHFTX(1),SHFTY(1),I=1,NFILE)
ASSIGN 1010 TO JUMP4
WRITE (6,1330)
LINES=LINES+1
GO TO 980
1010 WRITE (6,1180) SHELX,SHELY
LINES=LINES+2
GO TO JUMP5, (1020,1080)
1020 CALL SHOWW (IPNT)
GO TO 1040
1030 IF (KSYM.EQ.2) READ (PTAPE1)
1040 IF (IPNT.LT.NPNTS) GO TO 960
C
1050 ENCODE (70,1290,IFMT1(1) )
ASSIGN 1080 TO JUMP5
IKRIT=0
1060 IKRIT=IKRIT+1
REWINO PTAPE1
IPNT=0
1070 IPNT=IPNT+1
READ (PTAPE1) HC6,CELL,KSYM,ICOL1,IROW1,LYMXL,LYMY8,LYMYT,
1 NFILE,((LAMD2(I,J),I=LYMXL,LYMY8),J=LYMY8,LYMYT),(FILE(1),
2 SHFTX(1),SHFTY(1),I=1,NFILE)
ENCODE (10,1270,IFMT1(15) ,IPNT
HHOB(IPNT)=HOB
SHELX=FLOAT(ICOL1)*.5
SHELY=FLOAT(IROW1)*.5
CELL=CELL*12.
WRITE (6,IFMT1) KRIT(IKRIT),HOB,CELL1
LINES=1
GO TO 970
1080 CALL PEKAY (LAP.)
C
FOLLOWING INSTRUCTION MERELY GUARANTEES LAP1 .NE. 0
LAP1=NX
CALL OUTPUT (LAP1)
IF (CCC.EQ.10CHCNTGUR ) CALL CONTR
IF (IPNT.LT.NPNTS) GO TO 1070
IF (IKRIT.LT.NKRIT) GO TO 1060
C
IF (AAA(1).EQ.1CHASSEMBLE .OR.AAA(1).EQ.10H ASSEMBLE .OR.AAA(1).ELASV777
10.10H ASSEMBLE) GO TO 530
GO TO 80
C
C
C

```

```

LASV721 007300
LASV722 007310
LASV723 007320
LASV724 007330
LASV725 007340
LASV726 007350
LASV727 007360
LASV728 007370
LASV729 007380
LASV730 007390
LASV731 007400
LASV732 007410
LASV733 007420
LASV734 007430
LASV735 007440
LASV736 007450
LASV737 007460
LASV738 007470
LASV739 007480
LASV740 007490
LASV741 007500
LASV742 007510
LASV743 007520
LASV744 007530
LASV745 007540
LASV746 007550
LASV747 007560
LASV748 007570
LASV749 007580
LASV750 007590
LASV751 007600
LASV752 007610
LASV753 007620
LASV754 007630
LASV755 007640
LASV756 007650
LASV757 007660
LASV758 007670
LASV759 007680
LASV760 007690
LASV761 007700
LASV762 007710
LASV763 007720
LASV764 007730
LASV765 007740
LASV766 007750
LASV767 007760
LASV768 007770
LASV769 007780
LASV770 007790
LASV771 007800
LASV772 007810
LASV773 007820
LASV774 007830
LASV775 007840
LASV776 007850
LASV777 007860
LASV778 007870
LASV779 007880
LASV780 007890

```



```
* 838* 1 008460
BLOKD 2 008490
BLOKD 3 008500
BLOKD 40 008510
BLOKD 5- 008520
```

```
BLOCK DATA
COMMON /DISC/ DISC(15016)
INTEGER DISC
DATA DISC /15016*0/
END
```

```
* 843* 2 008530
FILNM 2 008540
FILNM 3 008550
FILNM 4 008560
FILNM 5 008570
FILNM 6 008580
FILNM 7 008590
FILNM 8 008600
FILNM 9 008610
FILNM10 008620
FILNM11 008630
FILNM12 008640
FILNM13 008650
FILNM14 008660
FILNM15 008670
FILNM16 008680
FILNM17 008690
FILNM18 008700
FILNM19 008710
FILNM20- 008720
```

```
SUBROUTINE FILNAM (NAME3,NAME4)
THIS SUBROUTINE RETURNS THE NAMES OF THE 3RD AND 4TH FILES AS
SPECIFIED ON THE PROGRAM CARD OR ON A CONTROL CARD EQUIVALENCING
A FILE NAME TO THESE FILES.
```

C
C
C
C

```
DIMENSION DUM(1)
I=LOC(DUM(1))
I--1
J=IBITS(DUM(I+5),0,16)
K=J+1+1
NAME3=IBITS(DUM(K),18,42)
J=IBITS(DUM(I+6),0,18)
K=J+1+1
NAME4=IBITS(DUM(K),18,42)
NAME3=SHIFT(NAME3,18)
NAME4=SHIFT(NAME4,18)
CALL BLFILL (NAME3,NAME3)
CALL BLFILL (NAME4,NAME4)
RETURN
END
```

```
* 863* 3 008730
USED 2 008740
USED 3 008750
USED 4 008760
USED 5 008770
USED 6 008780
USED 7 008790
USED 8 008800
USED 9 008810
USED 10 008820
USED 11 008830
USED 12- 008840
```

```
INTEGER FUNCTION USED (DUMMY)
THIS FUNCTION RETURNS THE NUMBER OF LINES USED ON THE CURRENT PAGEUSED
COMMON /PAGE/ LINES, PAGE
INTEGER PAGE
IF (LINES-63) 20,20,23
10 LINES=LINES+60
20 USED=LINES
RETURN
30 LINES=LINES-(LINES/PAGE)*PAGE
IF (LINES-3) 10,10,20
END
```

C
C

```

C
SUBROUTINE FRAG (KEY)
COMMON /COM3/COM3(10000)
DIMENSION SPRBS(46),VSTMN(46),VSTMX(46),NSP(46),FNSP(46),M(40,46)
1 EQUIVALENCE (COM3(1),SPRBS(1)),(COM3(139),VSTMN(1))
1 (COM3(185),VSTMX(1)),(COM3(323),NSP(1)),FNSP(1))
2 (COM3(369),M(1,1)),(COM3(209),Q(1,1))
3 (COM3(409),SGST(1)),(COM3(936),NSPRA,FNSPRA)
4 (COM3(940),SHAPE),(COM3(941),AA),(COM3(9942),NNSP)
5 (COM3(9963),K22),(COM3(9984),K22)
C
COMMON /AAA/AAA(8)
COMMON /CONST/CONSTT(6)
EQUIVALENCE (CONSTT(1),T0P1),(CONSTT(2),RT0G),(CONSTT(3),DGTOR)
COMMON /NUM4/NUM(46)
C
DIMENSION WORD(3)
C
INTEGER AAA,WORD
REAL M,NUM
C
DATA (WORD(1),I=1,3) /6H M , 6H Q , 6H /
C
ENTRY FRAG1
DECODE (20,19C,AAA(3)) SHAPE,AA
READ (5,190) FNSPRA,(FNSP(I),I=1,7)
NSPRA=FNSPRA*.1
IF (NSPRA-6T.7) READ (5,190) (FNSP(I),I=8,NSPRA)
DO 10 I=1,NSPRA
10 NSP(I)=FNSP(I)*.1
DO 40 K2=1,NSPRA
K1=NSP(K2)
IF (K1-4) 40,20,30
20 READ (5,190) M(4,K2)
30 READ (5,190) (M(I-1,K2),Q(I,K2),I=5,K1),M(K1,K2)
40 CONTINUE
DO 50 I=1,NSPRA
50 CONTINUE
READ (5,160) SPRBS(I),SPRBS(I+1),VSTMN(I),VSTMX(I),NUM(I),SGST(I)
CSB52=1.
DO 60 I=1,NSPRA
60 I=1,NSPRA
SPRBS(I+1)=SPRBS(I)+1*DGTOR
NO NEED TO CONVERT SPRBS(I)=G.
CSB51=CSB52
CSB52=CSB51*(SPRBS(I+1))
SOLANG=TWCP1*(CSB51-CSB52)
IF (NUM(I).LT..0000001) NUM(I)=SGST(I)*SOLANG
IF (SGST(I).LT..0000001) SGST(I)=NUM(I)/SOLANG
60 CONTINUE
C
FIND THE BLOCKS OF DYNAMIC SPRAYS, FRONT AND REAR, FOR WHICH SGST
IS ZERO TO ELIMINATE THEM FROM CONSIDERATION
DO 70 K22=1,NSPRA
70 K22=1,NSPRA
IF (SGST(K22)-6T..0000001) 60 TO 60
70 CONTINUE
60 DO 60 K=1,NSPRA
K222=NSPRA-K+1
IF (SGST(K222)-6T..0000001) 60 TO 170

```

```

* 875* 4 00885C
FRAG 2 008860
FRAG 3 008870
FRAG 4 008880
FRAG 5 008890
FRAG 6 008900
FRAG 7 008910
FRAG 8 008920
FRAG 9 008930
FRAG 10 008940
FRAG 11 008950
FRAG 12 008960
FRAG 13 008970
FRAG 14 008980
FRAG 15 008990
FRAG 16 009000
FRAG 17 009010
FRAG 18 009020
FRAG 19 009030
FRAG 20 009040
FRAG 21 009050
FRAG 22 009060
FRAG 23 009070
FRAG 24 009080
FRAG 25 009090
FRAG 26 009100
FRAG 27 009110
FRAG 28 009120
FRAG 29 009130
FRAG 30 009140
FRAG 31 009150
FRAG 32 009160
FRAG 33 009170
FRAG 34 009180
FRAG 35 009190
FRAG 36 009200
FRAG 37 009210
FRAG 38 009220
FRAG 39 009230
FRAG 40 009240
FRAG 41 009250
FRAG 42 009260
FRAG 43 009270
FRAG 44 009280
FRAG 45 009290
FRAG 46 009300
FRAG 47 009310
FRAG 48 009320
FRAG 49 009330
FRAG 50 009340
FRAG 51 009350
FRAG 52 009360
FRAG 53 009370
FRAG 54 009380
FRAG 55 009390
FRAG 56 009400
FRAG 57 009410
FRAG 58 009420
FRAG 59 009430
FRAG 60 009440

```

```

90 CONTINUE
   GO TO 170

C
ENTRY FRAG2
WRITE (6,21G) KEY
DO 14G K2=1,NSPRA
  WRITE (6,24G) K2
  NSP=NSP(K2)
  KNT1=NSP/1C
  IF (KNT1*10.EQ.NNSP) KNT1=KNT1-1
  III=C
  IIII=1
  IF (KNT1.LE.C) GO TO 110
  DO 10G I=1,KNT1
    II=(I-1)*10+1
    III=I*1C
    WRITE (6,230) WORD(IIII),(M(K1,K2),K1=II,IIII)
  100 IIII=3
  110 III=IIII+1
    WRITE (6,230) WORD(IIII),(M(K1,K2),K1=III,NNSP)
    III=0
    IIII=2
    IF (KNT1.LE.C) GO TO 130
    DO 120 I=1,KNT1
      II=(I-1)*1C+1
      III=I*1C
      WRITE (6,230) WORD(IIII),(Q(K1,K2),K1=II,IIII)
  120 IIII=3
  130 III=IIII+1
    WRITE (6,230) WORD(IIII),(Q(K1,K2),K1=III,NNSP)
  140 CONTINUE
    WRITE (6,200)
    DO 150 I=1,NSPRA
      SPRES(I+1)=SPRBS(I+1)*RTDGG
      WRITE (6,220) I,SPRBS(I),SPRBS(I+1),VSTMN(I),VSTMX(I),NUM(I),
        1 SGST(I)
  150 CONTINUE
    DO 16C I=1,NSPRA
      SPRBS(I+1)=SPRBS(I+1)*DGTOR
  160 SPRBS(I+1)=SPRBS(I+1)*DGTOR
  170 RETURN

C
180 FORMAT (10X,7E1C.4)
190 FORMAT (8E1C.4)
200 FORMAT (/10H,EX,5HSPRAY,EX,7HLEADING,EX,6HTRAILING,EX,6HMEDIAN,EXFRAG104
  1,8HMAXIMUM,2(5X,8HFRAGMENT)/1H,5X,8HNUMBER,4X,2(6H EDGE,7X),2(8HFRAG105
  2HVELOCITY,5X),7H NUMBER,EX,7H DENSITY/)
210 FORMAT (A1/31H THE FRAGMENTATION DATA FOLLOW.)
220 FORMAT (1H,11C,2F13.1)
230 FORMAT (1H,1AC,1C12.4)
240 FORMAT (/13H SPAY NUMBER,13/)
      END

```

```

FRAG 61 00945C
FRAG 62 009460
FRAG 63 00947C
FRAG 64E 009480
FRAG 65W 00949C
FRAG 66 009500
FRAG 67W 009510
FRAG 68 009520
FRAG 69 009530
FRAG 70 009540
FRAG 71 009550
FRAG 72 009560
FRAG 73 009570
FRAG 74 00958C
FRAG 75 009590
FRAG 76 009600
FRAG 77W 009610
FRAG 78 009620
FRAG 79 00963C
FRAG 80W 00964C
FRAG 81 009650
FRAG 82 009660
FRAG 83 009670
FRAG 84 009680
FRAG 85 009690
FRAG 86 00970C
FRAG 87W 009710
FRAG 88 009720
FRAG 89 00973C
FRAG 90W 00974C
FRAG 91 00975C
FRAG 92W 00976C
FRAG 93 00977C
FRAG 94 009780
FRAG 95W 00979C
FRAG 96W 00980C
FRAG 97 00981C
FRAG 98 009820
FRAG 99 00983C
FRAG10C 00984C
FRAG101 00985C
FRAG102 00986C
FRAG103 00987C
FRAG104 00988C
FRAG105 00989C
FRAG106 009900
FRAG107 00991C
FRAG108 00992C
FRAG109 009930
FRAG11C 009940
FRAG111- 009950

```

```

SUBROUTINE VECTR
C THIS SUBROUTINE VECTORS THE SPRAYS FORWARD TO ACCOUNT FOR THE
C PROJECTILE TERMINAL VELOCITY.
C THIS ROUTINE EXPECTS THE VELOCITIES TO CORRESPOND TO THE SPRAY
C MIDPOINTS. THE 1ST AND LAST SPRAYS MUST BE CONES CENTERED AT 0
C AND 180 DEGREES, RATHER THAN CONICAL ANNULLI. NOTE THAT THE
C MIDSpray POINT FOR THESE 2 SPRAYS IS AT THE OUTER SPRAY BOUNDARY,
C RATHER THAN AT THE AVERAGE OF THE 2 BOUNDARIES.
C
COMMON /COM3/COM3(13000)
DIMENSION SPRBS(46),SPRBD(92),VST(92),VDYN(92),SGDIN(92)
EQUIVALENCE (COM3(1)),SPRBS(1), (COM3(47)),SPRBD(1))
EQUIVALENCE (COM3(139)),VST(1), (COM3(231)),VDYN(1))
1 (COM3(139)),VST(1), (COM3(231)),VDYN(1))
2 (COM3(4095)),SGDIN(1), (COM3(9930)),NSPRA)
3 (COM3(9961)),VTERM)
C
COMMON /CONST/CONST(6)
EQUIVALENCE (CONST(1)),TWOP1)
COMMON /NUP46/NUP(46)
C
REAL NUM
C
RATHER THAN OBTAIN THE ANGLES AT WHICH THE DYNAMIC SPRAY EDGES
OCCUR, WE LEAVE THEM AS COSINES
C
DO THE 1ST HALF OF THE 92 WORD ARRAYS-IE, V STATIC MEDIAN.
II=NSPRA-1
VTM2=VTERM**2
K=0
C LEADING EDGE OF FIRST SPRAY
10 CSBS1=1.
SPRBD(1+K)=1.
DO 20 I=1,II
J=I+K
C POSITIONS OF DYNAMIC SPRAY EDGES
CSBS2=CS(SPRBS(1+I))
VBND5=(VST(J)+VST(J+1))/2.
VBND5=SQRT(VBND5**2+2.*VBND5*VTERM*CSBS2+VTM2)
SPRBD(J+1)=(VBND5*CSBS2+VTERM)/VBND5
C VECTOR THE DENSITIES
SGDIN(J)=NUM(I)/(ABS(SPRBD(J+1))-SPRBD(J))*TWOP1)
C VECTOR THE STATIC SPRAY SPEEDS (CORE)PCND TO SPRAY MID POINT)
SPRMS=(SPRBS(I)+SPRBS(I+1))/2.
VDYN(J)=SQRT(VST(J)**2+2.*VST(J)*VTERM*CS(SPRMS)+VTM2)
C SET UP FOR NEXT SPRAY.
20 CSBS1=CSBS2
C THE 1ST SPRAY
VDYN(1+K)=VST(1+K)+VTERM
C THE LAST SPRAY.
SGDIN(NSPRA+K)=NUM(NSPRA)/(ABS(1.-SPRBD(NSPRA+K))*TWOP1)
VDYN(NSPRA+K)=VST(NSPRA+K)-VTERM
SPRBD(NSPRA+1+K)=-1.
C FINISHED WITH VSTM, CG VSTM, CR, FINISHED WITH VSTM, RETURN
IF (K.EQ.46) RETURN
K=46
GL TC 10
END

```

```

* 986* 5 009960
VECTR 2 009960
VECTR 3 009960
VECTR 4 009990
VECTR 5 010000
VECTR 6 010010
VECTR 7 010020
VECTR 8 010030
VECTR 9 010040
VECTR10 010050
VECTR11 010060
VECTR12 010070
VECTR13 010080
VECTR14 010090
VECTR15 010100
VECTR16 010110
VECTR17 010120
VECTR18 010130
VECTR19 010140
VECTR20 010150
VECTR21 010160
VECTR22 010170
VECTR23 010180
VECTR24 010190
VECTR25 010200
VECTR26 010210
VECTR27 010220
VECTR28 010230
VECTR29 010240
VECTR30 010250
VECTR31 010260
VECTR32 010270
VECTR33 010280
VECTR34 010290
VECTR35 010300
VECTR36 010310
VECTR37 010320
VECTR38 010330
VECTR39 010340
VECTR40 010350
VECTR41 010360
VECTR42 010370
VECTR43 010380
VECTR44 010390
VECTR45 010400
VECTR46 010410
VECTR47 010420
VECTR48 010430
VECTR49 010440
VECTR50 010450
VECTR51 010460
VECTR52 010470
VECTR53 010480
VECTR54 010490
VECTR55 010500
VECTR56 010510
VECTR57- 010520

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93


```

IF (IFSTA.LE.ILSTB) GO TO 160
VOID2=2
GO TO 210
100 DD 12C II=IFSTA,ILSTB
XX=2*(II-ICOL)
DD 12C JJ=1,NYY
Y=2*(JJ-IROW)-1
PRFK=C.
DD 110 K=1,NZ
FK=2*K-1
X=XX+FK*COSSA
Z=H-FK*SINAA
R2=X**2+Y**2+Z**2
R=SQRT(R2)
ETA=-Z*COSSA-X*SINAA
THETA=(X*COSSA-Z*SINAA)/R
STER=4.*ETA/(R2*R)
C
CALL DANCE
C
110 PRFK=PRFK+PRF1
120 PERFI(JJ)=PRFK/2.
IF (IFSTA.EQ.1.AND.ILSTB.EQ.NXX) GO TO 14C
I11=1
I12=MAX
IF (IFSTA.NE.1) I12=IFSTA-1
IF (ILSTB.NE.NXX) I11=ILSTB+1
DD 130 II=I11,I12
DD 13C JJ=1,NYY
130 PERFI(JJ)=0.
14C IF (H.GT.EPSLN.OR.ABS(AI)-90..GT..0001) GO TO 200
C
PROJECTILE IMPACT ON PLATE
FN2=NZ
F=EPSLN/2.
IF (H.GT.C.) F=SQRT(EPSLN**2-H**2)/2.
IF (AINT(F).NE.F.OR.F.EQ.0.) F=F+1.
K=F
LIMYB=IROW-K
LIMYT=IROW+K
LIMXL=ICOL-K
LIMXR=ICOL+K
IF (LIMYB.LT.1) LIMYB=1
IF (LIMYT.GT.NYY) LIMYT=NYY
IF (LIMYB.GT.LIMYT) GO TO 20C
IF (90.-ABS(AI).LE..0001) GO TO 180
TEMP1=EPSLN*COSSA
TEMP2=2.*FN2*SINAA
IF (H.LT.TEMP1-TEMP2) GO TO 150
F=(TEMP1-H)/ABS(TANA)+EPSLN*SINAA
GO TO 17C
150 TEMP1=2.*FN2*COSSA
IF (H.LT.-TEMP2) GO TO 160
F=TEMP1+SQRT(EPSLN**2-(TEMP2+H)**2)
GO TO 17C
160 F=TEMP1+EPSLN
170 F=F/2.
IF (AINT(F).NE.F) F=F+1.
K=F
IF (A.GT.C.) LIMXL=ICOL-K

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GEOM121 011730
GEOM122 011740
GEOM123 011750
GEOM124 011760
GEOM125 011770
GEOM126 011780
GEOM127 011790
GEOM128 011800
GEOM129 011810
GEOM130 011820
GEOM131 011830
GEOM132 011840
GEOM133 011850
GEOM134 011860
GEOM135 011870
GEOM136 011880
GEOM137 011890
GEOM138 011900
GEOM139 011910
GEOM140 011920
GEOM141 011930
GEOM142 011940
GEOM143 011950
GEOM144 011960
GEOM145 011970
GEOM146 011980
GEOM147 011990
GEOM148 012000
GEOM149 012010
GEOM150 012020
GEOM151 012030
GEOM152 012040
GEOM153 012050
GEOM154 012060
GEOM155 012070
GEOM156 012080
GEOM157 012090
GEOM158 012100
GEOM159 012110
GEOM160 012120
GEOM161 012130
GEOM162 012140
GEOM163 012150
GEOM164 012160
GEOM165 012170
GEOM166 012180
GEOM167 012190
GEOM168 012200
GEOM169 012210
GEOM170 012220
GEOM171 012230
GEOM172 012240
GEOM173 012250
GEOM174 012260
GEOM175 012270
GEOM176 012280
GEOM177 012290
GEOM178 012300
GEOM179 012310
GEOM180 012320

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      IF (A.LT.O.) LIMR=ICOL*K
180  IF (LIMXL.LT.1) LIMXL=1
      IF (LIMR.GT.NXX) LIMR=NXX
      IF (LIMXL.GT.LIMR) GO TO 200
      C  ASSUME 10000. IS LARGE ENOUGH TO YIELD PK=1. FOR ALL KILL CRITERIA
      DO 190 J=LIMB,LIMT
      DO 190 I=LIMXL,LIMR
      C 190 PERF(I,J)=10000.
      C
      IF (VOID2.EQ.O) GO TO 200
      VOID2=O
      GO TO 210
200  IF (VOID2.EQ.O) CALL BLANK
210  ICOL=ICOL-1
      GO TO 300
      C
      C  ENTRY B1SID
      C  THIS ENTRY HANDLES A SINGLE SIDE WHERE THE JUNCTION OF THAT SIDE
      C  WITH THE TOP IS PARALLEL TO THE X AXIS. IN THIS ENTRY, BETA
      C  IS POSITIVE (NEGATIVE) WHEN THE OUTWARD DRAWN NORMAL TO THE SIDE
      C  HAS A COMPONENT IN THE POSITIVE (NEGATIVE) Y DIRECTION.
      C
      IROW=IROW+1
      JFSTA=1
      JLISTB=NY
      COSB8=CCSB
      SINB8=SINB
      XF (B.GT.C.) GO TO 220
      COSB8=-COSB8
      SINB8=-SINB8
220  IF (NNSPRA.GT.C) GO TO 230
      VOID2=1
      GO TO 300
230  VAL=O.
      IF (ABS(ABS(B)-9C.).GT..COC1) VAL=H/(2.*TANB)
      IVAL=VAL
      F=IVAL
      IF (F.NE.VAL.AND.(9C.-ABS(B).GT..COC1.AND.H.GE.C..OR.ABS(B)-90..GT
1..COC1.AND.H.LT.C.)) GO TO 240
      IVAL=IVAL-1
      IF (B.LT.O.) IVAL=IVAL+2
240  IF (B.GT.C..AND.IVAL+IROW.LT.NY) JLISTB=IVAL+IROW
      IF (B.LT.O..AND.IVAL+IROW.GT.1) JFSTA=IVAL+IROW
      IF (JLISTB.GE.1.AND.JFSTA.LE.NY) GO TO 250
      VOID2=2
      GO TO 300
      C
      C  JJ SPECIFIES THE ROW BOUNDARY AT WHICH THE TOP EDGE OF THE SIDE
      C  LOCATED. THE ROW BOUNDARY NUMBERED *K* IS ON THE LCM ORDER SIDE
      C  OF ROW K.
250  IF (H.GE.C..OR.ABS(B)-90..LT..COC1) GO TO 260
      IF (JLISTB.GT.IROW.AND.B.GT.C.) JLISTB=IROW
      IF (JFSTA.LT.IROW.AND.B.LT.C.) JFSTA=IROW
      IF (JFSTA.LE.JLISTB) GO TO 260
      VOID2=2
      GO TO 300
260  JJ=JFSTA,JLISTB
      YY=2*(J-IROW)
      GO 200 II=1,NXX
      GEOM181 012330
      GEOM182 012340
      GEOM183 012350
      GEOM184 012360
      GEOM185 012370
      GEOM186 012380
      GEOM187 012390
      GEOM188 012400
      GEOM189 012410
      GEOM190 012420
      GEOM191 012430
      GEOM192 012440
      GEOM193 012450
      GEOM194 012460
      GEOM195 012470
      GEOM196 012480
      GEOM197 012490
      GEOM198E 012500
      GEOM199 012510
      GEOM200 012520
      GEOM201 012530
      GEOM202 012540
      GEOM203 012550
      GEOM204 012560
      GEOM205 012570
      GEOM206 012580
      GEOM207 012590
      GEOM208 012600
      GEOM209 012610
      GEOM210 012620
      GEOM211 012630
      GEOM212 012640
      GEOM213 012650
      GEOM214 012660
      GEOM215 012670
      GEOM216 012680
      GEOM217 012690
      GEOM218 012700
      GEOM219 012710
      GEOM220 012720
      GEOM221 012730
      GEOM222 012740
      GEOM223 012750
      GEOM224 012760
      GEOM225 012770
      GEOM226 012780
      GEOM227 012790
      GEOM228 012800
      GEOM229 012810
      GEOM230 012820
      GEOM231 012830
      GEOM232 012840
      GEOM233 012850
      GEOM234 012860
      GEOM235 012870
      GEOM236 012880
      GEOM237 012890
      GEOM238 012900
      GEOM239 012910
      GEOM240 012920

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AD-A068 976

ARMY MATERIEL SYSTEMS ANALYSIS ACTIVITY ABERDEEN PROV--ETC F/G 19/3
LIGHTLY ARMORED STRUCTURE VULNERABILITY ESTIMATION METHODOLOGY --ETC(U)
JAN 79 C J LAPOINTE

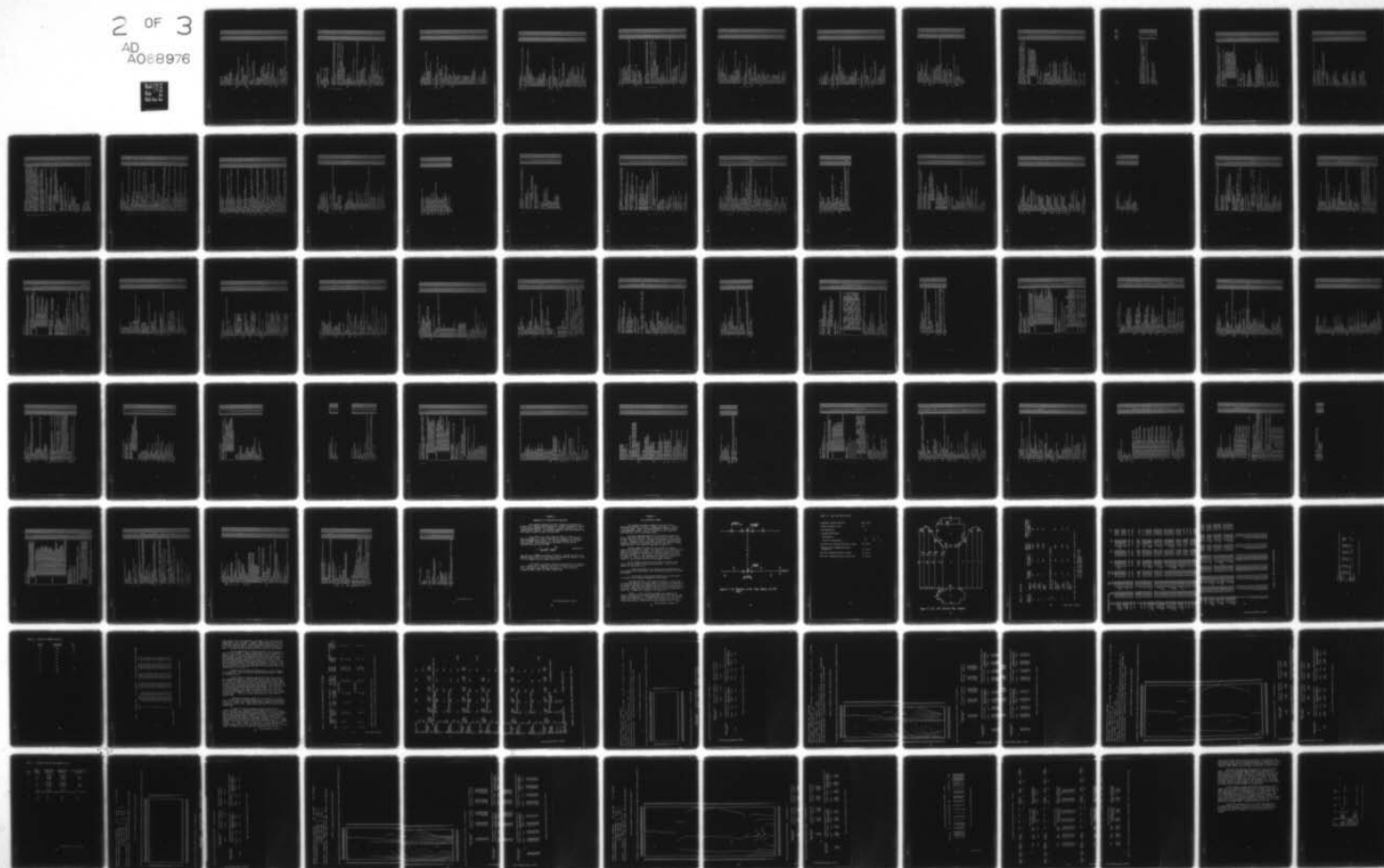
UNCLASSIFIED

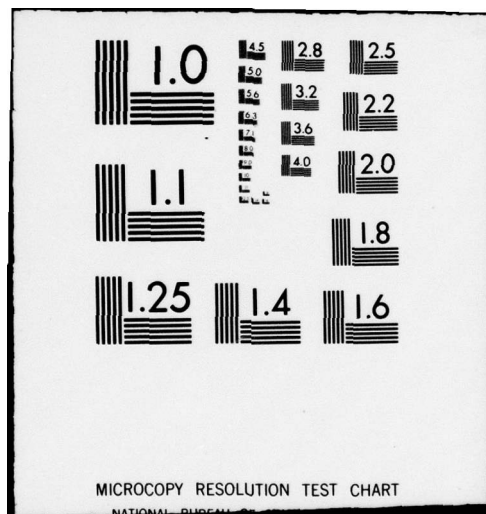
AMSAA-TR-254

NL

2 OF 3

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X=2*(II-ICOL)-1
PRFK=0.
DO 270 K=1,NZ
FK=2*K-1
Y=YY+FK*QCSB8
Z=H-FK*SINB6
R2=X**2+Y**2+Z**2
R=SQRT(R2)
ETA=-Z*CSB-Y*SINB
THETA=(X*CSB-Z*SINW)/R
STER=4.*ETA/(R2*R)
C
CALL DAME
C
270 PRFK=PRFK+PRF1
280 PERF(II,JJ)=PRFK/2.
IF (JFSTA.EQ.1.AND.JLSTB.EQ.NYY) GO TO 300
JJ1=1
JJ2=NY
IF (JFSTA.NE.1) JJ2=JFSTA-1
IF (JLSTB.NE.NYY) JJ1=JLSTB+1
DO 290 JJ=JJ1,JJ2
DO 290 II=1,NXX
290 PERF(II,JJ)=0.
300 IF (H.GT.EPSLN.OR.ABS(B)-90..GT..0001) GO TO 360
C
PROJECTILE IMPACT ON PLATE
FNZ=NZ
F=EPSLN/2.
IF (H.GT.0.) F=SQRT(EPSLN**2-H**2)/2.
IF (AINT(F).NE.F.OR.F.EQ.0.) F=F+1.
K=F
LIMXL=ICOL-K
LIMXR=ICOL+K
LIMYB=IRON-K
LIMY=IRON+K
IF (LIMXL.LT.1) LIMXL=1
IF (LIMXR.GT.NXX) LIMXR=NXX
IF (LIMXL.GT.LIMXR) GO TO 360
IF (90.-ABS(B)).LE..0001) GO TO 340
TEMP1=EPSLN*CSB
TEMP2=2.*FNZ*SINPB
IF (H.LT.TEMP1-TEMP2) GO TO 310
F=(TEMP1-H)/ABS(TANB)+EPSLN*SINBB
GO TO 330
310 TEMP1=2.*FNZ*CSB
IF (H.LT.-TEMP2) GO TO 320
F=TEMP1+SQRT(EPSLN**2-(TEMP2+H)**2)
GO TO 330
320 F=TEMP1+EPSLN
330 F=F/2.
IF (AINT(F).NE.F) F=F+1.
K=F
IF (B.GT.0.) LIMYB=IRON-K
IF (B.LT.0.) LIMY=IRON+K
340 IF (LIMYB.LT.1) LIMYB=1
IF (LIMY.GT.NYY) LIMY=NY
IF (LIMYB.GT.LIMY) GO TO 360
ASSUME 10000. IS LARGE ENOUGH TO YIELD PK=1. FOR ALL KILL CRITERIA
OL 550 I=LIMXL,LIMXR
GEOM241 012930
GEOM242 012940
GEOM243 012950
GEOM244 012960
GEOM245 012970
GEOM246 012980
GEOM247 012990
GEOM248 013000
GEOM249 013010
GEOM250 013020
GEOM251 013030
GEOM252 013040
GEOM253 013050
GEOM254 013060
GEOM255 013070
GEOM256 013080
GEOM257 013090
GEOM258 013100
GEOM259 013110
GEOM260 013120
GEOM261 013130
GEOM262 013140
GEOM263 013150
GEOM264 013160
GEOM265 013170
GEOM266 013180
GEOM267 013190
GEOM268 013200
GEOM269 013210
GEOM270 013220
GEOM271 013230
GEOM272 013240
GEOM273 013250
GEOM274 013260
GEOM275 013270
GEOM276 013280
GEOM277 013290
GEOM278 013300
GEOM279 013310
GEOM280 013320
GEOM281 013330
GEOM282 013340
GEOM283 013350
GEOM284 013360
GEOM285 013370
GEOM286 013380
GEOM287 013390
GEOM288 013400
GEOM289 013410
GEOM290 013420
GEOM291 013430
GEOM292 013440
GEOM293 013450
GEOM294 013460
GEOM295 013470
GEOM296 013480
GEOM297 013490
GEOM298 013500
GEOM299 013510
GEOM300 013520

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```

      DO 350 J=LIMYB,LIMYT
      350 PERF(I,J)=IC000C.
      C
      IF (VOID2.EQ.C) GO TO 360
      GO TO 370
      360 IF (VOID2.EQ.C) CALL BLANK
      370 IKW=IKW-1
      380 IF (VOID2.EQ.O) CALL SUMP
      IF (VOID2.NE.O) CALL VOID
      RETURN
      C
      C
      ENTRY AZSID
      THIS ENTRY HANDLES TWO SIDES WHERE THEIR JUNCTION WITH THE TOP IS
      PARALLEL TO THE Y AXIS. IN THIS ENTRY, ALPHA AND FNK ARE ALWAYS
      GREATER THAN ZERO.
      C
      C
      HLFXA AND HLFXB DEFINE THE CENTER OF THE ASSEMBLY IN THE MANNER
      USED BY SUBROUTINE SUMP.
      C
      IFSTA IS THE FIRST II FOR WHICH SIDE A CONTRIBUTES. ILSTB IS THE
      LAST II FOR WHICH SIDE B CONTRIBUTES.
      C
      SIDE A HAS A NORMAL WITH A COMPONENT IN THE -X DIRECTION AND
      SIDE B, IN THE +X DIRECTION
      C
      IF (INSPRA.GT.O) GO TO 390
      VOID2=1
      GO TO 530
      390
      ILFXA=2*(NX/2)+1
      HLFXA=ILFXA
      ILFXB=2*(NX-NX/2)-1
      HLFXB=ILFXB
      VAL=C.
      IF (ABS(A-90.)>.0001) VAL=H/(2.*TANA)
      IF (VAL=VAL)
      F=IVAL
      IF (F.NE.VAL.AND.(90.-A.GT..COOL.AND.H.6E.C..OR.A-9C..6T..0001.AND.GEOM336
      1.H.LT.O.)) GO TO 400
      IVAL=IVAL-1
      IFSTA=ICGL-IVAL+NX/2+1
      IF (IFSTA.LT.1) IFSTA=1
      ILSTB=ICGL-IVAL+NX/2+1
      IF (ILSTB.GT.NX) ILSTB=NKX
      IF (IFSTA.LE.NXK.OR.ILSTB.GE.1) GO TO 410
      VOID2=2
      GO TO 530
      C
      C
      ONLY B CONTRIBUTES
      410
      ISTOP=IFSTA-1
      IF (IFSTA.GT.ILSTB) ISTOP=ILSTB
      IF (H.LT.C..AND.ISTOP.GT.ICGL-NX+NX/2+1) ISTOP=ICGL-NX+NX/2+1
      IF (ISTOP.LT.1) GO TO 440
      LOOP ON X COORDINATE OF TARGET CENTER
      DO 430 II=1,ISTOP
      XXB=2*(II-ICGL)-1+ILFXB
      LOOP ON Y COORDINATE OF STRIP OF CELLS IN SLAB
      DO 430 JJ=1,NY
      Y=2*(JJ-IROW)-1
      LOOP ON ALL CELLS IN STRIP
      PRFK=C.
      DO 420 K=1,NZ

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      GEM301 013530
      GEM302 013540
      GEM303 013550
      GEM304 013560
      GEM305 013570
      GEM306 013580
      GEM307 013590
      GEM308 013600
      GEM309 013610
      GEM310 013620
      GEM311 013630
      GEM312 013640
      GEM313 013650
      GEM314E 013660
      GEM315 013670
      GEM316 013680
      GEM317 013690
      GEM318 013700
      GEM319 013710
      GEM320 013720
      GEM321 013730
      GEM322 013740
      GEM323 013750
      GEM324 013760
      GEM325 013770
      GEM326 013780
      GEM327 013790
      GEM328 013800
      GEM329 013810
      GEM330 013820
      GEM331 013830
      GEM332 013840
      GEM333 013850
      GEM334 013860
      GEM335 013870
      GEM336 013880
      GEM337 013890
      GEM338 013900
      GEM339 013910
      GEM340 013920
      GEM341 013930
      GEM342 013940
      GEM343 013950
      GEM344 013960
      GEM345 013970
      GEM346 013980
      GEM347 013990
      GEM348 014000
      GEM349 014010
      GEM350 014020
      GEM351 014030
      GEM352 014040
      GEM353 014050
      GEM354 014060
      GEM355 014070
      GEM356 014080
      GEM357 014090
      GEM358 014100
      GEM359 014110
      GEM360 014120

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```

C
  FK=2*K-1
  XB=XB+FK*COXA
  Z=-H-FK*SINA
  RB2=XB**2+Y**2+Z**2
  RB=SQRT(RB2)
  RB*COSETAI, ETA=ANGLE BETWEEN RB AND CELL NORMAL
  ETA=-Z*COXA-XB*SINA
  THETA=(XB*COSW-Z*SINW)/RB
  STEP=4.*ETA/(RB2*RB)
  GEOMETRY FOR THIS CELL IS COMPLETE
C
  CALL DAME
C
  420 PRF=PRF+PRF1
  430 PERF(II,JJ)=PRF/2.
  REGION IN WHICH ONLY B CONTRIBUTES IS DONE
C
  BOTH A AND B CONTRIBUTE
  440 IF (H.LT.0.) GO TO 45C
  IF (IFSTA.LE.ILSTB) GO TO 47C
  450 II=ILSTB+1
  IF (II.LT.1) II=1
  IF (IFSTA.GT.NXX+1) IFSTA=NXX+1
  IF (II.EQ.IFSTA) GO TO 50C
  I2=IFSTA-1
  DO 460 II=1,I2
  DO 460 JJ=1,NYY
  460 PERF(II,JJ)=Q.
  GO TO 50C
  470 DO 490 II=IFSTA,ILSTB
  XX=2*(II-ICOLI)-1
  XXA=XX-HLFXA
  XKB=XX+HLFXB
  DO 49C JJ=1,NYY
  Y=2*(JJ-IROW)-1
  PRF=C.
  DO 480 K=1,NZ
  FK=2*K-1
  XB=XB+FK*COXA
  XA=XA-FK*COXA
  Z=-H-FK*SINA
  YZ2=Y**2+Z**2
  RB2=XB**2+YZ2
  RA2=XA**2+YZ2
  SIDE B
  RB=SQRT(RB2)
  ETA=-Z*COXA-XB*SINA
  THETA=(XB*COSW-Z*SINW)/RB
  STEP=4.*ETA/(RB2*RB)
  CALL DAME
C
  PRF=PRF+PRF1
  SIDE A
  RA=SQRT(RA2)
  ETA=XA*SINA-Z*COXA
  THETA=(XA*COSW-Z*SINW)/RA
  STEP=4.*ETA/(RA2*RA)
  CALL DAME
C

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```

GEOM361 014130
GEOM362 014140
GEOM363 014150
GEOM364 014160
GEOM365 014170
GEOM366 014180
GEOM367 014190
GEOM368 014200
GEOM369 014210
GEOM370 014220
GEOM371 014230
GEOM372 014240
GEOM373 014250
GEOM374 014260
GEOM375 014270
GEOM376 014280
GEOM377 014290
GEOM378 014300
GEOM379 014310
GEOM380 014320
GEOM381 014330
GEOM382 014340
GEOM383 014350
GEOM384 014360
GEOM385 014370
GEOM386 014380
GEOM387 014390
GEOM388 014400
GEOM389 014410
GEOM390 014420
GEOM391 014430
GEOM392 014440
GEOM393 014450
GEOM394 014460
GEOM395 014470
GEOM396 014480
GEOM397 014490
GEOM398 014500
GEOM399 014510
GEOM400 014520
GEOM401 014530
GEOM402 014540
GEOM403 014550
GEOM404 014560
GEOM405 014570
GEOM406 014580
GEOM407 014590
GEOM408 014600
GEOM409 014610
GEOM410 014620
GEOM411 014630
GEOM412 014640
GEOM413 014650
GEOM414 014660
GEOM415 014670
GEOM416 014680
GEOM417 014690
GEOM418 014700
GEOM419 014710
GEOM420 014720

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C 480 PRFK=PRFK+PREI
C 490 PERF(11,JJ)=PRFK/2.
C THIS FINISHES THE REGION IN WHICH BOTH A AND B CONTRIBUTE.
C
C ONLY A CONTRIBUTES
C 500 ISTR=ILSTB+1
IF (IFSTA.GT.ILSTB) ISTR=IFSTA
IF (H.LT.O..AND.ISTR.LT.ICOL+NX/2+1) ISTR=ICOL+NX/2+1
IF (ISTR.GT.NXX) GO TO 530
DO 520 II=ISTR,NXX
XIA=2*(II-ICOL)-1-ILFXA
DO 520 JJ=1,NYY
YI2*(JJ-IROW)-1
PRFK=0.
DO 510 K=1,NZ
FK=2*K-1
XA=XA-FK*COXA
Z=-H-FK*SINA
KA2=XA**2+YI**2+Z**2
RA=SQRT(RA2)
ETA=XA*SINA-Z*COXA
THETA=(XA*COXW-Z*SINW)/RA
STER=4*ETA/(RA2*RA)
C CALL DAMAGE
C
C 510 PRFK=PRFK+PREI
C 520 PERF(11,JJ)=PRFK/2.
C
C 530 IF (H.GT.EPSLN-OR.A-90..GT..G001.) GO TO 860
IF (VOID2.EQ.0) GO TO 550
DO 540 I=1,NXX
DO 540 J=1,NYY
C 540 PERF(I,J)=C.
C
C PROJECTILE IMPACT ON SIDES
C
C 550 FNZ=NZ
F=EPSLN/2.
IF (H.GT.O.) F=SQRT(EPSLN**2-H**2)/2.
IF (AINT(F).NE.F.DR.F.ER.O.) F=F+1.
K=F
JSTR=IROW-K
JSTOP=IPOM+K
ISTCP=ICOL+K-NX+NX/2+1
KSTR=ICOL-K+NX/2+1
IF (JSTR.LT.1) JSTR=1
IF (JSTOP.GT.NYY) JSTOP=NYY
IF (JSTR.GT.JSTOP) GO TO 86C
IF (IC-A.LE..QCOL) GO TO 590
TEMP1=EPSLN*COXA
TEMP2=2.*FNZ*SINA
IF (H.LT.TEMP1-TEMP2) GO TO 560
F=(TEMP1-H)/TANA+EPSLN*SINA
GO TO 56C
C 56C TEMP1=2.*FNZ*COXA
IF (H.LT.-TEMP2) GO TO 57C
F=TEMP1+SQRT(EPSLN**2-(TEMP2+H)**2)
GO TO 56C
C 57C F=TEMP1+EPSLN

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GEOM421 C14730
GEOM422 C14740
GEOM423 C14750
GEOM424 C14760
GEOM425 C14770
GEOM426 C14780
GEOM427 C14790
GEOM428 C14800
GEOM429 C14810
GEOM430 C14820
GEOM431 C14830
GEOM432 C14840
GEOM433 C14850
GEOM434 C14860
GEOM435 C14870
GEOM436 C14880
GEOM437 C14890
GEOM438 C14900
GEOM439 C14910
GEOM440 C14920
GEOM441 C14930
GEOM442 C14940
GEOM443 C14950
GEOM444 C14960
GEOM445 C14970
GEOM446 C14980
GEOM447 C14990
GEOM448 C15000
GEOM449 C15010
GEOM450 C15020
GEOM451 C15030
GEOM452 C15040
GEOM453 C15050
GEOM454 C15060
GEOM455 C15070
GEOM456 C15080
GEOM457 C15090
GEOM458 C15100
GEOM459 C15110
GEOM460 C15120
GEOM461 C15130
GEOM462 C15140
GEOM463 C15150
GEOM464 C15160
GEOM465 C15170
GEOM466 C15180
GEOM467 C15190
GEOM468 C15200
GEOM469 C15210
GEOM470 C15220
GEOM471 C15230
GEOM472 C15240
GEOM473 C15250
GEOM474 C15260
GEOM475 C15270
GEOM476 C15280
GEOM477 C15290
GEOM478 C15300
GEOM479 C15310
GEOM480 C15320

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580 F=F/2.
   IF (AINT(F).NE.F) F=F+1.
   K=F
590 ISTRT=ICOL-K-NX+NY/2+1
   IF (ISTRT.LT.1) ISTRT=1
   IF (JSTOP.GT.NX) JSTOP=NX
   KSTOP=ICOL+K+NX/2+1
   IF (KSTRT.LT.1) KSTRT=1
   IF (KSTOP.GT.NX) KSTOP=NX
   C ASSUME 10000. IS LARGE ENOUGH TO YIELD PK=1. FOR ALL KILL CRITERIA
   IF (ISTRT.GT.JSTOP) GO TO 610
   C SIDE B
   DO 600 J=JSTRT,JSTOP
   DO 600 I=ISTRT,ISTOP
   600 PERF(I,J)=10000.
   610 IF (KSTRT.GT.KSTOP) GO TO 860
   C SIDE A
   DO 620 J=JSTRT,JSTOP
   DO 620 K=KSTRT,KSTOP
   620 PERF(K,J)=10000.
   GO TO 870
   C
   C
   C ENTRY B2SID
   C THIS ENTRY HANDLES TWO SIDES WHERE THEIR JUNCTION WITH THE TOP IS
   C PARALLEL TO THE X AXIS. IN THIS ENTRY, BETA AND FNY ARE ALWAYS
   C GREATER THAN ZERO.
   C
   C HLFYA AND HLFYB DEFINE THE CENTER OF THE ASSEMBLY IN THE MANNER
   C USED BY SUBROUTINE SUMPF.
   C JFSTA IS THE FIRST JJ FOR WHICH SIDE A CONTRIBUTES. JLSB IS THE
   C LAST JJ FOR WHICH SIDE B CONTRIBUTES.
   C SIDE A HAS A NORMAL WITH A COMPONENT IN THE -X DIRECTION AND
   C SIDE B, IN THE +X DIRECTION
   C IF (MNSPRA.GT.0) GO TO 630
   VOID2=1
   GO TO 77C
   630 ILFYA=2*(NY/2)+1
   HLFYA=ILFYA
   ILFYB=2*(NY-NY/2)-1
   HLFYB=ILFYB
   VAL=G.
   IF (ABS(B-90.)*.GT..0001) VAL=H/(2.*TANB)
   IVAL=VAL
   F=IVAL
   IF (F.NE.VAL.AND.(90.-B.GT..COCL.AND.H.GE.0..OR.B-90..GT..COCL.AND
   1.H.LT.0.)) GO TO 640
   IVAL=IVAL-1
   640 JFSTA=IFOW-IVAL+NY/2+1
   IF (JFSTA.LT.1) JFSTA=1
   JLSB=IFOW+IVAL-NY+NY/2+1
   IF (JLSB.GT.NY) JLSB=NY
   C IF (JFSTA.LE.NY.OR.JLSB.GE.1) GO TO 650
   VOID2=2
   GO TO 77C
   C ONLY B CONTRIBUTES
   650 JSTOP=JFSTA-1
   IF (JFSTA.GT.JLSB) JSTOP=JLSB
   IF (H.LT.C..AND.JSTOP.GT.16CN-NY+NY/2+1) JSTOP=16CN-NY+NY/2+1

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```

GEOM481 01533C
GEOM482 01534C
GEOM483 01535C
GEOM484 01536C
GEOM485 01537C
GEOM486 01538C
GEOM487 01539C
GEOM488 01540C
GEOM489 01541C
GEOM490 01542C
GEOM491 01543C
GEOM492 01544C
GEOM493 01545C
GEOM494 01546C
GEOM495 01547C
GEOM496 01548C
GEOM497 01549C
GEOM498 01550C
GEOM499 01551C
GEOM500 01552C
GEOM501 01553C
GEOM502 01554C
GEOM503 01555C
GEOM504 01556C
GEOM505 01557C
GEOM506 01558C
GEOM507 01559C
GEOM508 01560C
GEOM509 01561C
GEOM510 01562C
GEOM511 01563C
GEOM512 01564C
GEOM513 01565C
GEOM514 01566C
GEOM515 01567C
GEOM516 01568C
GEOM517 01569C
GEOM518 01570C
GEOM519 01571C
GEOM520 01572C
GEOM521 01573C
GEOM522 01574C
GEOM523 01575C
GEOM524 01576C
GEOM525 01577C
GEOM526 01578C
GEOM527 01579C
GEOM528 01580C
GEOM529 01581C
GEOM530 01582C
GEOM531 01583C
GEOM532 01584C
GEOM533 01585C
GEOM534 01586C
GEOM535 01587C
GEOM536 01588C
GEOM537 01589C
GEOM538 01590C
GEOM539 01591C
GEOM540 01592C

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```

C      IF (JSTCP.LT.1) GO TO 66C
C      LOOP ON Y COORDINATE OF TARGET CENTER
C      DO 670 JJ=1,JSTCP
C      YYB=2*(JJ-IRDM)-1+ILFYB
C      LOOP ON X COORDINATE OF STRIP OF CELLS IN SLAB
C      DO 670 II=1,NXX
C      X=2*(II-ICOL)-1
C      LOOP ON ALL CELLS IN STRIP
C      PRFK=0.
C      DO 66C K=1,NZ
C      FK=2*K-1
C      YB=YYB+FK*CCSB
C      Z=H-FK*SINB
C      RB2=YB**2+X**2+Z**2
C      RB=SQRT(RB2)
C      RB=COS(ETA), ETA=ANGLE BETWEEN RB AND CELL NORMAL
C      ETA=-Z*CCSB-YB*SINB
C      THETA=(X*CCSB-Z*SINW)/RB
C      STEP=4.*ETA/(RB2*RB)
C      GEOMETRY FOR THIS CELL IS COMPLETE
C      CALL DANGE
C      660 PRFK=PRFK+PRFK1
C      670 PERF(II,JJ)=PRFK/2.
C      REGION IN WHICH ONLY B CONTRIBUTES IS DONE
C      C
C      BOTH A AND B CONTRIBUTE
C      680 IF (H.LT.C.) GO TO 69C
C      IF (JFSTA.LE.JLSTB) GO TO 710
C      690 J1=JLSTB+1
C      IF (J1.LT.1) J1=1
C      IF (JFSTA.GT.NY+1) JFSTA=NY+1
C      IF (J1.EQ.JFSTA) GO TO 740
C      J2=JFSTA-1
C      DO 700 JJ=J1,J2
C      DO 700 II=1,NXX
C      700 PERF(II,JJ)=C.
C      GO TO 740
C      710 DO 730 JJ=JFSTA,JLSTB
C      YY=2*(JJ-IRDM)-1
C      YYA=YY-HLFYA
C      YB=YY+HLFYB
C      DO 730 II=1,NXX
C      X=2*(II-ICOL)-1
C      PRFK=C.
C      DO 720 K=1,NZ
C      FK=2*K-1
C      YB=YYB+FK*CCSB
C      YA=YYA-FK*CCSB
C      Z=H-FK*SINB
C      XL2=X**2+Z**2
C      R62=YB**2+XZ2
C      R42=YA**2+XZ2
C      THET=X*CCSB-Z*SINW
C      SIDE B
C      RB=SQRT(RB2)
C      ETA=-Z*CCSB-YB*SINB
C      THETA=THET/RB
C      STEP=4.*ETA/(R62*RB)

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GEOM541 015930
GEOM542 015940
GEOM543 015950
GEOM544 015960
GEOM545 015970
GEOM546 015980
GEOM547 015990
GEOM548 016000
GEOM549 016010
GEOM550 016020
GEOM551 016030
GEOM552 016040
GEOM553 016050
GEOM554 016060
GEOM555 016070
GEOM556 016080
GEOM557 016090
GEOM558 016100
GEOM559 016110
GEOM560 016120
GEOM561 016130
GEOM562 016140
GEOM563 016150
GEOM564 016160
GEOM565 016170
GEOM566 016180
GEOM567 016190
GEOM568 016200
GEOM569 016210
GEOM570 016220
GEOM571 016230
GEOM572 016240
GEOM573 016250
GEOM574 016260
GEOM575 016270
GEOM576 016280
GEOM577 016290
GEOM578 016300
GEOM579 016310
GEOM580 016320
GEOM581 016330
GEOM582 016340
GEOM583 016350
GEOM584 016360
GEOM585 016370
GEOM586 016380
GEOM587 016390
GEOM588 016400
GEOM589 016410
GEOM590 016420
GEOM591 016430
GEOM592 016440
GEOM593 016450
GEOM594 016460
GEOM595 016470
GEOM596 016480
GEOM597 016490
GEOM598 016500
GEOM599 016510
GEOM600 016520

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C      CALL DANGE
C      PRFK=PRFK+PRF1
C      SIDE A
C      RA=SQRT(RA2)
C      ETA=YA*SINB-Z*CCSB
C      THETA=THET/RA
C      STER=4.*ETA/(RA2*RA)
C      CALL DANGE
C      720 PRFK=PRFK+PRF1
C      730 PERF(II,JJ)=PRFK/2.
C      THIS FINISHES THE REGION IN WHICH BOTH A AND B CONTRIBUTE.
C
C      740 ONLY A CONTRIBUTES
C      JSTRT=JLSTB+1
C      IF (JFSTA.GT.JLSTB) JSTRT=JFSTA
C      IF (H.LT.O..AND..JSTRT.LT.IROW+NY/2+1) JSTRT=IROW+NY/2+1
C      IF (JSTRT.GT.NY) GO TO 77C
C      DO 760 JJ=JSTRT,NY
C      YYA=2*(JJ-IROW)-1-ILFYA
C      DO 760 II=1,NXX
C      X=2*(II-ICOL)-1
C      PRFK=C.
C      DO 750 K=1,NZ
C      FK=2*K-1
C      YA=YA-FK*CCSB
C      Z=-H-FK*SINB
C      RA2=YA**2+X**2+Z**2
C      RA=SQRT(RA2)
C      ETA=YA*SINB-Z*CCSB
C      THETA=(X*CCSB-Z*SINB)/RA
C      STER=4.*ETA/(RA2*RA)
C      CALL DANGE
C      750 PRFK=PRFK+PRF1
C      760 PERF(II,JJ)=PRFK/2.
C      77C IF (H.GT.EPSLN.GR.8-90..GT..COOL) GO TO 880
C      IF (VOID2.EQ.O) GO TO 790
C      DO 780 I=1,NXX
C      DO 780 J=1,NY
C      780 PERF(II,J)=C.
C
C      PROJECTILE IMPACT ON SIDES
C      790 FNZ=Z
C      F=EPSLN/2.
C      IF (H.GT.G.) F=SQRT(EPSLN**2-H**2)/2.
C      IF (AINT(F).NE.F.OR.F.EQ.O.) F=F+1.
C      K=F
C      IJSTRT=ICOL-K
C      IJSTOP=ICOL+K
C      JSTCP=IROW+K-NY+NY/2+1
C      KJSTRT=IROW-K+NY/2+1
C      IF (IJSTRT.LT.1) IJSTRT=1
C      IF (IJSTOP.GT.NXX) IJSTOP=NXX
C      IF (IJSTRT.GT.IJSTOP) GO TO 88C

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GECM601 016530
GECM602 01654C
GECM603 016550
GECM604 016560
GECM605 016570
GECM606 01658C
GECM607 016590
GECM608 016600
GECM609 016610
GECM610 016620
GECM611 016630
GECM612 01664C
GECM613 016650
GECM614 01666C
GECM615 016670
GECM616 016680
GECM617 016690
GECM618 016700
GECM619 016710
GECM620 01672C
GECM621 016730
GECM622 01674C
GECM623 016750
GECM624 016760
GECM625 016770
GECM626 01678C
GECM627 016790
GECM628 016800
GECM629 016810
GECM630 016820
GECM631 016830
GECM632 016840
GECM633 016850
GECM634 01686C
GECM635 016870
GECM636 01688C
GECM637 01689C
GECM638 016900
GECM639 016910
GECM640 01692C
GECM641 016930
GECM642 016940
GECM643 01695C
GECM644 01696C
GECM645 01697C
GECM646 01698C
GECM647 01699C
GECM648 01700C
GECM649 017010
GECM650 01702C
GECM651 01703C
GECM652 01704C
GECM653 01705C
GECM654 01706C
GECM655 01707C
GECM656 01708C
GECM657 01709C
GECM658 01710C
GECM659 01711C
GECM660 01712C

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IF (90.-B.LE.C0C1) GO TO 830
TEMP1=EPSLN*CSB
TEMP2=2.*FNZ*SINB
IF (H.LI.-TEMP2) GO TO 800
F=(TEMP1-H)/TANB+EPSLN*SINB
GO TO 820
800 TEMP1=2.*FNZ*CSB
IF (H.LI.-TEMP2) GO TO 810
F=TEMP1+EPSLN*(TEMP2+H)**2)
GO TO 820
810 F=TEMP1+EPSLN
820 F=F/2.
IF (AINT(F).NE.F) F=F+1.
K=F
830 JSTRT=IRON-K-NY+NY/2+1
KSTOP=IRON+K+NY/2+1
IF (JSTRT.LI.1) JSTRT=1
IF (JSTOP.GT.NY) JSTOP=NY
IF (KSTRT.LI.1) KSTRT=1
IF (KSTOP.GT.NY) KSTOP=NY
C ASSUME 1000. IS LARGE ENOUGH TO YIELD PK=1. FOR ALL KILL CRITERIA
C IF (JSTRT.GT.JSTOP) GO TO 850
C SIDE B
DO 840 I=JSTRT,ISTOP
DC 840 J=JSTRT,JSTOP
840 PERF(I,J)=10000.
850 IF (KSTRT.GT.KSTOP) GO TO 860
C SIDE A
DO 860 I=JSTRT,ISTOP
DC 860 K=KSTRT,KSTOP
860 PERF(I,K)=10000.
C
C ALL LOCATIONS OF THE SLAB (PAIR) ARE DONE
870 VOIDZ=0
880 IF (VOIDZ.NE.C) GO TO 910
890 CALL BLANK
900 IF (VLCID2.NE.C) GO TO 910
CALL SUMFF
RETURN
910 CALL VOID
RETURN
END

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GECM601 C1713C
GECM602 C1714C
GECM603 C1715C
GECM604 C1716C
GECM605 C1717C
GECM606 C1718C
GECM607 C1719C
GECM608 C1720C
GECM609 C1721C
GECM610 C1722C
GECM611 C1723C
GECM612 C1724C
GECM613 C1725C
GECM614 C1726C
GECM615 C1727C
GECM616 C1728C
GECM617 C1729C
GECM618 C1730C
GECM619 C1731C
GECM620 C1732C
GECM621 C1733C
GECM622 C1734C
GECM623 C1735C
GECM624 C1736C
GECM625 C1737C
GECM626 C1738C
GECM627 C1739C
GECM628 C1740C
GECM629 C1741C
GECM630 C1742C
GECM631 C1743C
GECM632 C1744C
GECM633 C1745C
GECM634 C1746C
GECM635 C1747C
GECM636 C1748C
GECM637 C1749C
GECM638 C1750C
GECM639 C1751C
GECM640 C1752C
GECM641 C1753C
GECM642 C1754C

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1745	7	0.1755C
GOTHU 2		0.1756B
GOTHU 3		0.1757C
GOTHU 4		0.1758D
GOTHU 5		0.1759D
GOTHU 6		0.1760D
GOTHU 7		0.1761D
GOTHU 8		0.1762D
GOTHU 9		0.1763D
GOTHU10		0.1764D
GOTHU11		0.1765D
GOTHU12		0.1766D
GOTHU13		0.1767D
GOTHU14		0.1768D
GOTHU15		0.1769D
GOTHU16		0.1770D
GOTHU17		0.1771C
GOTHU18		0.1772D
GOTHU19		0.1773D
GOTHU20		0.1774D
GOTHU21		0.1775C
GOTHU22		0.1776C
GOTHU23		0.1777D
GOTHU24		0.1778D
GOTHU25		0.1779C
GOTHU26		0.1780D
GOTHU27		0.1781D
GOTHU28		0.1782D
GOTHU29		0.1783D
GOTHU30		0.1784D
GOTHU31		0.1785D
GOTHU32		0.1786D
GOTHU33		0.1787D
GOTHU34		0.1788D
GOTHU35		0.1789D
GOTHU36		0.1790C
GOTHU37		0.1791C
GOTHU38		0.1792D
GOTHU39		0.1793D
GOTHU40		0.1794C
GOTHU41		0.1795C
GOTHU42		0.1796D
GOTHU43		0.1797D
GOTHU44		0.1798C
GOTHU45		0.1799D
GOTHU46		0.1800D
GOTHU47		0.1801D
GOTHU48		0.1802C
GOTHU49		0.1803D
GOTHU50		0.1804C
GOTHU51		0.1805D
GOTHU52		0.1806D
GOTHU53		0.1807C
GOTHU54		0.1808C
GOTHU55		0.1809C
GOTHU56		0.1810C
GOTHU57		0.1811D
GOTHU58		0.1812D
GOTHU59		0.1813C
GOTHU60		0.1814C

GOTHU61 C1815C
GOTHU62 C1816C
GOTHU63- C18170

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SUBROUTINE DAME
C THIS SUBROUTINE GETS THE PERFORATIONS ON EACH CELL. M AND VDN
C ARE THEIR OWN LOGARITHMS. VIMPCT IS THE (LOGARITHM OF THE)
C VELOCITY WITH WHICH THE FRAGMENT STRIKES THE PLATE.
C
COMMON /COM3/COM3(10000)
DIMENSION SPRBD(92),VDYN(92),M(40,46),Q(40,46),SGDIN(92)
1 XREF(3680)
EQUIVALENCE (COM3(47),SPRBD(1)),(COM3(231),VDYN(1))
1 (COM3(369),M(1,1)),(COM3(2209),Q(1,1))
2 (COM3(4095),SGDIN(1)),(COM3(4713),XREF(1))
3 (COM3(9939),NNSPRA),(COM3(9946),GAMAV)
4 (COM3(9951),GAMAM),(COM3(9952),LAMDAM)
5 (COM3(9953),CNST1),(COM3(9954),CNST3V)
6 (COM3(9955),CNST4V),(COM3(9956),CNST5V)
7 (COM3(9958),CNST4M),(COM3(9959),CNST5M)
8 (COM3(9993),R),(COM3(9994),THETA),(COM3(9995),STER)
9 (COM3(9996),PRF1),(COM3(9999),ETA)
C
COMMON /THOR70/RATION,RATIOV
C
INTEGER XREF
REAL LAMDAM,M,MLOSS
C
DATA TEN / .461568834/
TEN=10.**(-1./3.)
C
PRF1=0.
TEMP3=ALOG10(R/ETA)
CNST5V=CNST4V+GAMAV*TEMP3
CNST5M=CNST4M+GAMAM*TEMP3
CNST6=CNST1*R
C
KI=0
10 KI=KI+1
CALL GET (XREF(KI),K1,K2,K3)
20 IF (THETA.GT.SPRBD(K3).GR.THETA.LE.SPRBD(K3+1)) GO TO 40
VIMPCT=VDYN(K3)+CNST6*TEMP3*(K1,K2)
VLOSS=CNST5V+CNST3V*M(K1,K2)*RATIOV
MLOSS=CNST5M+LAMDAM*VIMPCT+RATIOV
IF (VLOSS.GE.VIMPCT.OR.MLOSS.GE.M(K1,K2)) GO TO 40
PRF1=PRF1+SGDIN(K3)*STER*(K1,K2)
IF (KI.LT.NNSPRA) GO TO 10
30 RETURN
C
40 IF (KI.EQ.NNSPRA) GO TO 30
KI=KI
KI=KI+1
50 KI=KI+1
CALL GET (XREF(KI),K1,K2,K3)
IF (K31.EQ.K3) GO TO 60
K3=K31
KI=KI
GO TO 20
60 IF (KI1.LT.NNSPRA) GO TO 50
GO TO 30
END

```

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C          SUEFLUTINE BLANK
C          THIS SUBROUTINE ELIMINATES FROM CONSIDERATION THAT PORTION OF THE
C          PERFORM ARRAY WHICH IS VOID
C
C          COMMON /COM1/COM1(20100)
C          DIMENSION PERF(100,100)
C          EQUIVALENCE (COM1(1),PERF(1,1))
C
C          COMMON /COM3/COM3(10000)
C          EQUIVALENCE (COM3(9979),LIMXL),(COM3(9980),LIMXR)
C          1      , (COM3(9981),LIMYB),(COM3(9982),LIMYT)
C
C          COMMON /NXXNY/NXX,NYY
C          COMMON /VOID2/VOID2
C          INTEGER VOID2
C
C          SUM=0.
C          DO 20 LIMXL=1,NXX
C          DO 10 JJ=1,NYY
C          10      SUM=SUM+PERF(LIMXL,JJ)
C          20      CONTINUE
C          VOID2=1
C          RETURN
C
C          30      SUM=C.
C          DO 50 K=LIMXL,NXX
C          LIMXR=NXX-K+LIMXL
C          DO 40 JJ=1,NYY
C          40      SUM=SUM+PERF(LIMXR,JJ)
C          50      CONTINUE
C
C          60      SUM=0.
C          DO 80 LIMYB=1,NYY
C          DO 70 II=LIMXL,LIMXR
C          70      SUM=SUM+PERF(II,LIMYB)
C          IF (SUM.NE.0.) GO TO 90
C          80      CONTINUE
C
C          90      SUM=0.
C          DO 110 K=LIMYB,NYY
C          LIMYT=NYY-K+LIMYB
C          DO 100 II=LIMXL,LIMXR
C          100      SUM=SUM+PERF(II,LIMYT)
C          IF (SUM.NE.0.) RETURN
C          110      CONTINUE
C          END

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*1681*10  C18910
BLANK 2  C18920
BLANK 3  C18930
BLANK 4  C18940
BLANK 5  C18950
BLANK 6  C18960
BLANK 7  C18970
BLANK 8  C18980
BLANK 9  C18990
BLANK 10 C19000
BLANK 11 C19010
BLANK 12 C19020
BLANK 13 C19030
BLANK 14 C19040
BLANK 15 C19050
BLANK 16 C19060
BLANK 17 C19070
BLANK 18 C19080
BLANK 19 C19090
BLANK 20 C19100
BLANK 21 C19110
BLANK 22 C19120
BLANK 23 C19130
BLANK 24 C19140
BLANK 25 C19150
BLANK 26 C19160
BLANK 27 C19170
BLANK 28 C19180
BLANK 29 C19190
BLANK 30 C19200
BLANK 31 C19210
BLANK 32 C19220
BLANK 33 C19230
BLANK 34 C19240
BLANK 35 C19250
BLANK 36 C19260
BLANK 37 C19270
BLANK 38 C19280
BLANK 39 C19290
BLANK 40 C19300
BLANK 41 C19310
BLANK 42 C19320
BLANK 43 C19330
BLANK 44 C19340
BLANK 45 C19350
BLANK 46 C19360
BLANK 47 C19370
BLANK 48 C19380
BLANK 49- C19390

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SUBROUTINE SUMPF
C THE GEOMETRY AND DAMAGE SUBROUTINES HAVE PRODUCED THE PERFORATION
C ARRAY. IF THE TARGET WAS A FLAT PLATE, THE INFORMATION CONTAINED
C THEREIN IS THE NUMBER OF PERFORATIONS SUSTAINED BY EACH CELL OF A
C LARGE FLAT PLATE. IF THE TARGET WAS ONE OR TWO SLANTED SIDES, THEN
C THIS INFORMATION IS THE TOTAL NUMBER OF PERFORATIONS SUSTAINED BY
C THE SIDE(S) WHEN THE LENGTH (DIMENSION) ALONG THE JUNCTION BETWEEN
C THE SIDE(S) AND THE TOP) OF THE TARGET IS ONLY ONE CELL, FOR EACH
C POSITION OF THIS TARGET'S CENTER. THIS SUBROUTINE SUMS THE TOTAL
C INFORMATION AND PRODUCES THE LAMBDA ARRAY WHICH CONTAINS THE TOTAL
C NUMBER OF PERFORATIONS SUSTAINED BY THE ENTIRE TARGET FOR EACH
C POSITION OF THE TARGET CENTER. NOTE THAT 'TARGET', AS USED AT THIS
C POINT, REALLY ADDRESSES A PIECE OF A COMPLETE TARGET.
C
C FOR TARGETS WHICH EXHIBIT SYMMETRY ACROSS THE ROW BOUNDARY IN
C WHICH THE PROJECTILE IS IMBEDDED, THE SYMMETRY IS UTILIZED TO
C OBTAIN THE CONTRIBUTION OF THAT PART OF THE TARGET WHICH EXTENDS
C INTO 'ROWS' NUMBERED LESS THAN 1.
C
C II AND JJ LOCATE THE TARGET CENTER, DEFINED AS NX/2+1,NY/2+1, ON
C THE GRID. III, JJJ PICK OUT GRID COLUMNS AND ROWS.
C
COMMON /COM1/COM1(20100)
DIMENSION PERF(100,100),LAMBDA(100,100),SUM(100,100)
EQUIVALENCE (COM1(1),PERF(1,1)),LAMBDA(1,1)),(COM1(10001),SUM(1,1))
C
COMMON /COM3/COM3(10000)
EQUIVALENCE (COM3(9965),NX), (COM3(9966),NY), (COM3(9969),A)
1 , (COM3(9970),B), (COM3(9979),LIMXL), (COM3(9980),LIMXR)
2 , (COM3(9981),LIMYB), (COM3(9982),LIMYT)
3 , (COM3(9988),IFLAG)
C
COMMON /COLROW/ICOL, IROW, ICOLL, IROWL
COMMON /LYMIT/LYMXL, LYMYB, LYMYT
COMMON /NXXNY/NXX,NYY
C
INTEGER SNUM1,SNUM2,SNUM3,SNUM4,SNUM5,SNUM6
REAL LAMBDA,LAMDE
C
IF (B.EQ.C..AND.NY.GT.1) GO TO 30
LYMYB=LIMYB
LYMYT=LIMYT
IF (B.EQ.C..AND.A.NE.C.) GO TO 20
DO 10 JJ=LYMYB,LYMYT
DO 10 IC=LYMXL,LIMXR
10 SUM(II,JJ)=PERF(II,JJ)
20 GO TO 250
LYMXL=LIMXL
LYMYB=LIMYB
RETURN
C
30 NY2=NY/2
TARGET MID ROW
NYMID=NY2+1
TARGET TOP ROW IS NYTOP ROWS ABOVE NYMID. TARGET BOTTOM ROW IS NY2
ROWS BELOW NYMID
NYTOP=NY-NYMID
BOUNDARIES FOR MOVEMENT OF TARGET MID ROW FROM BOTTOM TO TOP OF
ARRAY

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```

*1930*11
C1940C
C19410
C19420
C19430
C19440
C19450
C19460
C19470
C19480
C19490
C19500
C19510
C19520
C19530
C19540
C19550
C19560
C19570
C19580
C19590
C19600
C19610
C19620
C19630
C19640
C19650
C19660
C19670
C19680
C19690
C19700
C19710
C19720
C19730
C19740
C19750
C19760
C19770
C19780
C19790
C19800
C19810
C19820
C19830
C19840
C19850
C19860
C19870
C19880
C19890
C19900
C19910
C19920
C19930
C19940
C19950
C19960
C19970
C19980
C19990

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LYMB=LYMB-NYTOP
IF (LYMB.LT.1.AND.IROW.NE.C) FLAG=IFLAG+4
LYMT=LYMT-NY2
IF (LYMT.LE.NY) GO TO 40
IFLAG=IFLAG+8
LYMT=NY
C VARIOUS SUMMATION LIMITS
C LOCATION OF TARGET TOP ROW WHEN TARGET MID ROW IS JUST BELOW ARRAY
C ROW 1
40 LIM1=NYTOP
C AVOID SUMMING ZEROS
C IF (LIM1.GT.LIMY) LIM1=LIMY
C LOCATION OF TARGET MID ROW WHEN TARGET BOTTOM ROW IS IN LIMYB
C LIM2=LIMY+NY2
C NO STORAGE BEYOND ARRAY LIMITS
C IF (LIM2.GT.NY) LIM2=NY
C FIRST STORAGE OF LAMDE OCCURS IN THIS TARGET MID ROW POSITION
C LIM3=LYMB
C NO STORAGE BEYOND ARRAY LIMITS
C IF (LYMB.LT.1) LIM3=1
C LOCATION OF TARGET MID ROW WHEN TARGET TOP ROW IS IN LIMY
C LIM4=LYMT-NYTOP
C IF LIM5(=LIM2).GT.LIM4, THE TARGET TOP ROW WILL BE BEYOND LIMY
C WHEN THE TARGET BOTTOM ROW IS IN LIMYB
C LIM5=LIM2
C IF (LIM5.GT.LIM4) LIM5=LIM4
C LIM6=LIM5+1
C IF (LYMB.LT.1.AND.LIM1.EQ.LIMY) LIM6=1
C LIM7=LIM2+1
C IF (LIM5.LT.LIM4.AND.(LYMB.GT.0.OR.LIM1.LT.LIMY)) LIM7=LIM4+1
C FOLLOWING 2 LIMITS ARE USED FOR SYMMETRY
C LIM8=2*IROW+1
C LIM9=2*IROW+NY2
C IF (LIM9.GT.LIMY) LIM9=LIMY
C LIMC=NYMID-LIM9+2*IROW-1
C SET UP LOGIC
C ASSIGN 120 TO SNUM1
C IF (LYMB.GT.0) GO TO 50
C LYMB.LT.1 MEANS THAT, WHEN SUMMING STARTS, NO STORAGE OF LAMDE
C WILL OCCUR BECAUSE THE TARGET MID ROW WILL NOT BE WITHIN THE ARRAY
C ASSIGN 100 TO SNUM1
C ASSIGN 120 TO SNUM2
C IF (LIM1.LT.LIMY) GO TO 50
C LIM1=LYMT MEANS THAT THERE ARE NO MORE NON-ZERO ARRAY ROWS TO
C BE SUMMED
C ASSIGN 160 TO SNUM2
C GO TO 60
50 ASSIGN 140 TO SNUM3
C LIM5.LT.LIM4 MEANS THAT THE TARGET BOTTOM ROW IS IN LIMYB BEFORE
C THE TARGET TOP ROW REACHES LIMY
C IF (LIM5.LT.LIM4) GO TO 60
C ASSIGN 160 TO SNUM3
C IF (LIM5.LT.LIM2) GO TO 60
C LIM5=LYMT MEANS THAT THE TARGET BOTTOM ROW REACHES LIMYB AS THE
C TARGET TOP ROW REACHES LIMY
C ASSIGN 180 TO SNUM3
C IF (LIM7.LE.NY) GO TO 70
C LIM7.GT.NY MEANS THAT THERE IS NO MORE SPACE AVAILABLE FOR
C STORAGE, SO WE MOVE ON TO SYMMETRY
C ASSIGN 200 TO SNUM3

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SUMPF61 020000
SUMPF62 020010
SUMPF63 020020
SUMPF64 020030
SUMPF65 020040
SUMPF66 020050
SUMPF67 020060
SUMPF68 020070
SUMPF69 020080
SUMPF70 020090
SUMPF71 020100
SUMPF72 020110
SUMPF73 020120
SUMPF74 020130
SUMPF75 020140
SUMPF76 020150
SUMPF77 020160
SUMPF78 020170
SUMPF79 020180
SUMPF80 020190
SUMPF81 020200
SUMPF82 020210
SUMPF83 020220
SUMPF84 020230
SUMPF85 020240
SUMPF86 020250
SUMPF87 020260
SUMPF88 020270
SUMPF89 020280
SUMPF90 020290
SUMPF91 020300
SUMPF92 020310
SUMPF93 020320
SUMPF94 020330
SUMPF95 020340
SUMPF96 020350
SUMPF97 020360
SUMPF98 020370
SUMPF99 020380
SUMPF100 020390
SUMP101 020400
SUMP102 020410
SUMP103 020420
SUMP104 020430
SUMP105 020440
SUMP106 020450
SUMP107 020460
SUMP108 020470
SUMP109 020480
SUMP110 020490
SUMP111 020500
SUMP112 020510
SUMP113 020520
SUMP114 020530
SUMP115 020540
SUMP116 020550
SUMP117 020560
SUMP118 020570
SUMP119 020580
SUMP120 020590

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C      LIMB-ET-LIMYT MEANS THAT WHAT WE WOULD PICK UP DUE TO SYMMETRY IS
C      BEYOND THE ARRAY LIMITS
C      IF (LIMB-LE-LIMYT) GO TO 8C
C      ASSIGN 24C TO SNUM3
C      GO TO 9C
C      60  ASSIGN 16C TO SNUM4
C      IF (LIM7-LE-NYI) GO TO 7C
C      LIM7-GT-NYI MEANS THAT THERE IS NO MORE SPACE AVAILABLE FOR
C      STORAGE, SO WE MOVE ON TO SYMMETRY
C      ASSIGN 20C TO SNUM4
C      LIMB-GT-LIMYT MEANS THAT WHAT WE WOULD PICK UP DUE TO SYMMETRY IS
C      BEYOND THE ARRAY LIMITS
C      IF (LIMB-LE-LIMYT) GO TO 8C
C      ASSIGN 24C TO SNUM4
C      GO TO 9C
C      70  ASSIGN 20C TO SNUM5
C      LIMB-GT-LIMYT MEANS THAT WHAT WE WOULD PICK UP DUE TO SYMMETRY IS
C      BEYOND THE ARRAY LIMITS
C      IF (LIMB-LE-LIMYT) GO TO 8C
C      ASSIGN 24C TO SNUM5
C      GO TO 9C
C      80  ASSIGN 22C TO SNUM6
C      IF (LIM10-LT-1) ASSIGN 24C TO SNUM6
C      DO THE SUPMATION FOR EACH CONTRIBUTING ARRAY COLUMN
C      90  DO 240 II=LIMXL,LIMXR
C      LAMDE=0.
C      GO TO SNUM1, (130+12C)
C      100 DO 110 JJ=LIMYB,LIM1
C      DO THAT PART OF THE SUMMATION FOR WHICH NO STORAGE OF LAMDE OCCURS
C      BECAUSE THE TARGET MID ROW IS BELOW ARRAY ROW 1
C      110 LAMDE=LAMDE+PERF(II,JJ)
C      GO TO SNUM2, (120+16C)
C      120 DO 130 JJ=LIM3,LIM5
C      SUCCESSIVE ARRAY ROWS .LE-LIMYT ARE COVERED BUT NONE .GE-LIMYB ARE
C      UNCOVERED AS THE TARGET MOVES UPWARD. STORAGE OF LAMDE OCCURS.
C      LAMDE=LAMDE+PERF(II,JJ+NYTDF)
C      130 SUM(II,JJ)=LAMDE
C      GO TO SNUM3, (140+16C+20C+24C)
C      140 DO 150 JJ=LIM6,LIM4
C      AS THE TARGET MOVES UPWARD, THE TARGET TOP ROW COVERS ONE AND THE
C      TARGET BOTTOM ROW UNCOVERS ANOTHER NON-ZERO ARRAY ROW. STORAGE OF
C      LAMDE OCCURS.
C      LAMDE=LAMDE+PERF(II,JJ+NYTDF)-PERF(II,JJ-NYMTD)
C      IF (LAMDE-LT-0.) LAMDE=0.
C      150 SUM(II,JJ)=LAMDE
C      GO TO SNUM4, (160+20C+24C)
C      160 DO 170 JJ=LIM6,LIM2
C      ALL NON-ZERO ARRAY ROWS REMAIN COVERED AS THE TARGET MOVES UPWARD
C      170 SUM(II,JJ)=LAMDE
C      GO TO SNUM4, (180+20C+24C)
C      180 DO 19C JJ=LIM7,LIMT
C      TARGET BOTTOM ROW UNCOVERS NON-ZERO ARRAY ROWS AS THE TARGET MOVES
C      UPWARD. TARGET TOP ROW IS BEYOND LIMIT. STORAGE OF LAMDE OCCURS.
C      LAMDE=LAMDE+PERF(II,JJ-NYMTD)
C      IF (LAMDE-LT-0.) LAMDE=0.
C      190 SUM(II,JJ)=LAMDE
C      GO TO SNUM5, (20C+24C)
C      ALL FOR SYMMETRY ABOUT THE ROW BOUNDARY IN WHICH THE PROJECTILE
C      IS IMBEDDED. NOTE THAT THIS IS ALLOWED ONLY FOR A FLAT TARGET OR
C      FOR ONE OF TWO SIDES WHOSE JUNCTION WITH THE TOP IS IN THE Y

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020600  SUMP121
020610  SUMP122
020620  SUMP123
020630  SUMP124
020640  SUMP125
020650  SUMP126
020660  SUMP127
020670  SUMP128
020680  SUMP129
020690  SUMP130
020700  SUMP131
020710  SUMP132
020720  SUMP133
020730  SUMP134
020740  SUMP135
020750  SUMP136
020760  SUMP137
020770  SUMP138
020780  SUMP139
020790  SUMP140
020800  SUMP141
020810  SUMP142
020820  SUMP143
020830  SUMP144
020840  SUMP145
020850  SUMP146
020860  SUMP147
020870  SUMP148
020880  SUMP149
020890  SUMP150
020900  SUMP151
020910  SUMP152
020920  SUMP153
020930  SUMP154
020940  SUMP155
020950  SUMP156
020960  SUMP157
020970  SUMP158
020980  SUMP159
020990  SUMP160
021000  SUMP161
021010  SUMP162
021020  SUMP163
021030  SUMP164
021040  SUMP165
021050  SUMP166
021060  SUMP167
021070  SUMP168
021080  SUMP169
021090  SUMP170
021100  SUMP171
021110  SUMP172
021120  SUMP173
021130  SUMP174
021140  SUMP175
021150  SUMP176
021160  SUMP177
021170  SUMP178
021180  SUMP179
021190  SUMP180

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C      DIRECTION.
C      200  LAMDE=0.
C      210  JJ=JJ+LIM5*LIM9
C      211  LAMDE=LAMDE+PERF(I,J,JJ)
C      212  JJ=NYMID-JJJ+2*IRON
C      213  SUM(II,JJ)=SUM(II,JJ)+LAMDE
C      214  GO TO SNUM6, (220,240)
C      220  DO 230 JJ=1,LIM1
C      230  SUM(II,JJ)=SUM(II,JJ)+LAMDE
C      240  CONTINUE
C
C      IF (LYMYB.LT.1) LYMYB=1
C
C      THIS PART OF THE SUBROUTINE IS ANALOGOUS TO THE PRECEEDING EXCEPT
C      THAT SYMMETRY IS NOT CONSIDERED
C      250  IF (A.EC.C.AND.NX.GT.1) GO TO 270
C      LYMXL=LIMXL
C      LYPXR=LIMXR
C      DO 260 JJ=LYMYB,LYMYT
C      260  II=LYMXL,LYMYR
C      LAMDA(II,JJ)=SUM(II,JJ)
C      RETURN
C
C      270  NX2=NX/2
C      NXPID=NX2+1
C      NXRIT=NX-NXMID
C      LYMXL=LIMXL-NXRIT
C      IF (LYMXL.LT.1) IFLAG=IFLAG+1
C      LYPXR=LIMXR+NX2
C      IF (LYMYR.LE.NXX) GO TO 280
C      IFLAG=IFLAG+2
C      LYMXR=NX
C
C      280  LIM1=NXRIT
C      IF (LIM1.GT.LIMXK) LIM1=LIMXR
C      LIM2=LIMXL+NX2
C      IF (LIM2.GT.NXX) LIM2=NX
C      LIM3=LYMXL
C      IF (LYMXL.LT.1) LIM3=1
C      LIM4=LIMXR-NXRIT
C      LIM5=LIM2
C      IF (LIM5.GT.LIM4) LIM5=LIM4
C      LIM6=LIM5+1
C      IF (LYMXL.LT.1.AND.LIM1.EQ.LIMXK) LIM6=1
C      LIM7=LIM2+1
C      IF (LIM5.LT.LIM4.AND.(LYMXL.GT.C.OR.LIM1.LT.LIMXR)) LIM7=LIM4+1
C      ASSIGN 340 TO SNUM1
C      IF (LYMXL.GT.0) GO TO 290
C      ASSIGN 320 TO SNUM1
C      ASSIGN 340 TO SNUM2
C      IF (LIM1.LT.LIPXR) GO TO 290
C      ASSIGN 380 TO SNUM2
C      GO TO 300
C      290  ASSIGN 360 TO SNUM3
C      IF (LIM1.LT.LIP4) GO TO 300
C      ASSIGN 360 TO SNUM3
C      IF (LIM5.LT.LIM2) GO TO 300
C      ASSIGN 400 TO SNUM3
C      IF (LIM7.GT.PXX) ASSIGN 420 TO SNUM3
C      GO TO 310

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SUMP181 0212CC
SUMP182 02121C
SUMP183 02122C
SUMP184 02123C
SUMP185 02124C
SUMP186 02125C
SUMP187 02126C
SUMP188 02127C
SUMP189 02128C
SUMP190 02129C
SUMP191 02130C
SUMP192 02131C
SUMP193 02132C
SUMP194 02133C
SUMP195 02134C
SUMP196 02135C
SUMP197 02136C
SUMP198 02137C
SUMP199 02138C
SUMP200 02139C
SUMP201 02140C
SUMP202 02141C
SUMP203 02142C
SUMP204 02143C
SUMP205 02144C
SUMP206 02145C
SUMP207 02146C
SUMP208 02147C
SUMP209 02148C
SUMP210 02149C
SUMP211 02150C
SUMP212 02151C
SUMP213 02152C
SUMP214 02153C
SUMP215 02154C
SUMP216 02155C
SUMP217 02156C
SUMP218 02157C
SUMP219 02158C
SUMP220 02159C
SUMP221 02160C
SUMP222 02161C
SUMP223 02162C
SUMP224 02163C
SUMP225 02164C
SUMP226 02165C
SUMP227 02166C
SUMP228 02167C
SUMP229 02168C
SUMP230 02169C
SUMP231 02170C
SUMP232 02171C
SUMP233 02172C
SUMP234 02173C
SUMP235 02174C
SUMP236 02175C
SUMP237 02176C
SUMP238 02177C
SUMP239 02178C
SUMP240 02179C

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300 ASSIGN 400 TO SNUM4
   IF (LIM7.GT.NXX) ASSIGN 420 TO SNUM4
310 DO 420 JJ=LYMY8,LYMYT
    LAMDE=0.
    GO TO SNUM1, (320,340)
320 DO 330 III=LIMXL,LIM1
330 LAMDE=LAMDE+SUM(III,JJ)
    GO TO SNUM2, (340,360)
340 DO 350 II=LIM3,LIM5
    LAMDE=LAMDE+SUM(II+NXRIT,JJ)
350 LAMDA(II,JJ)=LAMDE
    GO TO SNUM3, (360,380,400,420)
360 DO 370 II=LIM6,LIM4
    LAMDE=LAMDE+SUM(II+NXRIT,JJ)-SUM(II-NXMID,JJ)
    IF (LAMDE.LT.0.) LAMDE=0.
370 LAMDA(II,JJ)=LAMDE
    GO TO SNUM4, (400,420)
380 DO 390 II=LIM6,LIM2
390 LAMDA(II,JJ)=LAMDE
    GO TO SNUM4, (400,420)
400 DO 410 II=LIM7,LYMYR
    LAMDE=LAMDE-SUM(II-NXMID,JJ)
    IF (LAMDE.LT.0.) LAMDE=0.
410 LAMDA(II,JJ)=LAMDE
420 CONTINUE
    RETURN
    IF (LYMYXL.LT.1) LYMYXL=1
END

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SUMP241 021800
SUMP242 021810
SUMP243 021820
SUMP244 021830
SUMP245 021840
SUMP246 021850
SUMP247 021860
SUMP248 021870
SUMP249 021880
SUMP250 021890
SUMP251 021900
SUMP252 021910
SUMP253 021920
SUMP254 021930
SUMP255 021940
SUMP256 021950
SUMP257 021960
SUMP258 021970
SUMP259 021980
SUMP260 021990
SUMP261 022000
SUMP262 022010
SUMP263 022020
SUMP264 022030
SUMP265 022040
SUMP266 022050
SUMP267 022060
SUMP268- 022070

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114


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SUBROUTINE PAIR
C THIS SUBROUTINE PIECES TOGETHER 2 EXPECTED PERFORATIONS MATRICES
C EACH REPRESENTING A HALF-INFINITE PLANE) TO OBTAIN A COMPLETE
C MATPIX
C
COMMON /COM1/COM1(20100)
DIMENSION LAMDA2(100,100),LAMDA1(100,100)
EQUIVALENCE (COM1(1),LAMDA2(1,1)),(COM1(10001),LAMDA1(1,1))
C
COMMON /COM3/COM3(10000)
DIMENSION FILE2(7),SHFTX2(7),SHFTY2(2)
EQUIVALENCE (COM3(8439),FILE2(1)),(COM3(8440),SHFTX2(1))
1 EQUIVALENCE (COM3(8453),SHFTY2(1))
C
COMMON /DISC/DISC(15016)
EQUIVALENCE (DISC(15010),NFILE),(DISC(15012),PTAPE1)
C
COMMON /CELL/CELL
COMMON /COLROW/ICOL,IRON,ICOLL,IRON1
COMMON /CONSTT/CONSTT(6)
EQUIVALENCE (CONSTT(5),DIMX),(CONSTT(6),DIMY)
COMMON /HOB/HOB,NHOB,HOB
COMMON /KSYM/KSYM
COMMON /LOMIT/LOMIXL,LOMYR
COMMON /LYMIT/LYMXL,LYMYR,LYMYB,LYMYT
COMMON /SHIFTS/FILE(7),SHFTX(7),SHFTY(7)
C
EQUIVALENCE (SLIP1,SLIP2,ITEMP),(SLIP3,SLIP4)
C
INTEGER DIMX,DIMY,FILE,FILE2,PTAPE1,SHFTX,SHFTY,SHFTX2,SHFTY2
1 ,SLIPX1,SLIPX2,SLIPY2,SLIP1,SLIP2,SLIP3,SLIP4
REAL LAMDA1,LAMDA2
C
REFLECT THE SECOND HALF OF THE PAIR THROUGH THE PROJECTIONS
C TRAJECTORY
NFILE2=NFILE
DO 10 I=1,NFILE2
FILE2(I)=FILE(I)
SHFTX2(I)=SHFTX(I)
10 SHFTY2(I)=SHFTY(I)
C
SLIPX2=ICOL-ICOLL
SLIPY2=0
IF (SLIP4,LT,C) SLIP4=0
IF (SLIPX2) 30,50,20
C
20 IF (SLIPX2.LE.SLIP4) GO TO 40
SLIP1=1-LOMYL
IF (SLIP1.GT.0) SLIP1=C
SLIPX1=SLIP4-SLIPX2
SLIPY1=SLIP4
IF (SLIPX1.GE.SLIP1) GO TO 40
SLIPX1=SLIP1
SLIPY1=ICOL-ICOLL+SLIP1
GO TO 40
C
30 SLIP2=1-LYMXL
IF (SLIP2.GT.C) SLIP2=C
IF (SLIPX2.GE.SLIP2) GO TO 40

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*2235*13 022450
PAIR 2 022460
PAIR 3 022470
PAIR 4 022480
PAIR 5 022490
PAIR 6 022500
PAIR 7 022510
PAIR 8 022520
PAIR 9 022530
PAIR 10 022540
PAIR 11 022550
PAIR 12 022560
PAIR 13 022570
PAIR 14 022580
PAIR 15 022590
PAIR 16 022600
PAIR 17 022610
PAIR 18 022620
PAIR 19 022630
PAIR 20 022640
PAIR 21 022650
PAIR 22 022660
PAIR 23 022670
PAIR 24 022680
PAIR 25 022690
PAIR 26 022700
PAIR 27 022710
PAIR 28 022720
PAIR 29 022730
PAIR 30 022740
PAIR 31 022750
PAIR 32 022760
PAIR 33 022770
PAIR 34 022780
PAIR 35 022790
PAIR 36 022800
PAIR 37 022810
PAIR 38 022820
PAIR 39 022830
PAIR 40 022840
PAIR 41 022850
PAIR 42 022860
PAIR 43 022870
PAIR 44 022880
PAIR 45 022890
PAIR 46 022900
PAIR 47 022910
PAIR 48 022920
PAIR 49 022930
PAIR 50 022940
PAIR 51 022950
PAIR 52 022960
PAIR 53 022970
PAIR 54 022980
PAIR 55 022990
PAIR 56 023000
PAIR 57 023010
PAIR 58 023020
PAIR 59 023030
PAIR 60 023040

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SLIP3=DIMX-LOMXR
IF (SLIP3.LT.C) SLIP3=C
SLIPX1=SLIP2-SLIPX2
SLIPX2=SLIP2
IF (SLIPX1.LE.SLIP3) GO TO 4C
SLIPX1=SLIP3
SLIPX2=ICCL-ICOLI+SLIP3
C AT THIS POINT WE HAVE SLIPX1 AND SLIPX2
C SLIPX2 IS THE AMOUNT BY WHICH THE CURRENT ARRAY (IN LAMDA1) IS
C SHIFTED AS IT MOVES INTO LAMDA2. PART OF THIS ARRAY MAY BE CHOPPED
C OFF. SLIPX1 IS THE AMOUNT BY WHICH THE ARRAY ON TAPE WILL BE
C SHIFTED WITHIN LAMDA1 AFTER IT IS READ IN.
40 LYMNL=LYMNL+SLIPX2
LYMNR=LYMNR+SLIPX2
IF (LYMNL.LT.1) LYMNL=1
IF (LYMNR.GT.DIMX) LYMNR=DIMX
50 SLIPY2=DIMY+1+IRGM1
ITEMP=LYMYB
LYMYB=SLIPY2-LYMYT
LYMYT=SLIPY2-ITEMP
C DOESN'T MATTER IF WE SPILL OUT THE TOP HERE
DO 6C I=LYMNL,LYMNR
DO 6C J=LYMYB,LYMYT
60 LAMDA2(I,J)=LAMDA1(I-SLIPX2,SLIPY2-J)
C LOW ORDER ROWS OF THE ICX2CC ARRAY ARE IN PLACE WITH X AND Y
C LIMITS LYMNL, LYMNR, LYMYB, LYMYT
C READ IN THE HIGH ORDER ROWS WITH NO SHIFTING
READ (PTAPE1) ICGL,IRGM,LOMXL,LOMNR,LOMYB,LOMYT,NFILE,((LAMDA1(I,
1 J),I=LOMXL,LOMNR),J=LOMYB,LOMYT),(FILE(I),SHIFT(I)),I=1,
2 NFILE)
BACKSPACE PTAPE1
IF (LOMYB.LE.IRGM) LOMYB=IRGM+1
C MUST START WITH THE SIDE TOWARD WHICH WE SHIFT
IF (SLIPX1.GT.O) GO TO 8C
DO 7C I=LOMXL,LOMNR
DO 7C J=LOMYB,LOMYT
70 LAMDA1(I+SLIPX1,J-IRGM)=LAMDA1(I,J)
GO TO 10C
80 DO 9C I=LOMXL,LOMNR
I=LOMNR+LOMNL-I
DO 9C J=LOMYB,LOMYT
90 LAMDA1(I+SLIPX1,J-IRGM)=LAMDA1(I,J)
100 LOMXL=LOMXL+SLIPX1
LOMNR=LOMNR+SLIPX1
LOMYB=LOMYB-IRGM
LOMYT=LOMYT-IRGM
C BOTH PARTS OF THE LOOX2CC ARRAY ARE IN. STRAIGHTEN THE SIDES WITH
C ZERGES.
IF (LOMNL-LYMNL) 130,15C,11C
110 ITEMP=LOMNL-I
DO 12C J=LOMYB,LOMYT
DO 12C I=LYMNL,ITEMP
120 LAMDA1(I,J)=C.
GO TO 15C
130 ITEMP=LYMNL-I
DO 14C J=LYMYB,LYMYT
DO 14C I=LOMNL,ITEMP
140 LAMDA2(I,J)=C.
LYMNL=LOMNL
C LOW X SIDE IS STRAIGHT

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PAIR 61 023050
PAIR 62 02306C
PAIR 63 02307C
PAIR 64 02308C
PAIR 65 02309C
PAIR 66 02310C
PAIR 67 02311C
PAIR 68 02312C
PAIR 69 02313C
PAIR 70 02314C
PAIR 71 02315C
PAIR 72 02316C
PAIR 73 02317C
PAIR 74 02318C
PAIR 75 02319C
PAIR 76 02320C
PAIR 77 02321C
PAIR 78 02322C
PAIR 79 02323C
PAIR 80 02324C
PAIR 81 02325C
PAIR 82 02326C
PAIR 83 02327C
PAIR 84 02328C
PAIR 85 02329C
PAIR 86 02330C
PAIR 87 02331C
PAIR 88 02332C
PAIR 89 02333C
PAIR 90 02334C
PAIR 91 02335C
PAIR 92 02336C
PAIR 93 02337C
PAIR 94 02338C
PAIR 95 02339C
PAIR 96 02340C
PAIR 97 02341C
PAIR 98 02342C
PAIR 99 02343C
PAIR 100 02344C
PAIR 101 02345C
PAIR 102 02346C
PAIR 103 02347C
PAIR 104 02348C
PAIR 105 02349C
PAIR 106 02350C
PAIR 107 02351C
PAIR 108 02352C
PAIR 109 02353C
PAIR 110 02354C
PAIR 111 02355C
PAIR 112 02356C
PAIR 113 02357C
PAIR 114 02358C
PAIR 115 02359C
PAIR 116 02360C
PAIR 117 02361C
PAIR 118 02362C
PAIR 119 02363C
PAIR 120 02364C

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```

150 IF (LOMXX-LYMXR) 160,200,180
160 ITEMP=LQMXR+1
    DO 170 J=LQMYB,LQMYT
    DO 170 I=ITEMP,LYMXR
170 LAMDA2(I,J)=0.
    GO TO 200
180 ITEMP=LYMXR+1
    DO 190 J=LQMYB,LQMYT
    DO 190 I=ITEMP,LQMXR
190 LAMDA2(I,J)=0.
    LYMXR=LQMXR
    NOW WE NEED ONLY INSURE THERE IS NO GAP IN THE MIDDLE
C 200 IF (LQMYB+DIMY.EQ.LYMYT+1) GO TO 220
    LYMYT=LYMYT+1
    LQMYB=LQMYB+DIMY-1
    DO 210 I=LYMXL,LYMXR
    DO 210 J=LYMYT,LQMYB
210 LAMDA2(I,J)=0.
220 LYMYT=LQMYT+DIMY
C DONE. LIMITS ARE LYMXL, LYMXR, LYMYB, LYMYT
    ICOL1=ICOL+SLIPX1
    IFGW1=DIMY
    WRITE (PTAPE1) HOB,CELL,KSVM,ICOL1,LYMXL,LYMYB,LYMYT,
1  NFIL,((LAMDA2(I,J),I=LYMXL,LYMXR),J=LYMYB,LYMYT),(FILE1),
2  SHFTX(1),SHFTY(1),I=1,NFILE)
    WRITE (PTAPE1) NFIL2,(FILE2(I),SHFTX2(I),SHFTY2(I),I=1,NFILE2)
    RETURN
    END

```

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PAIR121 023650
PAIR122 023660
PAIR123 023670
PAIR124 023680
PAIR125 023690
PAIR126 023700
PAIR127 023710
PAIR128 023720
PAIR129 023730
PAIR130 023740
PAIR131 023750
PAIR132 023760
PAIR133 023770
PAIR134 023780
PAIR135 023790
PAIR136 023800
PAIR137 023810
PAIR138 023820
PAIR139 023830
PAIR140 023840
PAIR141 023850
PAIR142 023860
PAIR143 023870
PAIR144 023880
PAIR145 023890
PAIR146 023900
PAIR147 023910
PAIR148- 023920

```

PEKAT1	02393A
PEKAT2	02394A
PEKAT3	02395A
PEKAT4	02396A
PEKAT5	02397A
PEKAT6	02398A
PEKAT7	02399A
PEKAT8	02400A
PEKAT9	02401A
PEKAT10	02402A
PEKAT11	02403A
PEKAT12	02404A
PEKAT13	02405A
PEKAT14	02406A
PEKAT15	02407A
PEKAT16	02408A
PEKAT17	02409A
PEKAT18	02410A
PEKAT19	02411A
PEKAT20	02412A
PEKAT21	02413A
PEKAT22	02414A
PEKAT23	02415A
PEKAT24	02416A
PEKAT25	02417A
PEKAT26	02418A
PEKAT27	02419A
PEKAT28	02420A
PEKAT29	02421A
PEKAT30	02422A
PEKAT31	02423A
PEKAT32	02424A
PEKAT33	02425A
PEKAT34	02426A
PEKAT35	02427A
PEKAT36	02428A
PEKAT37	02429A
PEKAT38	02430A
PEKAT39	02431A
PEKAT40	02432A
PEKAT41	02433A
PEKAT42	02434A
PEKAT43	02435A
PEKAT44	02436A
PEKAT45	02437A
PEKAT46	02438A
PEKAT47	02439A
PEKAT48	02440A
PEKAT49	02441A
PEKAT50	02442A
PEKAT51	02443A
PEKAT52	02444A
PEKAT53	02445A
PEKAT54	02446A
PEKAT55	02447A
PEKAT56	02448A
PEKAT57	02449A
PEKAT58	02450A
PEKAT59	02451A
PEKAT60	02452A


```

          PK(IJ,JJ)=PEK
90  CONTINUE
      ASSIGN 20 TO JUMP1
100  GO TO JUMP2, (110,130)
110  DLETHL(IPNT)=AREA*(CELL*FTTOM)**2
      DRILL(IPNT)=F*GAT(IISUM)*(CELL*FTTOM)**2
      JTEMP1=JTEMP2+1
      JTEMP2=LYMYT
120  ASSIGN 130 TO JUMP2
      GO TO JUMP1, (10,20,260)
130  FSUM=ISUM
      LETHL(IPNT)=AREA*(CELL*FTTOM)**2
      KILL(IPNT)=FSUM*(CELL*FTTOM)**2
      PKAY=0.
      IF (ISUM.NE.0) PKAY=AREA/FSUM
      LAPI=ISUM
      IF (ISUM.EG.0) GO TO 260
      SUM=0.
      DO 150 LIMIT=LYMYB,LYMYT
          LIMIT4=LYMYT+LYMYB-LIMIT
          DO 140 I=LYMYL,LYMYR
              SUM=SUM+PK(I,LIMIT4)
              IF (SUM.NE.0.) GO TO 160
140  SUM=SUM+PK(I,LIMIT4)
150  CONTINUE
160  SUM=0.
      DO 180 LIMIT=LYMYL,LYMYR
          LIMIT2=LYMYR+LYMYL-LIMIT
          DO 170 J=LYMYB,LIMIT4
              SUM=SUM+PK(LIMIT2,J)
              IF (SUM.NE.0.) GO TO 190
170  SUM=SUM+PK(LIMIT2,J)
180  CONTINUE
190  SUM=C.
      DO 210 LIMIT1=LYMYL,LYMYR
          DO 200 J=LYMYB,LIMIT4
              SUM=SUM+PK(LIMIT1,J)
              IF (SUM.NE.C.) GO TO 220
200  SUM=SUM+PK(LIMIT1,J)
210  CONTINUE
220  SUM=0.
      DO 240 LIMIT3=LYMYB,LYMYT
          DO 230 I=LIMIT1,LIMIT2
              SUM=SUM+PK(I,LIMIT3)
              IF (SUM.NE.C.) GO TO 250
230  SUM=SUM+PK(I,LIMIT3)
240  CONTINUE
250  RETURN
C
260  LIMIT1=ICGL1
      LIMIT3=IRCWL1
      IF (LIMIT1.LT.1) LIMIT1=1
      IF (LIMIT3.LT.1) LIMIT3=1
      IF (LIMIT1.GT.NXX-1) LIMIT1=NXX-1
      II=NY
      IF (KSYF.EG.2) II=2*NY
      IF (LIMIT3.GT.II-1) LIMIT3=II-1
      LIMIT2=LIMIT1+1
      LIMIT4=LIMIT3+1
      GO TO 250
C
270  KRYT=KRIT(IKRIT)-1
C  LOOP ON THE TARGET CENTER POSITIONS
280  DO 320 JJ=JTEMP1,JTEMP2

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```

PEKAY61 024530
PEKAY62 024540
PEKAY63 024550
PEKAY64 024560
PEKAY65 024570
PEKAY66 024580
PEKAY67 024590
PEKAY68 024600
PEKAY69 024610
PEKAY70 024620
PEKAY71 024630
PEKAY72 024640
PEKAY73 024650
PEKAY74 024660
PEKAY75 024670
PEKAY76 024680
PEKAY77 024690
PEKAY78 024700
PEKAY79 024710
PEKAY80 024720
PEKAY81 024730
PEKAY82 024740
PEKAY83 024750
PEKAY84 024760
PEKAY85 024770
PEKAY86 024780
PEKAY87 024790
PEKAY88 024800
PEKAY89 024810
PEKAY90 024820
PEKAY91 024830
PEKAY92 024840
PEKAY93 024850
PEKAY94 024860
PEKAY95 024870
PEKAY96 024880
PEKAY97 024890
PEKAY98 024900
PEKAY99 024910
PEKAL00 024920
PEKAL01 024930
PEKAL02 024940
PEKAL03 024950
PEKAL04 024960
PEKAL05 024970
PEKAL06 024980
PEKAL07 024990
PEKAL08 025000
PEKAL09 025010
PEKAL10 025020
PEKAL11 025030
PEKAL12 025040
PEKAL13 025050
PEKAL14 025060
PEKAL15 025070
PEKAL16 025080
PEKAL17 025090
PEKAL18 025100
PEKAL19 025110
PEKAL20 025120

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```

DO 320 II=LYMXL,LYNXR
X=LAMDA(II,JJ)
IF (X.LT.675.84) GO TO 290
PEK=1.
GO TO 310
290 SUM=1.
TERM=1.
DO 300 J=1,KRYT
FJ=J
TERM=TERM*X/FJ
300 SUM=SUM+TERM
PEK=1.-EXP(-X)*SUM
IF (PEK.GE..0005) GO TO 310
PEK=0.
GO TO 320
310 ISUM=ISUM+1
AREA=AREA+PEK
320 PK(II,JJ)=PEK
GO TO 100
END

```

```

PEKA121 02513C
PEKA122 02514C
PEKA123 02515C
PEKA124 02516C
PEKA125 02517C
PEKA126 02518C
PEKA127 02519C
PEKA128 02520C
PEKA129 02521C
PEKA130 02522C
PEKA131 02523C
PEKA132 02524C
PEKA133 02525C
PEKA134 02526C
PEKA135 02527C
PEKA136 02528C
PEKA137 02529C
PEKA138 02530C
PEKA139 02531C
PEKA140- 02532C

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C SUBROUTINE OUTPUT (LAP1)
C THIS SUBROUTINE OUTPUTS THE PD MATRIX, THE LETHAL AREA, THE AREA
C IN WHICH PD IS NON ZERO (DAMAGE AREA), AND THE AVERAGE PD IN THAT
C AREA.
C
C COMMON /COM1/COM1(20100)
C DIMENSION PK(100,200)
C EQUIVALENCE (COM1(1),PK(1,1))
C
C COMMON /COM3/COM3(10000)
C DIMENSION KILL(25),DKILL(25),LETHL(25),DLETHL(25)
C EQUIVALENCE (COM3(4420),KILL(1))
C EQUIVALENCE (COM3(4445),DKILL(1)),(COM3(4470),DLETHL(1))
C EQUIVALENCE (COM3(4495),DLETHL(1)),(COM3(10000),PKAY)
C
C COMMON /COLROW/ICOL,IROW,ICOLL,IROW1
C COMMON /HOB/INHOB,NHOB,HOB
C EQUIVALENCE (INHOB,IPNT)
C COMMON /KSYM/KSYM
C COMMON /LIMIT/LIMIT1,LIMIT2,LIMIT3,LIMIT4
C EQUIVALENCE (LIMIT1,LYMXL), (LIMIT2,LYMXR), (LIMIT3,LYMYB)
C EQUIVALENCE (LIMIT4,LYMYT)
C
C 1 NOTE THAT THE 4 LYM-- VARIABLES ARE NOT THE ONES STORED IN COMMON
C COMMON /NOPK/NOPK
C COMMON /PAGE/LINES,PAGE
C COMMON /VOID2/VOID2
C
C DIMENSION IFMT1(4),IFMT2(5)
C
C INTEGER PAGE,USED,VOID2
C REAL KILL,LETHL
C
C DATA (IFMT1(1),1,1,4),10H(2H ,13,2, 2HX, ,1JH20F6.3,15)
C 1 ,1CH20F6.3,15//
C DATA (IFMT2(1),1,1,5),10H(1H ,5X ,1CH 2016 ),10H 2016 )
C 1 ,1CH(1H ,5X ,10H(1H1/ 6X, /
C
C IF (VOID2.NE.0) GO TO 90
C WRITE (6,100) LETHL(IPNT),PKAY,KILL(IPNT)
C LINES=LINES+2
C IF (KSYM.EQ.2.OR.LYMYB.GT.IROW1.OR.LYMYT.LE.IROW1) GO TO 10
C F1=LETHL(IPNT)-DLETHL(IPNT)
C F2=KILL(IPNT)-DKILL(IPNT)
C PKAY=C.
C IF (ABS(F2).GT..CC001) PKAY=F1/F2
C WRITE (6,120) F1,PKAY,F2
C LINES=LINES+4
C IF INOPK.NE.10HNC PROBABI.AND.LAP1.NE.0) GO TO 20
C 10 IF INOPK.NE.10HNC PROBABI.AND.LAP1.NE.0) GO TO 20
C WRITE (6,110)
C LINES=LINES+7
C GO TO 80
C 20 KNT=LYMYT-LYMYB+1
C KNT1=(LYMXR-LYMXL+1)/20
C KEY=LYMXR-LYMXL+1-20*KNT1
C IF (KNT1.EQ.C) GO TO 60
C DO 50 I=1,KNT1
C IF (I.EG.1) GO TO 30
C LINES=USED(LINES)
C IF (PAGE-LINES.LE.KNT+5) GO TO 30
C IFMT2(1)=IFMT1(1)

```

```

LINES=-1
30  ISTRT=LYMXL+(I-1)*20
    ISTOP=ISTRT+19
    WRITE (6,IFMT2) (IICOL,IICOL=ISTRT,ISTOP)
    IFMT2(1)=IFMT2(4)
    WRITE (6,130)
    DO 40 J=1,KNT
        IIRWM=LYMYT+1-J
        WRITE (6,IFMT1) IIRWM,(PK(IICOL,IIRWM),IICOL=ISTRT,ISTOP),IIRWM
40  CONTINUE
    WRITE (6,IFMT2) (IICOL,IICOL=ISTRT,ISTOP)
    LINES=LINES+KNT+5
50  CONTINUE
    IF (KEY.EQ.0) RETURN
    LINES=USED(LINES)
    IF (PAGE-LINES.GE.KNT+5) GO TO 60
    IFMT2(1)=IFMT2(5)
    LINES=-1
60  ISTRT=LYMXL+KNT+1*20
    ENCODE (10,140,IFMT1(3)) KEY
    ENCODE (10,150,IFMT2(2)) KEY
    WRITE (6,IFMT2) (IICOL,IICOL=ISTRT,LYMYR)
    IFMT2(1)=IFMT2(4)
    WRITE (6,130)
    DO 70 J=1,KNT
        IIRWM=LYMYT+1-J
        WRITE (6,IFMT1) IIRWM,(PK(IICOL,IIRWM),IICOL=ISTRT,LYMYR),IIRWM
70  CONTINUE
    WRITE (6,IFMT2) (IICOL,IICOL=ISTRT,LYMYR)
    LINES=LINES+KNT+5
    IFMT1(3)=IFMT1(4)
    IFMT2(2)=IFMT2(3)
80  RETURN
90  WRITE (6,160)
    LINES=LINES+7
    IF (VOID2.NE.2) GO TO 80
    WRITE (6,170)
    LINES=LINES+1
    GO TO 80

C
100 FORMAT (13H LETHAL AREA=,F7.3,14H SQUARE METERS,4X,31HAVERAGE PROB,OUTP101
    LABILITY OF DAMAGE =,F2.3,6CH OVER ,F8.3,14H SQUARE METERS,/)
110 FORMAT (///11H ,35X,62HOUTPUT OF THE PROBABILITY OF DAMAGE MATRI,OUTP103
    1X HAS BEEN SUPPRESSED)
120 FORMAT (99H CORRESPONDING VALUES FOR ONLY THE ROWS OF HIGHER ORDER,OUTP105
    1 THAN THE PROJECTILE LOCATION ARE AS FOLLOWS,14H LETHAL AREA =,F6,OUTP106
    2,2,14H SQUARE METERS,4X,31HAVERAGE PROBABILITY OF DAMAGE =,F5.3,6HOUTP107
    3 OVER ,F8.3,14H SQUARE METERS,/)
130 FORMAT (1H )
140 FORMAT (12,8HF6.3,15))
150 FORMAT (16,4HIC )
160 FORMAT (///164H THE LETHAL AREA IS ZERO BECAUSE NO PERFORATIONS ,OUTP112
    WERE SUSTAINED,/)
170 FORMAT (42H FURTHERMORE, THE PRESENTED AREA WAS ZERO,.)
    END

```

```

OUTP101 025930
OUTP102 025940
OUTP103 025950
OUTP104 025960
OUTP105 025970
OUTP106 025980
OUTP107 025990
OUTP108 026000
OUTP109 026010
OUTP110 026020
OUTP111 026030
OUTP112 026040
OUTP113 026050
OUTP114 026060
OUTP115 026070
OUTP116 026080
OUTP117 026090
OUTP118 026100
OUTP119 026110
OUTP120 026120
OUTP121 026130
OUTP122 026140
OUTP123 026150
OUTP124 026160
OUTP125 026170
OUTP126 026180
OUTP127 026190
OUTP128 026200
OUTP129 026210
OUTP130 026220
OUTP131 026230
OUTP132 026240
OUTP133 026250
OUTP134 026260
OUTP135 026270
OUTP136 026280
OUTP137 026290
OUTP138 026300
OUTP139 026310
OUTP140 026320
OUTP141 026330
OUTP142 026340
OUTP143 026350
OUTP144 026360
OUTP145 026370
OUTP146 026380
OUTP147 026390
OUTP148 026400
OUTP149 026410
OUTP150 026420
OUTP151 026430
OUTP152 026440
OUTP153 026450
OUTP154 026460
OUTP155 026470

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SUBROUTINE CONTR
C
COMMON /COM1/COM1(20100)
DIMENSION PK(100,200),PPKK(20000),KONTR(100,200),KUNTR(20000)
EQUIVALENCE (COM1(1),PK(1,1),PPKK(1),KONTR(1,1),KUNTR(1))

C
COMMON /COM3/COM3(10000)
DIMENSION PKBAR(13),RANGEM(13),DEFM(13),MIDRGM(13),MIDDFM(13)
1  ,TEMPLA(12),TEMPKA(12),FEMPKA(12),RANGEC(13),DEFEC(13)
2  ,MIDRGC(13),MIDDFC(13),BOUND(13,4),BUFFER(97),ABUFFER(97)
3  ,HEADER(124)
EQUIVALENCE (COM3(4520),PKBAR(1))
1  , (COM3(4531),RANGEM(1)), (COM3(4546),DEFM(1))
2  , (COM3(4559),MIDRGM(1)), (COM3(4572),MIDDFM(1))
3  , (COM3(4585),TEMPLA(1))
4  , (COM3(4597),TEMPKA(1),FEMPKA(1))
5  , (COM3(4609),RANGEC(1)), (COM3(4622),DEFEC(1))
6  , (COM3(4635),MIDRGC(1)), (COM3(4648),MIDDFC(1))
7  , (COM3(4661),BOUND(1,1))
8  , (COM3(4660),BUFFER(1),ABUFFER(1))
9  , (COM3(4662),HEADER(1)), (COM3(4675),IKRIT)
A  , (COM3(4677),SHELX), (COM3(4678),SHELX)

C
COMMON /DISC/DISC(15016)
DIMENSION SLIST(5002,2)
EQUIVALENCE (DISC(5005),SLIST(1,1)), (DISC(15011),NSTAPE)
1  , (DISC(15013),STAPE) , (DISC(15016),SNAME)

C
COMMON /CELL/CELL
COMMON /COLROW/ICOL, IROW, ICOLL, IROW1
COMMON /CONST/CONST(6)
EQUIVALENCE (CONST(4),FTTOP), (CONST(5),DIMX)
COMMON /HOB/INHOB, NHOB, HOB
EQUIVALENCE (INHOB, IPNT)
COMMON /KRIT/KRIT(7)
COMMON /KSYM/KSYM
COMMON /LEVEL3/LEVEL3(20000)
LEVEL 3, LEVEL3
COMMON /LIMIT/LIMIT1, LIMIT2, LIMIT3, LIMIT4
EQUIVALENCE (LIMIT1,LYMX1), (LIMIT2,LYMX2), (LIMIT3,LYMY8)
1  , (LIMIT4,LYMYT)
NOTE THAT THE 4 LYM-- VARIABLES ARE NOT THE ONES STOKED IN COMMON
COMMON /PAGE/LINES,PAGE

C
DIMENSION ALFA(13),BNND(13),BNND(14),IFMT1(2),IFMT2(17)
EQUIVALENCE (ALFA(13),BLANK), (BNND(1),BNND(2)), (ZERO)

C
INTEGER ALFA,BLANK,BOUND,BUFFER,DIMX,HEADER,PAGE,SLIST,SNAME,SPACE
1  ,STAPE,TEMPKA,TCP,USED,ZERO
REAL MIDDFC,MIDDFM,MIDRGC,MIDRGM

C
DATA (IFMT2(1),1,1,17)/1CH(
1  ,10HNTCURS FOR,10H THIS TARG,10HET, HUB, A,10HND DAMAGE
2  ,10HCRTITION,10HEFOLLOW, TH,10HE NUMBERS,10HARE PD,10,
3  ,10H (TRUNCATE,10H), AND E,10H,CC05, **,10H,0)
4  ,10H( 131,10H,131/ 131/
DATA (BNND(1),1,14) /-1, 0, .0005, .0095, .1995, .2995, .3995, .4995, .5995, .6995, .7995, .8995, .9995, 1.1/
DATA (ALFA(1),1,13) /1HQ, 1HE, 1H, 1H2, 1H3, 1H4, 1H5, 1H6, 1H7, 1H8, 1H9, 1H*, 1H, /
1  , 1H, 1H9, 1H*, 1H, /

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```

*2638*16 026480
CONTR 2 026490
CONTR 3 026500
CONTR 4 026510
CONTR 5 026520
CONTR 6 026530
CONTR 7 026540
CONTR 8 026550
CONTR 9 026560
CONTR10 026570
CONTR11 026580
CONTR12 026590
CONTR13 026600
CONTR14 026610
CONTR15 026620
CONTR16 026630
CONTR17 026640
CONTR18 026650
CONTR19 026660
CONTR20 026670
CONTR21 026680
CONTR22 026690
CONTR23 026700
CONTR24 026710
CONTR25 026720
CONTR26 026730
CONTR27 026740
CONTR28 026750
CONTR29 026760
CONTR30 026770
CONTR31 026780
CONTR32 026790
CONTR33 026800
CONTR34 026810
CONTR35 026820
CONTR36 026830
CONTR37 026840
CONTR38 026850
CONTR39 026860
CONTR40 026870
CONTR41 026880
CONTR42 026890
CONTR43 026900
CONTR44 026910
CONTR45 026920
CONTR46 026930
CONTR47 026940
CONTR48 026950
CONTR49 026960
CONTR50 026970
CONTR51 026980
CONTR52 026990
CONTR53 027000
CONTR54 027010
CONTR55 027020
CONTR56 027030
CONTR57 027040
CONTR58 027050
CONTR59 027060
CONTR60 027070

```

```

C
DATA ONE, ICNE /1., 1/
LX1=LXPL
LXR=LXPR
LYB=LYPB
LYT=LYPT
SLX=SLXL
SHY=SHLY
SPACE=24
CNSTNT=CELL*FTTOM
CNSTT2=CNSTNT**2
J=LYB
ASSIGN 250 TO JUMP1
ASSIGN 470 TO JUMP3
IF (KSYN.EQ.2.OR.LMYB.GT.IROW1.OR.LMYT.LE.IROW1) GO TO 10
ASSIGN 460 TO JUMP3
NEVEL3=(LYT-LYB+1)*100
CALL MOVLEV (PK1,LYB),LEVEL3(1),NEVEL3)
10 J1=J+1
DO 20 K=1,13
BOUND(K,1)=99999
BOUND(K,2)=-99999
BOUND(K,3)=999.9
BOUND(K,4)=-99999
TEMPLA(K)=0.
20 TEMPA(K)=0
GET KILL AREA AND LETHAL AREA FOR EACH PD REGION
K=1
DO 60 KI=LX1,LXR
DO 60 KJ=J,LYT
KQ=DIMX*(KJ-1)+KI
IF (PPKK(KQ).LT.BND(K)) GO TO 40
K=K+1
30 IF (PPKK(KQ).LT.BND(K+1)) GO TO 50
GO TO 30
40 K=K+1
IF (PPKK(KQ).LT.BND(K)) GO TO 40
50 TEMPLA(K)=TEMPLA(K)+PPKK(KQ)
60 TEMPA(K)=TEMPA(K)+1
GET CONTOURS AND MAXIMUM EXTENT THEREOF FOR TLP AND BOTTOM ROWS
70 I=LX1
KQ=DIMX*(J-1)+I
K=1
80 IF (PPKK(KQ).GE.BND(K)) GO TO 120
90 KUNTR(KQ)=ALFA(K-1)
IF (BOUND(K,1).GT.I) BOUND(K,1)=I
IF (BOUND(K,2).LT.I) BOUND(K,2)=I
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J
I=I+1
IF (I.EQ.LMYB) GO TO 130
KQ=KQ+1
IF (PPKK(KQ).GE.BND(K)) GO TO 120
IF (PPKK(KQ).GE.BND(K-1)) GO TO 90
DO 100 KK=1,K
KKKK=KK
100 CONTINUE
110 K=KKK
120 GO TO 90

```

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CONTR610 027060
CONTR62 027050
CONTR63 027100
CONTR64 027110
CONTR65 027120
CONTR66 027130
CONTR67 027140
CONTR68 027150
CONTR69 027160
CONTR70 027170
CONTR71 027180
CONTR72 027190
CONTR73 027200
CONTR74 027210
CONTR75 027220
CONTR76 027230
CONTR77 027240
CONTR78 027250
CONTR79 027260
CONTR80 027270
CONTR81 027280
CONTR82 027290
CONTR83 027300
CONTR84 027310
CONTR85 027320
CONTR86 027330
CONTR87 027340
CONTR88 027350
CONTR89 027360
CONTR90 027370
CONTR91 027380
CONTR92 027390
CONTR93 027400
CONTR94 027410
CONTR95 027420
CONTR96 027430
CONTR97 027440
CONTR98 027450
CONTR99 027460
CONTR100 027470
CONTR101 027480
CONTR102 027490
CONTR103 027500
CONTR104 027510
CONTR105 027520
CONTR106 027530
CONTR107 027540
CONTR108 027550
CONTR109 027560
CONTR110 027570
CONTR111 027580
CONTR112 027590
CONTR113 027600
CONTR114 027610
CONTR115 027620
CONTR116 027630
CONTR117 027640
CONTR118 027650
CONTR119 027660
CONTR120 027670

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120 K=K+1
130 IF (K.LE.13) GO TO 60
130 IF (J.EQ.LMYT) GO TO 140
J=LMYT
GO TO 70
C GET CONTOURS AND MAXIMUM EXTENT THEREOF FOR REST OF ARRAY
140 J2=LMYT-1
IF (J1.GT.J2) GO TO 240
DO 230 J=J1,J2
I=LMXL
KQ=DIRX*(J-1)+I
K=1
150 IF (PPKK(KQ).GE.BND(K)) GO TO 210
KUNTR(KQ)=ALFA(K-1)
IF (BOUND(K,1).GT.I) BOUND(K,1)=I
IF (BOUND(K,2).LT.I) BOUND(K,2)=I
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J
IF (I.EQ.LMXR) GO TO 230
160 I=I+1
KQ=KQ+1
IF (PPKK(KQ).GE.END(K)) GO TO 210
IF (PPKK(KQ).LT.BND(K-1)) GO TO 170
IF (I.EQ.LMXR) GO TO 220
KUNTR(KQ)=BLANK
GO TO 160
170 KUNTR(KQ-1)=ALFA(K-1)
IF (BOUND(K,1).GT.I-1) BOUND(K,1)=I-1
IF (BOUND(K,2).LT.I-1) BOUND(K,2)=I-1
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J
II=I
DO 160 KK=1,K
KKK=K-KK
IF (PPKK(KQ).GE.END(KKK-1)) GO TO 190
180 CONTINUE
190 K=KKK
200 IF (I.EQ.LMXR) GO TO 220
I=I+1
KQ=KQ+1
IF (PPKK(KQ).LT.BND(K-1)) GO TO 170
KUNTR(KQ-1)=BLANK
IF (PPKK(KQ).LT.BND(K)) GO TO 200
KUNTR(II,J)=ALFA(K-1)
IF (BOUND(K,1).GT.II) BOUND(K,1)=II
IF (BOUND(K,2).LT.II) BOUND(K,2)=II
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J
KUNTR(KQ-1)=ALFA(K-1)
IF (BOUND(K,1).GT.I-1) BOUND(K,1)=I-1
IF (BOUND(K,2).LT.I-1) BOUND(K,2)=I-1
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J
210 K=K+1
220 IF (K.LE.13) GO TO 150
220 KUNTR(KQ)=ALFA(K-1)
IF (BOUND(K,1).GT.I) BOUND(K,1)=I
IF (BOUND(K,2).LT.I) BOUND(K,2)=I
IF (BOUND(K,3).GT.J) BOUND(K,3)=J
IF (BOUND(K,4).LT.J) BOUND(K,4)=J

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CONT121 027680
CONT122 027690
CONT123 027700
CONT124 027710
CONT125 027720
CONT126 027730
CONT127 027740
CONT128 027750
CONT129 027760
CONT130 027770
CONT131 027780
CONT132 027790
CONT133 027800
CONT134 027810
CONT135 027820
CONT136 027830
CONT137 027840
CONT138 027850
CONT139 027860
CONT140 027870
CONT141 027880
CONT142 027890
CONT143 027900
CONT144 027910
CONT145 027920
CONT146 027930
CONT147 027940
CONT148 027950
CONT149 027960
CONT150 027970
CONT151 027980
CONT152 027990
CONT153 028000
CONT154 028010
CONT155 028020
CONT156 028030
CONT157 028040
CONT158 028050
CONT159 028060
CONT160 028070
CONT161 028080
CONT162 028090
CONT163 028100
CONT164 028110
CONT165 028120
CONT166 028130
CONT167 028140
CONT168 028150
CONT169 028160
CONT170 028170
CONT171 028180
CONT172 028190
CONT173 028200
CONT174 028210
CONT175 028220
CONT176 028230
CONT177 028240
CONT178 028250
CONT179 028260
CONT180 028270

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230 CONTINUE
C 240 ASSIGN 41C TO JUMP2
GO TO JUMP1, (250,330)
C 250 OUTPUT PAGE HEADING
LINES=USED(LINES)
KNTY=LMYI-LMYB+1
KNTX=LMX-LMXL+1
ASSIGN 420 TO JUMP2
IF (PAGE-LINES-GE.KNTY+14) GO TO 260
IFMT2(1)=IFMT2(17)
LINES=0
GO TO 270
C 260 WRITE (6,490)
LINES=LINES+4
270 WRITE (6,IFMT2)
LINES=LINES+1
IFMT2(1)=IFMT2(16)
C LABEL ARRAY COLUMNS
TOP=0
280 J=C
DO 290 I=LMXL,LMXR
J=J+1
K=I/100
HEADER(J)=10H
IF (K-NE.0) ENCODE (10,510,HEADER(J) ) K
290 CONTINUE
WRITE (6,520) (HEADER(I),I=1,J)
J=0
DO 300 I=LMXL,LMXR
J=J+1
K=I/100
HEADER(J)=I-(I/100)*100/10
WRITE (6,530) (HEADER(I),I=1,J)
J=0
DO 310 I=LMXL,LMXR
J=J+1
K=I/100
HEADER(J)=I-(I/100)*10
WRITE (6,530) (HEADER(I),I=1,J)
LINES=LINES+4
JUMP OUT IF WE'VE JUST LABELED COLUMNS AT THE BOTTOM OF THE MAP
IF (TOP-NE.0) GO TO 330
TOP=1
ENCODE (20,550,IFMT1(1) ) KNTX
WRITE (6,540)
C 220 OUTPUT CONTOUR MAP
DO 230 JJ=1,KNTY
J=LMYI-JJ+1
WRITE (6,IFMT1) J,(KONTR(I,J),I=LMXL,LMXR),J
230 CONTINUE
LINES=LINES+KNTY+1
C GO BACK AND LABEL COLUMNS AT BOTTOM OF MAP
GO TO 250
C 330 OUTPUT OF MAP IS COMPLETE
N=C
DO 350 M=1,12
IF (BOUND(M+1,1),EQ.99999) GO TO 350
N=N+1
FKBAR(N)=C.
FEMPKA(N)=FLOAT(TEMPK(K))*CNST12
TEMPLA(N)=TEMPLA(K)*CNST12

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CONT161 028280
CONT182 028290
CONT183 028300
CONT184 028310
CONT185 028320
CONT186 028330
CONT187 028340
CONT188 028350
CONT189 028360
CONT190 028370
CONT191 028380
CONT192 028390
CONT193 028400
CONT194 028410
CONT195 028420
CONT196 028430
CONT197 028440
CONT198 028450
CONT199 028460
CONT200 028470
CONT201 028480
CONT202 028490
CONT203 028500
CONT204 028510
CONT205 028520
CONT206 028530
CONT207 028540
CONT208 028550
CONT209 028560
CONT210 028570
CONT211 028580
CONT212 028590
CONT213 028600
CONT214 028610
CONT215 028620
CONT216 028630
CONT217 028640
CONT218 028650
CONT219 028660
CONT220 028670
CONT221 028680
CONT222 028690
CONT223 028700
CONT224 028710
CONT225 028720
CONT226 028730
CONT227 028740
CONT228 028750
CONT229 028760
CONT230 028770
CONT231 028780
CONT232 028790
CONT233 028800
CONT234 028810
CONT235 028820
CONT236 028830
CONT237 028840
CONT238 028850
CONT239 028860
CONT240 028870

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IF (FEMPKA(N).NE.3.) PKBAR(N)=TEMPLA(N)/FEMPKA(N)
DO 340 J=1,4
340  BOUND(N,J)=BOUND(N,1)+J
    RANGEC(N)=BOUND(N,2)-BOUND(N,1)+1
    DEFC(N)=BOUND(N,4)-BOUND(N,3)+1
    RANGEM(N)=RANGEC(N)*CNSTNT
    DEFM(N)=DEFC(N)*CNSTNT
    MIDRGC(N)=FLCAT(BOUND(N,1)+BOUND(N,2))/2.-SHLX
    MIDDFC(N)=FLCAT(BOUND(N,3)+BOUND(N,4))/2.-SHLY
    MIDRGM(N)=MIDRGC(N)*CNSTNT
    MIDDFM(N)=MIDDFC(N)*CNSTNT
350  CONTINUE
    KK1=1
    IF (PKBAR(1).LE..000499999) KK1=2
    IL=N+1-KK1
    SPACE=SPACE+2*IL
    CELL=12.*CELL
    C      OUTPUT SEQUENCE IS OUTERMOST REGION TO INNERMOST REGION. THIS IS
    C      USUALLY LOW PK TO HIGH PK ORDER.
    BUFFER(1)=NSTAPE
    BUFFER(2)=IPNT
    BUFFER(3)=KSYM
    BUFFER(4)=KRIT(KRIT)
    BUFFER(5)=LMXL
    BUFFER(6)=LMXR
    BUFFER(7)=LMYB
    BUFFER(8)=LMYT
    BUFFER(9)=SHLX
    ABUFFER(10)=SHLY
    ABUFFER(11)=HOB
    ABUFFER(12)=CELL1
    IF (KK1.GT.N) GO TO 370
    J3=13
    BUFFER(13)=11
    DO 360 I=KK1,N
    ABUFFER(J3+1)=PKBAR(I)
    ABUFFER(J3+2)=RANGEM(I)
    ABUFFER(J3+3)=DEFM(I)
    ABUFFER(J3+4)=MIDRGM(I)
    ABUFFER(J3+5)=MIDDFM(I)
    ABUFFER(J3+6)=TEMPLA(I)
    ABUFFER(J3+7)=FEMPKA(I)
360  J3=J3+7
    GO TO 390
370  IL=1
    BUFFER(13)=1
    ABUFFER(14)=C.
    DO 380 J3=15,20
380  ABUFFER(J3)=1.
    ABUFFER(19)=C.
390  CALL WRITMS (STAPE,BUFFER(1),J3,NSTAPE,-1,C)
    SLIST(NSTAPE,2)=J3
    LINES=USED(LINES)
    IF (PAGE-LINES.GE.SPACE) GO TO 400
    WRITE (6,48C)
    LINES=C
    GO TO JUMP2, (41C,42C)
400  WRITE (6,50C)
    LINES=LINES+3
    GO TO JUMP2, (41C,42C)

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CONT241 028880
CONT242 028890
CONT243 028900
CONT244 028910
CONT245 028920
CONT246 028930
CONT247 028940
CONT248 028950
CONT249 028960
CONT250 028970
CONT251 028980
CONT252 028990
CONT253 029000
CONT254 029010
CONT255 029020
CONT256 029030
CONT257 029040
CONT258 029050
CONT259 029060
CONT260 029070
CONT261 029080
CONT262 029090
CONT263 029100
CONT264 029110
CONT265 029120
CONT266 029130
CONT267 029140
CONT268 029150
CONT269 029160
CONT270 029170
CONT271 029180
CONT272 029190
CONT273 029200
CONT274 029210
CONT275 029220
CONT276 029230
CONT277 029240
CONT278 029250
CONT279 029260
CONT280 029270
CONT281 029280
CONT282 029290
CONT283 029300
CONT284 029310
CONT285 029320
CONT286 029330
CONT287 029340
CONT288 029350
CONT289 029360
CONT290 029370
CONT291 029380
CONT292 029390
CONT293 029400
CONT294 029410
CONT295 029420
CONT296 029430
CONT297 029440
CONT298 029450
CONT299 029460
CONT300 029470

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410 WRITE (6,560)
   LINES=LINES+3
   ASSIGN 470 TO JUMP3
420 WRITE (6,570) SNAME,NSTAPE
   NSTAPE=NSTAPE+1
   WRITE (6,580)
   SUMLA=0.
   SUMKA=0.
   DO 430 KK=KK1,N
     K=N-KK+KK1
     SUMLA=SUMLA+TEMPLA(K)
     SUMKA=SUMKA+FEMPKA(K)
   WRITE (6,590) PKBAR(K),TEMPLA(K),SUMLA,FEMPKA(K),SUMKA
430 CONTINUE
   DO 440 K=KK1,N
     RANGE(K)=RANGEM(K)/CNSTNT
     RANGE(K)=DEFCK(K)/CNSTNT
   WRITE (6,600)
   DO 450 KK=KK1,N
     K=N-KK+KK1
     WRITE (6,610) PKBAR(K),RANGEM(K),RANGEC(K),MIDRCH(K),MIDREC(K),
1 DEFCK(K),DEFCK(K),MIDDFCK(K),MIDDFCK(K)
450 CONTINUE
   LINES=LINES+2*(N+KK1)+22
C
   GO TO JUMP3, (460,470)
460 CALL MOVLEV (LEVEL3(I),PK(I),LHYB),NEVEL3)
   ASSIGN 330 TO JUMP1
   J=IROM1+1
   SPACE=27
   GO TO IC
C
470 RETURN
C
480 FORMAT (1H1)
490 FORMAT (///)
500 FORMAT (///)
510 FORMAT (11,5X)
520 FORMAT (1H6,6X,124A1)
530 FORMAT (1H,6X,124I1)
540 FORMAT (1H )
550 FORMAT (11H(1H,13,3X,13,6A1,15))
560 FORMAT (112H THE FOLLOWING RESULTS CORRESPOND TO THOSE PRECEEDING,CON1344
1 BLT ARE FOR ROWS OF HIGHER ORDER THAN THE PROJECTILE LOCATION ON1345
2Y,/)
270 FORMAT (45H THESE DATA ARE ON THE CAMAGE FUNCTION FILE (,A1C,1CH)
1AS RECORD NUMBER,14,/)
580 FORMAT (1H,26X,78H AVERAGE PD WITHIN LETHAL AREA IN METERS**CON1349
12 CAMAGE AREA IN METERS**2/1H,29X,11H EACH REGION/1H,44X,2(6CON1350
2,24HPEF REGION CUMULATIVE//)
590 FORMAT (1H,4F7.3,5X,2(F16.3,F14.3))
600 FORMAT (///124H AVERAGE PD WITHIN RECTANGULARIZED, UNCON1353
INORMALIZED RANGE DATA RECTANGULARIZED, UNNORMALIZED DEFLECTCON1354
3ON DATA/1H,10X,11H EACH REGION/1H,20X,2(11X,8H EXHIBENT OF REGION CON1355
5 LOCATION OF REGION//1H,22X,2(28X,21H CENTER WRT PROJECTILE//1H
4,15X,2(7X,2(5X,1CH METERS CELLS//)
6,11 FORMAT (1H,4F10.3,1X,2(7X,2(F11.3,F10.1)))
   END
CON1301W 029480
CON1302 029490
CON1303 029500
CON1304W 029510
CON1305 029520
CON1306W 029530
CON1307 029540
CON1308 029550
CON1309 029560
CON1310 029570
CON1311 029580
CON1312 029590
CON1313W 029600
CON1314 029610
CON1315 029620
CON1316 029630
CON1317 029640
CON1318W 029650
CON1319 029660
CON1320 029670
CON1321W 029680
CON1322W 029690
CON1323 029700
CON1324 029710
CON1325 029720
CON1326 029730
CON1327 029740
CON1328 029750
CON1329 029760
CON1330 029770
CON1331 029780
CON1332 029790
CON1333 029800
CON1334 029810
CON1335 029820
CON1336 029830
CON1337 029840
CON1338 029850
CON1339 029860
CON1340 029870
CON1341 029880
CON1342 029890
CON1343 029900
CON1344 029910
CON1345 029920
CON1346 029930
CON1347 029940
CON1348 029950
CON1349 029960
CON1350 029970
CON1351 029980
CON1352 029990
CON1353 030000
CON1354 030010
CON1355 030020
CON1356 030030
CON1357 030040
CON1358 030050
CON1359- 030060

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```

SUBROUTINE SHOW (KK)
C THIS SUBROUTINE OUTPUTS THE LAMBDA ARRAY
C
COMMON /COM1/COM1(20100)
DIMENSION LAMDA(100,200),LAMD(100,200)
EQUIVALENCE (COM1(1),LAMD(1,1),LAMD(1,1),DUMMY)
C
COMMON /CELL/CELL
COMMON /CONST/CONST(6)
EQUIVALENCE (CONST(4),FTTOM)
COMMON /LYMIT/LYMXL,LYMYR,LYMYB,LYMYT
COMMON /PAGE/LINES,PAGE
COMMON /SHOW/SHOW(25)
C
DIMENSION IFMT1(3),IFMT2(5)
EQUIVALENCE (AREA,IAREA)
C
INTEGER PAGE,SHOW,USED
REAL LAMDA
C
DATA (IFMT1(1),I=1,3)/10H(1H ,13,2X,10H,2016,15) ,10H,2016,15) /
DATA (IFMT2(1),I=1,5)/10H(/5H ,10H ,2016 ,10H ,2016 ) /
1 ,1CH(1H/ 5H ,10H(/5H
C
FACTR=10.**SHOW(KK)
CUTOFF=1./FACTR
IAREA=0
SUM=0.
DO 10 I=LYMXL,LYMYR
DO 10 J=LYMYB,LYMYT
IF (LAMD(I,J).LT.CUTOFF) GO TO 10
SUM=SUM+LAMD(I,J)
IAREA=IAREA+1
10 CONTINUE
AREA=FLOAT(IAREA)*(CELL*FTTOM)**2
IF (AREA.GT..000001) SUM=SUM/AREA
DO 20 I=LYMXL,LYMYR
DO 20 J=LYMYB,LYMYT
LAMD(I,J)=LAMD(I,J)*FACTR
KNT=LYMYT-LYMYB+1
WRITE (6,80) SUM,AREA
80 LINES=LINES+2
KNT1=(LYMYR-LYMXL+1)/20
KEY=LYMYR-LYMXL+1-20*KNT1
IF (KNT1.EQ.0) GO TO 60
DO 30 I=1,KNT1
LINES=USED(LINES)
IF (PAGE-LINES-GE.KNT+5) GO TO 30
IFMT2(1)=IFMT2(4)
LINES=-1
30 ISTRT=LYMXL+(I-1)*20
ISTOP=ISTRT+19
WRITE (6,1FMT2) (IICCL,IICOL=ISTRT,ISTOP)
IFMT2(1)=IFMT2(5)
WRITE (6,90)
DO 40 J=1,KNT
IIRBW=LYMYT+1-J
WRITE (6,1FMT1) IIRBW,(LAMD(IICCL,IIRBW),IICCL=1,FTT,ISTOP),IIRBW
40 CONTINUE
WRITE (6,1FMT2) (IICOL,IICOL=1,FTT,ISTOP)

```

```

*2597*17 030070
SHOW 2 030080
SHOW 3 030090
SHOW 4 030100
SHOW 5 030110
SHOW 6 030120
SHOW 7 030130
SHOW 8 030140
SHOW 9 030150
SHOW 10 030160
SHOW 11 030170
SHOW 12 030180
SHOW 13 030190
SHOW 14 030200
SHOW 15 030210
SHOW 16 030220
SHOW 17 030230
SHOW 18 030240
SHOW 19 030250
SHOW 20 030260
SHOW 21 030270
SHOW 22 030280
SHOW 23 030290
SHOW 24 030300
SHOW 25 030310
SHOW 26 030320
SHOW 27 030330
SHOW 28 030340
SHOW 29 030350
SHOW 30 030360
SHOW 31 030370
SHOW 32 030380
SHOW 33 030390
SHOW 34 030400
SHOW 35 030410
SHOW 36 030420
SHOW 37 030430
SHOW 38 030440
SHOW 39 030450
SHOW 40 030460
SHOW 41 030470
SHOW 42 030480
SHOW 43 030490
SHOW 44 030500
SHOW 45 030510
SHOW 46 030520
SHOW 47 030530
SHOW 48 030540
SHOW 49 030550
SHOW 50 030560
SHOW 51 030570
SHOW 52 030580
SHOW 53 030590
SHOW 54 030600
SHOW 55 030610
SHOW 56 030620
SHOW 57 030630
SHOW 58 030640
SHOW 59 030650
SHOW 60 030660

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```

      LINES=LINES+KNT*5
50 CONTINUE
   IF (KEY.EQ.0) RETURN
   LINES=USED(LINES)
   IF (PAGE-LINES*GE.KNT*5) GO TO 60
   IFMT2(1)=IFMT2(4)
   LINES=-1
60  ISTR=LYMXL+KNT1*20
   ENCODE (10,100,IFMT1(2) )KEY
   ENCODE (10,110,IFMT2(2) )KEY
   WRITE (6,IFMT2) (IICOL,IICOL=ISTR,LYMXR)
   IFMT2(1)=IFMT2(5)
   WRITE (6,90)
   DO 70 J=1,KNT
   IIRW=LYMT+1-J
   WRITE (6,IFMT1) IIRW,(LAND(IICOL,IIRW),IICOL=ISTR,LYMXR),IIRW
70 CONTINUE
   WRITE (6,IFMT2) (IICOL,IICOL=ISTR,LYMXR)
   LINES=LINES+KNT*5
   IFMT1(2)=IFMT1(3)
   IFMT2(2)=IFMT2(3)
   RETURN
C
80 FORMAT (14H AN AVERAGE OF,1PE10.3,55H PERFORATIONS PER METER**2 ISSHOW**84
1  SUSTAINED OVER AN AREA OF,1PE10.3,1CH METERS**2/)
90 FORMAT (1H )
100 FORMAT (1H,12,7H16,I5) )
110 FORMAT (4H ,I2,4H16 )
END
SHOW61 030670
SHOW62 030680
SHOW63 030690
SHOW64 030700
SHOW65 030710
SHOW66 030720
SHOW67 030730
SHOW68 030740
SHOW69* 030750
SHOW70* 030760
SHOW71* 030770
SHOW72 030780
SHOW73* 030790
SHOW74 030800
SHOW75 030810
SHOW76* 030820
SHOW77 030830
SHOW78* 030840
SHOW79 030850
SHOW80 030860
SHOW81 030870
SHOW82 030880
SHOW83 030890
SHOW84 030900
SHOW85 030910
SHOW86 030920
SHOW87 030930
SHOW88 030940
SHOW89- 030950

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SUBROUTINE INDEX (ERRCR)
C
COMMON /CM3/COM3(10000)
DIMENSION BUFFER(104),ABUFFER(104),CBUFFER(8,13)
EQUIVALENCE (COM3(8460),BUFFER(1),ABUFFER(1))
1  , (BUFFER(13),NN), (ABUFFER(14),CBUFFER(1,1))

C
COMMON /DISC/DISC(15016)
DIMENSION PLIST(2502,2),SLIST(5002,2)
EQUIVALENCE (DISC(1),PLIST(1,1)), (DISC(2505),SLIST(1,1))
1  , (DISC(15013),STAPE), (DISC(15014),TAPF)
2  , (DISC(15015),TNAME), (DISC(15016),SNAME)

C
COMMON /AAA/AAA(8)
COMMON /PAGE/LINES,PAGE

C
DIMENSION IFMT(61)

C
INTEGER AAA,BUFFER,ERROR,PAGE,PLIST,SLIST,SNAME,STAPE,TAPF,TNAME
1  ,USED

C
DATA (IFMT(I),I=1,61)/10H(
1  ,1GHNT SYM,10HTRY D,10HAMAGE ,10H LYMXL L
2  ,10HMYR LYM,10HYB LYMT,10H PROJEC,10HTILE L
3  ,10HMB ,10H CELL ,10H NUMBER/1,10H ,8X,216H
4  ,10HNUMBER,3X),10H,21HCHARAC,10HTER CRIT,10HIERON,30X,
5  ,10H4HLGCATIO,10HN (MET,10HERS) (IN,10HCHES) OF
6  ,10H REGIONS//,10H1H ,110,19,10H,110,2112,,10H318,3M (,
7  ,10HF6,1,1H,,F,10H6,1,1H),F9,10H,2,F10,2,1,10H11,5(//),1H
8  ,10H ,5X,23HD,10HAMAGE FUNC,10HTION REGI,10HNS//1H ,27
9  ,10HX,77HPDBAR,10H LETHA,10HL DAMAG,10HE DIMEN
A  ,10HSIUNS IN M,10HETERS ,10HOFFSET OF ,10HMIDPOINT M
B  ,10HRT/1H ,38X,10H,214HAEF,10HGX),16H (,10HUNNORMALIZ
C  ,10HED),9X,20H,10HPRGJECTILE,10H IN METERS,10H1H ,58X,2
D  ,10H(10HCHANGE ,10H DEFLECTI,10HGN,8X)//(1,10H ,F32.3,F
E  ,10H11.3,2F10,,10H3,F11.3,F1,10H5.3,F11.3),10H)
F  ,10H(
1H ,10H(1H1/ 1H /

C
IF (ERRCR.NE.C) GO TO 50
IF (AAA(1).NE.10HDAMAGE FUN.ANU.AAA(5).NE.10HDAMAGE FUN) GO TO 4C
WRITE (6,60) SNAME
LINES=4
DO 30 J=1,5000
N=SLIST(J,2)
IF (N.EQ.0) GO TO 30
CALL READMS (STAPE,BUFFER(1),N,J)
LINES=USED(LINES)
IF (PAGE-LINES.GE.-20+NN) GO TO 10
IFMT(1)=IFMT(61)
LINES=0
GO TO 20
10 WRITE (6,60)
LINES=LINES+6
20 WRITE (6,IFMT) (BUFFER(1),I=1,8),(ABUFFER(1),I=9,12),BUFFER(13),
1  ((CBUFFER(1),K),I=1,7),K=1,NN)
LINES=LINES+NN+14
IFMT(1)=IFMT(66)
30 CONTINUE
40 IF (AAA(1).NE.10CHEXPECTED P.ANU.AAA(5).NE.10CHEXPECTED P) GO TO 70
50 WRITE (6,100) TNAME

```

```

*308*16 030960
INDEX 2 030970
INDEX 3 030980
INDEX 4 030990
INDEX 5 031000
INDEX 6 031010
INDEX 7 031020
INDEX 8 031030
INDEX 9 031040
INDEX10 031050
INDEX11 031060
INDEX12 031070
INDEX13 031080
INDEX14 031090
INDEX15 031100
INDEX16 031110
INDEX17 031120
INDEX18 031130
INDEX19 031140
INDEX20 031150
INDEX21 031160
INDEX22 031170
INDEX23 031180
INDEX24 031190
INDEX25 031200
INDEX26 031210
INDEX27 031220
INDEX28 031230
INDEX29 031240
INDEX30 031250
INDEX31 031260
INDEX32 031270
INDEX33 031280
INDEX34 031290
INDEX35 031300
INDEX36 031310
INDEX37 031320
INDEX38 031330
INDEX39 031340
INDEX40 031350
INDEX41 031360
INDEX42 031370
INDEX43 031380
INDEX44 031390
INDEX45 031400
INDEX46 031410
INDEX47 031420
INDEX48 031430
INDEX49 031440
INDEX50 031450
INDEX51 031460
INDEX52 031470
INDEX53 031480
INDEX54 031490
INDEX55 031500
INDEX56 031510
INDEX57 031520
INDEX58 031530
INDEX59 031540
INDEX60 031550

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DO 60 I=1,2500
IF (PLIST(1,2).EQ.0) GO TO 6C
CALL READMS (TAPE,BUFFER(1),19,1)
ABUFFER(4)=ABUFFER(4)*2.
WRITE (6,110) (BUFFER(J),J=1,3),(ABUFFER(J),J=4,5),(BUFFER(J),J=6,
1 11,(ABUFFER(J),J=12,13),(BUFFER(J),J=14,17),(ABUFFER(J),J=18,19)
60 CONTINUE
70 CALL WRITMS (TAPE,PLIST(1,2),2501,2501,-1,0)
CALL WRITMS (TAPE,SLIST(1,2),5001,5001,-1,0)
CALL CLOSMS (TAPE)
CALL CLOSMS (TAPE)
WRITE (6,120)
STOP
C
60 FORMAT (1H1/1H ,36X,42HA TABULATION OF THE DAMAGE FUNCTION FILE (,
1A,C,5H) FOLLOWS//)
9C FORMAT (////)
100 FORMAT (1H1/1H ,35X,44HAN INCEX OF THE EXPECTED PERFORATIONS FILE INDEX78
1(A10,9H) FOLLOWS//1H0,16X,99HRECORD NXX NYY CELL HUB IROM ICINDEX79
20L LYMYB LYMYT LYMXL LYMYR A B NSIDE NX NY NZ T THCK//INDEX80
3/)
110 FORMAT (1H ,12L,15,I4,F7.2,F6.2,3I5,3I6,2F7.1,I4,15,2I3,F5.1,F5.2) INDEX81
120 FORMAT (1H1) INDEX82
END INDEX83
INDEX84- 031790
INDEX61 031560
INDEX62 031570
INDEX63 031560
INDEX64 031590
INDEX65W 031600
INDEX66W 031610
INDEX67 031620
INDEX68 031630
INDEX69 031640
INDEX70 031650
INDEX71 031660
INDEX72W 031670
INDEX73 031680
INDEX74 031690
INDEX75 031700
INDEX76 031710
INDEX77 031720
INDEX78 031730
INDEX79 031740
INDEX80 031750
INDEX81 031760
INDEX82 031770
INDEX83 031780
INDEX84- 031790

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```

C      2      ,10H( 1HL/ ,10H(C(//),1H ,/
10  DECODE (50,430,AAA(2) )FN,FNVEH,FNVS,FNHTS,U1
    NFN+ .1
    NVEH=FNVEH+.1
    NVS=FNVS+.1
    NHTS=FNHTS+.1
    U2=U1
    READ (5,510) (AAA(I),I=1,8)
    IF (AAA(1).EQ.10HSAME CANN0) GO TO 20
    DECODE (80,430,AAA(1) )(A(I),I=1,8)
    IF (N-GT.8) READ (5,430) (A(I),I=9,N)
    READ (5,430) (B(I),I=1,N)
    GO TO 40
20  DO 30 I=1,N
30  B(I)=-B(I)
40  IF (AAA(1).EQ.10HSAME TARGE) GO TO 50
    DECODE (80,430,AAA(1) )(VDSR(I),I=1,8)
    IF (NVEH-GT.8) READ (5,430) (VDSR(I),I=9,NVEH)
    READ (5,430) (VDSR(I),I=1,NVEH)
    GO TO 70
50  DO 60 I=1,NVEH
60  VDSR(I)=-VDSR(I)
70  IF (AAA(1).EQ.10HSAME VOLLE) GO TO 90
    DECODE (80,430,AAA(1) )(FNN(I),I=1,8)
    IF (NVS-GT.8) READ (5,430) (FNN(I),I=9,NVS)
    DO 80 I=1,NVS
80  NNI(I)=FNN(I)+.1
90  READ (5,510) (AAA(I),I=1,8)
    IF (AAA(1).EQ.10HSAME ERRCR) GO TO 100
    DECODE (50,430,AAA(1) )J1,J2,T1,T2,R
    IF (T1.EQ.0.) T1=.00001
    IF (T2.EQ.0.) T2=.00001
100 READ (5,510) (AAA(I),I=1,8)
    WRITE (6,440) N
    WRITE (6,450) (A(I),I=1,N)
    WRITE (6,460)
    WRITE (6,450) (B(I),I=1,N)
    THIS SUBPROGRAM EXPECTS DEFLECTION RIGHT TO BE POSITIVE
    DO 110 I=1,N
110  B(I)=-B(I)
    IUI=UI+.1
    IUI=UI+.1
    WRITE (6,500) J1,J2,T1,T2,R,IUI,IU2
    WRITE (6,490) NVS,(NN(I),I=1,NVS)
    WRITE (6,470) NVEH
    WRITE (6,450) (VDSR(I),I=1,NVEH)
    WRITE (6,480)
    WRITE (6,450) (VDSR(I),I=1,NVEH)
    THIS SUBPROGRAM EXPECTS DEFLECTION RIGHT TO BE POSITIVE
    DO 120 I=1,NVEH
120  VDSR(I)=-VDSR(I)
    IF (AAA(1).EQ.10HSAME DAMAG) GO TO 190
    DO 180 I=1,NHTS
    IF (I-NE.1) READ (5,510) (AAA(J),J=1,R)
    KEY2(I)=10HCARDS
    DECODE (10,520,AAA(1) )(AAA(J),J=1,10)
    ASSIGN 180 TO JUMP

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SNOW 610 C32400
SNOW 62 C32410
SNOW 63* C32420
SNOW 64 C32430
SNOW 65 C32440
SNOW 66 C32450
SNOW 67 C32460
SNOW 68 C32470
SNOW 69* C32480
SNOW 70 C32490
SNOW 71* C32500
SNOW 72R C32510
SNOW 73R C32520
SNOW 74 C32530
SNOW 75 C32540
SNOW 76 C32550
SNOW 77R C32560
SNOW 78 C32570
SNOW 79* C32580
SNOW 80R C32590
SNOW 81R C32600
SNOW 82 C32610
SNOW 83 C32620
SNOW 84 C32630
SNOW 85R C32640
SNOW 86 C32650
SNOW 87* C32660
SNOW 88R C32670
SNOW 89 C32680
SNOW 90 C32690
SNOW 91R C32700
SNOW 92 C32710
SNOW 93* C32720
SNOW 94 C32730
SNOW 95 C32740
SNOW 96R C32750
SNOW 97M C32760
SNOW 98M C32770
SNOW 99M C32780
SNOW100M C32790
SNOW101 C32800
SNOW102 C32810
SNOW103 C32820
SNOW104 C32830
SNOW105 C32840
SNOW106M C32850
SNOW107M C32860
SNOW108M C32870
SNOW109M C32880
SNOW110M C32890
SNOW111M C32900
SNOW112 C32910
SNOW113 C32920
SNOW114 C32930
SNOW115 C32940
SNOW116 C32950
SNOW117R C32960
SNOW118 C32970
SNOW119* C32980
SNOW120 C32990

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DO 140 J=1,10
  IF (AAAA(J).GT.1HZ) GO TO 14C
  GO TO JUMP, (130,150)
130 IF (AAAA(J).NE.1HE) GO TO 15C
  ASSIGN 150 TO JUMP
140 CONTINUE
  GO TO 160
150 CALL INPUT (I)
  GO TO 180
160 DECODE (30,430,AAA(I)) HT(I),FNUMB(I),FNUMN(I)
  NUMB(I)=FNUMB(I)+1
  NUMN(I)=FNUMN(I)+1
  NBS=NUMB(I)
  DO 170 J=1,NBS
    READ (5,430) XSSP(I,J),X883(I,J),X884(I,J),XROSET(I,J),XDCSET(I,J)
170 CONTINUE
180 CONTINUE
190 LINES=41+4*(N-1)/10+(NVEH-1)/1C
  DO 230 I=1,NHTS
    LAPI=NUMB(I)
    LINES=USED(LINES)
    IF (PAGE-LINES.GE.LAPI+14) GO TO 200
    IFMT4(I)=IFMT4(I36)
    LINES=-6
200 IF (KEY2(I).NE.10HCARDS ) GO TO 210
    ENCODE (60,530,IFMT4(2) )
    GO TO 220
210 ENCODE (6C,540,IFMT4(2) )KEY2(I),SNAME
220 WRITE (6,IFMT4) HT(I),NUMB(I),FNUMN(I), (XSSP(I,J),X883(I,J),X884(I,J),XROSET(I,J),XDCSET(I,J),J=LAPI)
  LINES=LINES+14+LAPI
  IFMT4(I)=IFMT4(I35)
  DO 230 J=1,LAPI
    XROSET(I,J)=XROSET(I,J)
    XDCSET(I,J)=XDCSET(I,J)
230 XSSP(I,J)=XSSP(I,J)*R
  IF (NVS.GT.2C) GO TO 24C
  IFMT5(6)=IFMT5(9)
  IF (NVS.GT.1C) GO TO 24C
  IFMT5(4)=IFMT5(9)
  IFMT6(4)=IFMT6(1C)
240 LINEINC=13+2*NHTS*(NHTS+1)*(NVS-1)/10)
  DO 390 K=1,NVEH
    SU1=VOSP(K)
    SU2=VCSO(K)
    TU1=T1*U1
    TU2=T2*U2
    SSU3=0.
    SSU4=C.
    AJM=ABS(SU1-A(1))
    BJM=ABS(SU2-B(1))
    IF (N.EC.1) GO TO 260
    DO 25C J=2,N
      ASU1=ABS(SU1-A(J))
      BSU2=ABS(SU2-B(J))
      IF (ASU1.GT.AJM) AJM=ASU1
      IF (BSU2.GT.BJM) BJM=BSU2
25C CONTINUE
260 DO 27C J=1,N

```

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SNOW121 033000
SNOW122 033010
SNOW123 033020
SNOW124 033030
SNOW125 033040
SNOW126 033050
SNOW127 033060
SNOW128 033070
SNOW129 033080
SNOW130* 033090
SNOW131 033100
SNOW132 033110
SNOW133 033120
SNOW134 033130
SNOW135* 033140
SNOW136 033150
SNOW137 033160
SNOW138 033170
SNOW139 033180
SNOW140 033190
SNOW141 033200
SNOW142 033210
SNOW143 033220
SNOW144 033230
SNOW145 033240
SNOW146* 033250
SNOW147 033260
SNOW148* 033270
SNOW149 033280
SNOW150 033290
SNOW151 033300
SNOW152 033310
SNOW153 033320
SNOW154 033330
SNOW155 033340
SNOW156 033350
SNOW157 033360
SNOW158 033370
SNOW159 033380
SNOW160 033390
SNOW161 033400
SNOW162 033410
SNOW163 033420
SNOW164 033430
SNOW165 033440
SNOW166 033450
SNOW167 033460
SNOW168 033470
SNOW169 033480
SNOW170 033490
SNOW171 033500
SNOW172 033510
SNOW173 033520
SNOW174 033530
SNOW175 033540
SNOW176 033550
SNOW177 033560
SNOW178 033570
SNOW179 033580
SNOW180 033590

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NJ1=N-J+1
SSU3=SSU3+ABS(A(NJ1)+A(J))
SSU4=SSU4+ABS(B(NJ1)+B(J))
270 CONTINUE
S03=S01+SSU3
S04=S02+SSU4
U3=U1
IF (S03.NE.0.) U3=2.*U3
U4=U2
IF (S04.NE.0.) U4=2.*U4
LU3=U3
LU4=U4
SE12=2./U1
AK=U3
GO TO 290
280 AK=AK-1.
290 AX=0.
IF (AK.EQ.0.) GO TO 300
AX=2.*AK-1.
IF (S03.NE.0.) AX=AX-2.*U1
AX=AX*SE12
300 AA=5-ERF(AX)
IF (AA.GT..0001) GO TO 310
GO TO 280
310 SE3=(SE12+AX)/U1
SE22=2./U2
AK=U4
GO TO 330
320 AK=AK-1.
330 AY=0.
IF (AK.EQ.0.) GO TO 340
AY=2.*AK-1.
IF (S04.NE.0.) AY=AY-2.*U2
AY=AY*SE22
340 AA=5-ERF(AY)
IF (AA.GT..0001) GO TO 350
GO TO 320
350 LINES=USED(LINES)
IF (PAGE-LINES.GE.LINEINC) GO TO 360
IFMT7(1)=IFMT7(8)
LINES=0
360 V050(K)=-V050(K)
WRITE (6,IFMT7) K,V05R(K),VCSD(K)
V050(K)=-V050(K)
IFMT7(1)=IFMT7(9)
WRITE (6,IFMT5) (NN(I),I=1,NVS)
DO 380 L=1,NHTS
N6S=NUMB(L)
NNN=NUMN(L)
DO 370 JJ=1,N8S
B33(JJ)=XB33(L,JJ)
B64(JJ)=XB64(L,JJ)
SSP(JJ)=XSSP(L,JJ)
DOSET(JJ)=XDOSET(L,JJ)
DCSET(JJ)=XDCSET(L,JJ)
SE4=(SE22+AY)/U2
GSE1=(A(J)*X+.5*BB3(N8S)+4.*S1)/U1
GSE2=(B(J)*X+.5*BB4(N8S)+4.*S2)/U2
SE12=AMINI(SEE3*GSE1)*.2
SE22=AMINI(SEE4*GSE2)*.2

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SNOW181 C33600
SNOW182 C33610
SNOW183 C33620
SNOW184 C33630
SNOW185 C33640
SNOW186 C33650
SNOW187 C33660
SNOW188 C33670
SNOW189 C33680
SNOW190 C33690
SNOW191 C33700
SNOW192 C33710
SNOW193 C33720
SNOW194 C33730
SNOW195 C33740
SNOW196 C33750
SNOW197 C33760
SNOW198 C33770
SNOW199 C33780
SNOW200 C33790
SNOW201 C33800
SNOW202 C33810
SNOW203 C33820
SNOW204 C33830
SNOW205 C33840
SNOW206 C33850
SNOW207 C33860
SNOW208 C33870
SNOW209 C33880
SNOW210 C33890
SNOW211 C33900
SNOW212 C33910
SNOW213 C33920
SNOW214 C33930
SNOW215 C33940
SNOW216 C33950
SNOW217 C33960
SNOW218 C33970
SNOW219 C33980
SNOW220 C33990
SNOW221 C34000
SNOW222 C34010
SNOW223 C34020
SNOW224 C34030
SNOW225 C34040
SNOW226 C34050
SNOW227 C34060
SNOW228 C34070
SNOW229 C34080
SNOW230 C34090
SNOW231 C34100
SNOW232 C34110
SNOW233 C34120
SNOW234 C34130
SNOW235 C34140
SNOW236 C34150
SNOW237 C34160
SNOW238 C34170
SNOW239 C34180
SNOW240 C34190

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CALL A50 (K,L)
WRITE (6,IFMT6) HT(L),(ZZ(K,I,L),I=1,NVS)
380 CONTINUE
LINES=LINES+LINEINC
390 CONTINUE
400 READ (5,510) (AAA(I),I=1,8)
IF (AAA(1).NE.1CHSAME HOB D.AND.AAA(1).NE.10HHOB DISTRI.AND.AAA(1).NE.10HALL HUBS ) GO TO 410
1.NE.10HOPTIMIZE .AND.AAA(1).NE.10HALL HUBS ) GO TO 410
CALL CHBN
GO TO 400
410 IFMT5(4)=IFMT5(8)
IFMT5(6)=IFMT5(8)
IFMT6(4)=IFMT6(8)
IFMT6(6)=IFMT6(9)
IF (AAA(1).NE.1CHENCOUNTER .AND.AAA(1).NE.10H ENCOUNTER) RETURN
DO 420 I=1,NHTS
LAP1=NUMB(I)
DO 420 J=1,LAP1
XROSET(I,J)=XROSET(I,J)
XDOSET(I,J)=XDOSET(I,J)
420 XSSP(I,J)=XSSP(I,J)/R
GO TO 10
C
430 FORMAT (8F10.3)
440 FORMAT (1H1/10H THERE ARE,I3,7H CANNON//62H0 THE AIMING POINT
1RANGE COORDINATES FOR THE CANNON FOLLOW)
450 FORMAT (1H0.7X,10F10.2)
460 FORMAT (/67H0 THE AIMING POINT DEFLECTION COORDINATES FOR THE
1CANNON FOLLOW)
470 FORMAT (/10H0THERE ARE,I3,6H TARGETS//65H0 THE RANGE COORDINATES FOR THE
1TES FOR THE CENTERS OF THE TARGETS FOLLOW)
480 FORMAT (/70H0 THE DEFLECTION COORDINATES FOR THE CENTERS OF THE
1E TARGETS FOLLOW)
490 FORMAT (/10H0THERE ARE,I3,65H DIFFERENT VOLLEY SIZES. THE NUMBERS
1 OF ROUNDS PER CANNON FOR THE VOLLEY SIZES FOLLOW/1H0,2515)
500 FORMAT (/154H0THE ROUND-TO-ROUND SIGMAS IN RANGE AND DEFLECTION ARSNOW276
1E,F7.2,4H AND,F7.2,13H RESPECTIVELY/52H0THE AIMING ERROR SIGMAS INSNOW277
2 RANGE AND DEFLECTION ARE,F7.2,4H AND,F7.2,13H RESPECTIVELY/24H0THSNOW278
3E FUZE RELIABILITY IS,F6.3/10H0THERE ARE,I3,1H,12,51H INTEGRATIONSNOW279
4 STEPS IN EACH QUADRANT FOR EACH TARGET)
510 FORMAT (8A10)
520 FORMAT (10A1)
530 FORMAT (60H1H ,22X,30HTHE DAMAGE FUNCTION FROM CARDS
1 )
540 FORMAT (33H1H ,14X,47HDAMAGE FUNCTION NUMBER,I4,11H FROM FILE ,A10SNOW285
1,2H )
END
SNOW241 034200
SNOW242M 034210
SNOW243 034220
SNOW244 034230
SNOW245 034240
SNOW246R 034250
SNOW247 034260
SNOW248 034270
SNOW249 034280
SNOW250 034290
SNOW251 034300
SNOW252 034310
SNOW253 034320
SNOW254 034330
SNOW255 034340
SNOW256 034350
SNOW257 034360
SNOW258 034370
SNOW259 034380
SNOW260 034390
SNOW261 034400
SNOW262 034410
SNOW263 034420
SNOW264 034430
SNOW265 034440
SNOW266 034450
SNOW267 034460
SNOW268 034470
SNOW269 034480
SNOW270 034490
SNOW271 034500
SNOW272 034510
SNOW273 034520
SNOW274 034530
SNOW275 034540
SNOW276 034550
SNOW277 034560
SNOW278 034570
SNOW279 034580
SNOW280 034590
SNOW281 034600
SNOW282 034610
SNOW283 034620
SNOW284 034630
SNOW285 034640
SNOW286 034650
SNOW287- 034660

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```

C      SUBROUTINE A50 (KKDUM,LLDUM)
COMMON /COM1/COM1(20100)
DIMENSION ZZ(25,25,25)
EQUIVALENCE (COM1(1),ZZ(1,1,1))

C
COMMON /COM3/COM3(10000)
DIMENSION NN(25),SSSUM(25),ZZSUM(25)
EQUIVALENCE (COM3(1878),NN(1)),(COM3(2041),SSSUM(1))
1      ,(COM3(2066),ZZSUM(1)),(COM3(9881),LU3)
2      ,(COM3(9882),LU4),(COM3(9587),NVS),(COM3(9990),SE12)
3      ,(COM3(9991),SE22),(COM3(9994),SU3),(COM3(9995),SU4)
4      ,(COM3(9998),U1),(COM3(9999),U2)

C      KK=KKDUM
LL=LLDUM
DO 10 I=1,NVS
10  ZZSUM(I)=0.0
DO 60 J=1,LU3
DO 20 K=1,NVS
20  SSSUM(I)=0.0
X=2.*FLOAT(J)-1.
IF (SU3.NE.0.) X=X-2.*U1
X=X*SE12
DO 40 K=1,LU4
Y=2.*FLOAT(K)-1.
IF (SU4.NE.0.) Y=Y-2.*U2
Y=Y*SE22
PPK6=PK6(X,Y)
AF=ERF(Y+SE22)-ERF(Y-SE22)
DO 30 I=1,NVS
30  SSSUM(I)=SSSUM(I)*(1.0-PPK6**NN(I))*AF
40  CONTINUE
AF=ERF(X+SE12)-ERF(X-SE12)
DO 50 I=1,NVS
50  ZZSUM(I)=ZZSUM(I)+SSSUM(I)*AF
60  CONTINUE
DO 70 I=1,NVS
70  ZZ(KK,1,LL)=ZZSUM(I)
IF (SU5.NE.0.) GO TO 90
DO 80 I=1,NVS
80  ZZ(KK,1,LL)=2.*ZZ(KK,1,LL)
90  IF (SU4.NE.0.) GO TO 110
DO 100 I=1,NVS
100 ZZ(KK,1,LL)=2.*ZZ(KK,1,LL)
110 RETURN
END

```



```

C
FUNCTION PK6 (XXDUM,YYDUM)
COMMON /COM3/COM3(10000)
DIMENSION A(100),B(100),BB3(13),BB4(13),DDSET(13),ROSET(13)
1  SSP(13),XUA(100),YUB(100)
EQUIVALENCE (COM3(1),A(1)),(COM3(101),B(1)),(COM3(1826),BB3(1))
1  (COM3(1839),BB4(1)),(COM3(1852),DDSET(1))
2  (COM3(1865),ROSET(1)),(COM3(1903),SSP(1))
3  (COM3(2091),XUA(1)),(COM3(2191),YUB(1))
4  (COM3(9979),B1),(COM3(9980),B2),(COM3(9983),N)
5  (COM3(9984),NBS),(COM3(9985),NNN),(COM3(9988),S1)
6  (COM3(9989),S2),(COM3(9992),SUI),(COM3(9993),SU2)
7  (COM3(9996),T1),(COM3(9997),T2)

C
XX=XXDUM
YY=YYDUM
PK6=1.
DO 10 J=1,N
XUA(J)=XX*T1+SUI-A(J)
YUB(J)=YY*T2+SU2-B(J)
10 CONTINUE
DO 20 J=1,N
POLD=0.C
DO 20 I=1,NBS
XTA=XUA(J)-RCSET(I)
YTA=YUB(J)-DDSET(I)
B1=.5*BB3(I)
B2=.5*BB4(I)
PX1=SMF(XTA,B1,S1)
PY1=SMF(YTA,B2,S2)
IF (I.LE.NNN) GO TO 30
PK6=PK6*(1.-(PX1*PY1-POLD)*SSP(I))
POLD=PX1*PY1
20 CONTINUE
30 RETURN
PK6=PK6*(1.-PX1*PY1*SSP(I))
POLD=POLD+PX1*PY1
GO TO 20
END

```

```

#3504*21 035140
PK6 2 035150
PK6 3 035160
PK6 4 035170
PK6 5 035180
PK6 6 035190
PK6 7 035200
PK6 8 035210
PK6 9 035220
PK6 10 035230
PK6 11 035240
PK6 12 035250
PK6 13 035260
PK6 14 035270
PK6 15 035280
PK6 16 035290
PK6 17 035300
PK6 18 035310
PK6 19 035320
PK6 20 035330
PK6 21 035340
PK6 22 035350
PK6 23 035360
PK6 24 035370
PK6 25 035380
PK6 26 035390
PK6 27 035400
PK6 28 035410
PK6 29 035420
PK6 30 035430
PK6 31 035440
PK6 32 035450
PK6 33 035460
PK6 34 035470
PK6 35 035480
PK6 36 035490
PK6 37 035500
PK6 38 035510
PK6 39- 035520

```

```

FUNCTION SMF (OX,GY,S)
IF (S.EQ.0.) GO TO 10
SMF=ERF((OX+GY)/S)-ERF((OX-CY)/S)
GO TO 20
10 SMF=0.
IF (ABS(OX).LE.GY) SMF=1.
20 RETURN
END

```

```

*3543*22 035530
SMF 2 035540
SMF 3 035550
SMF 4 035560
SMF 5 035570
SMF 6 035580
SMF 7 035590
SMF 8- 035600

```

```

C
C
C
DATA P00T2 /.7C71067812/
ROUT2=SQRT(1./2.)
A=ABS(X)*P00T2
A2=A*A
IF (A.GT.4.17) GO TO 10
GO TO 20
10 ERF=.5
GO TO 50
20 IF (A.GT.1.51) GO TO 30
GO TO 40
30 ERF=.5-EXP(-A2)*.282094792*(A/(A2+.5)-(.5/(A2+2.5)-(3./(A2+4.5)-(7.5/(A2+6.5)-(10.663/(A2+4.265)))))))
GO TO 50
40 ERF=A*.564189584*(1.-1.0261*A2/(A2+10.216-(167.17/(A2+9.8103
1 + (201.39/(A2+11.773*(64.225759/(A2+5.5777245))))))
2 ))))
50 IF (X.LT.0.) ERF=-ERF
RETURN
END

```

```

*3551*23 035610
ERF 2 035620
ERF 30 035630
ERF 4 035640
ERF 5 035650
ERF 6 035660
ERF 7 035670
ERF 8 035680
ERF 9 035690
ERF 10 035700
ERF 11 035710
ERF 12 035720
ERF 13 035730
ERF 14 035740
ERF 15 035750
ERF 16 035760
ERF 17 035770
ERF 18 035780
ERF 19 035790
ERF 20 035800
ERF 21 035810
ERF 22- 035820

```

```

C
C
C
C
C
C
SUBROUTINE INPUT (IIIII)
THIS SUBROUTINE GENERATES A COMPLETELY NESTED DAMAGE FUNCTION FOR
THIS PROGRAM FROM THE DAMAGE FUNCTION DATA STORED ON THE DAMAGE
FUNCTION FILE BY SUBROUTINE CONTR
COMMON /COM3/COM3(10000)
DIMENSION QQ1(25,13),XSSP(325),PKBAR(325),QQ2(25,13),MAXRG(325)
1  ,RG(325),XBB3(325),QQ3(1,1),MAXDF(1,1),DFM(325)
2  ,XBB4(325),QQ4(25,13),MINDF(325),MIDDFM(325)
3  ,XDOSET(325),QQ5(25,13),MINRG(325),MIDRGM(325)
4  ,XROSET(325),HT(25),NUMB(25),NUMNN(25),QLA(25,13)
5  ,LA(325),OKA(25,13),KA(325),STEP52(13),FSTEPS(13)
6  ,BUFFER(13),ABUFFR(13),BUFR2(7,13),ABFR2(7,13)
7  ,KEY2(25)
EQUIVALENCE (COM3(201),QQ1(1,1),XSSP(1),PKBAR(1))
1  , (COM3(526),QQ2(1,1),MAXRG(1),RGM(1),XBB3(1))
2  , (COM3(851),QQ3(1,1),MAXDF(1),DFM(1),XBB4(1))
3  , (COM3(1176),QQ4(1,1),MINDF(1),MIDDFM(1),XDOSET(1))
4  , (COM3(1501),QQ5(1,1),MINRG(1),MIDRGM(1),XROSET(1))
5  , (COM3(1916),HT(1), (COM3(1941),NUMB(1))
6  , (COM3(1966),NUMNN(1), (COM3(2291),QLA(1,1),LA(1))
7  , (COM3(2616),OKA(1,1),KA(1))
8  , (COM3(2941),STEP52(1),FSTEPS(1))
9  , (COM3(3446),BUFR2(1),ABUFFR(1),KK), (BUFR2(13),JJ)
A  , (COM3(3459),BUFR2(1,1),ABFR2(1,1))
B  , (COM3(9954),KEY2(1), (COM3(9984),NBS,NSTEPS)

C
COMMON /DISC/DISC(15016)
DIMENSION SLIST(5002,2)
EQUIVALENCE (DISC(5005),SLIST(1,1)), (DISC(15013),STAPE)

C
COMMON /AAA/AAA(8)
COMMON /PAGE/LINES,PAGE

C
EQUIVALENCE (FILE2,FFILE2)

INTEGER AAA,BUFFER,BUFR2,FILE2,SLIST
1  ,STAPE,STEP52,STEPS,SUB1,SUB2
REAL KA,LA,LIM1,LIM2,LIM3,LIM4,LIM5,LIM6,LIM7,LIM8,MAXDF,MAXRG
1  ,MIDDFM,MIDRGM,MINDF,MINRG,NORM,NORM1,NORM2

C
I=IIIII
DECODE (60,220,AAA(3)) FFILE2,(FSTEPS(J),J=1,11)
FILE2=FFILE2+.1
DO 1C J=1,11
1C STEPS2(J)=FSTEPS(J)+.1
KEY2(1)=FILE2
CALL READMS (STAPE,BUFFER(1),SLIST(FILE2,2),FILE2)
HT(1)=ABUFFR(11)
NSTEPS=BUFR2(13)
DO 20 J=1,NSTEPS
QQ1(1,J)=ABFR2(1,J)
QQ2(1,J)=ABFR2(12,J)
QQ3(1,J)=ABFR2(13,J)
QQ4(1,J)=ABFR2(4,J)
QQ5(1,J)=ABFR2(5,J)
QQ6(1,J)=ABFR2(6,J)
QLA(1,J)=ABFR2(7,J)
20 QKA(1,J)=ABFR2(7,J)
IF (NSTEPS.EC.1) GO TO 40

```

```

C      CONTR OUTPUTS REGIONS FROM CUTERMOST TO INNERMOST. MAKE THE ORDER
C      IS REVERSED.
K=NSTEPS/2
DO 30 J=1,K
  SUB1=(J-1)*25+1
  SUB2=(NSTEPS-J)*25+1
  TEMP=PKBAR(SUB2)
  PKBAR(SUB2)=PKBAR(SUB1)
  PKBAR(SUB1)=TEMP
  TEMP=RGH(SUB2)
  RGH(SUB2)=RGH(SUB1)
  RGH(SUB1)=TEMP
  TEMP=DFM(SUB2)
  DFM(SUB2)=DFM(SUB1)
  DFM(SUB1)=TEMP
  TEMP=MIDGM(SUB2)
  MIDGM(SUB2)=MIDGM(SUB1)
  MIDGM(SUB1)=TEMP
  TEMP=MIDDFM(SUB2)
  MIDDFM(SUB2)=MIDDFM(SUB1)
  MIDDFM(SUB1)=TEMP
  TEMP=LA(SUB2)
  LA(SUB2)=LA(SUB1)
  LA(SUB1)=TEMP
  TEMP=KA(SUB2)
  KA(SUB2)=KA(SUB1)
  KA(SUB1)=TEMP
30 DO 50 J=1,NSTEPS
  SUB1=(J-1)*25+1
  MINRG(SUB1)=MIDGM(SUB1)-RGH(SUB1)/2.
  MAXRG(SUB1)=MINRG(SUB1)+RGH(SUB1)
  MINDF(SUB1)=MIDDFM(SUB1)-DFM(SUB1)/2.
  MAXDF(SUB1)=MINDF(SUB1)+DFM(SUB1)
  STEPS1=0
  IF (STEPS2(1).NE.0) GO TO 7C
  IF (STEPS2(1).NE.0) GO TO 7C
  DO 60 J=1,NSTEPS
    STEPS2(J)=1
  70 DO 80 J=1,NSTEPS
    IF (STEPS2(J).EQ.0) GO TO 9C
  80 STEPS1=STEPS1+STEPS2(J)
  C      STEPS1 IS THE NUMBER OF INPUT REGIONS USED
  J=NSTEPS+1
  J=J-1
  C      J IS THE NUMBER OF OUTPUT REGIONS
  IF (STEPS1.EQ.NSTEPS) GO TO 10C
  WRITE (6,230) NSTEPS,HT(1),STEPS1
  LINES=LINES+2
  IF (STEPS1.LT.NSTEPS) GO TO 10C
  WRITE (6,240)
  CALL INDEX (1)
100 NUMB(1)=J
  C      NUMB(1) IS THE NUMBER OF OUTPUT REGIONS FOR HT(1)
  NUMN(1)=C
  L2=C
  DO 12C K=1,J
    LCCP ON OUTPUT REGIONS
    L=L2+1
    L2=L2+STEPS2(K)
    SUB1=(K-1)*25+1
    SUB2=(L1-1)*25+1

```

```

INPUT61 03643C
INPUT62 03644C
INPUT63 03645C
INPUT64 03646C
INPUT65 03647C
INPUT66 03648C
INPUT67 03649C
INPUT68 03650C
INPUT69 03651C
INPUT70 03652C
INPUT71 03653C
INPUT72 03654C
INPUT73 03655C
INPUT74 03656C
INPUT75 03657C
INPUT76 03658C
INPUT77 03659C
INPUT78 03660C
INPUT79 03661C
INPUT80 03662C
INPUT81 03663C
INPUT82 03664C
INPUT83 03665C
INPUT84 03666C
INPUT85 03667C
INPUT86 03668C
INPUT87 03669C
INPUT88 03670C
INPUT89 03671C
INPUT90 03672C
INPUT91 03673C
INPUT92 03674C
INPUT93 03675C
INPUT94 03676C
INPUT95 03677C
INPUT96 03678C
INPUT97 03679C
INPUT98 03680C
INPUT99 03681C
INPUT100 03682C
INPUT101 03683C
INPUT102 03684C
INPUT103 03685C
INPUT104 03686C
INPUT105 03687C
INPUT106 03688C
INPUT107 03689C
INPUT108 03690C
INPUT109 03691C
INPUT110 03692C
INPUT111 03693C
INPUT112 03694C
INPUT113 03695C
INPUT114 03696C
INPUT115 03697C
INPUT116 03698C
INPUT117 03699C
INPUT118 03700C
INPUT119 03701C
INPUT120 03702C

```



```

MINRG(SUB1)=MINRG(SUB2)
MAXRG(SUB1)=MAXRG(SUB2)
MINDF(SUB1)=MINDF(SUB2)
MAXDF(SUB1)=MAXDF(SUB2)
LA(SUB1)=LA(SUB2)
KA(SUB1)=KA(SUB2)
IF (L1-EQ.L2) GO TO 120
L1=L1+1
DO 110 L=L1,L2
  LOOP ON INPUT REGIONS BEING COMBINED
  SUB2=(L-1)*25+1
  IF (MINRG(SUB2).LT.MINRG(SUB1)) MINRG(SUB1)=MINRG(SUB2)
  IF (MAXRG(SUB2).GT.MAXRG(SUB1)) MAXRG(SUB1)=MAXRG(SUB2)
  IF (MINDF(SUB2).LT.MINDF(SUB1)) MINDF(SUB1)=MINDF(SUB2)
  IF (MAXDF(SUB2).GT.MAXDF(SUB1)) MAXDF(SUB1)=MAXDF(SUB2)
  LA(SUB1)=LA(SUB1)+LA(SUB2)
  KA(SUB1)=KA(SUB1)+KA(SUB2)
  110 XSP(SUB1)=LA(SUB1)/KA(SUB1)
  120 NBS=J
  NORM1=0.
  DO 130 J=1,NBS
    SUB1=(J-1)*25+1
    XBB3(SUB1)=MAXRG(SUB1)-MINRG(SUB1)
    XBB4(SUB1)=MAXDF(SUB1)-MINDF(SUB1)
    XDCSET(SUB1)=MINRG(SUB1)+XBB3(SUB1)/2.
    XDCSET(SUB1)=MINDF(SUB1)+XBB4(SUB1)/2.
    NORM1=NORM1+KA(SUB1)
    NORM2=XBB3(SUB1)*XBB4(SUB1)
    NORM=SQRT(NORM1/NORM2)
    XBB3(SUB1)=XBB3(SUB1)*NORM
    XBB4(SUB1)=XBB4(SUB1)*NORM
    DO 140 J=2,NBS
      SUB1=(J-1)*25+1
      SUB2=(J-2)*25+1
      NORM2=XBB3(SUB1)*XBB4(SUB1)
      IF (XBB4(SUB1).GT.XBB4(SUB2)) GO TO 140
      XBB4(SUB1)=XBB4(SUB2)+.000001
      XBB3(SUB1)=NORM2/XBB4(SUB1)
      GO TO 150
    140 IF (XBB3(SUB1).GT.XBB3(SUB2)) GO TO 150
      XBB3(SUB1)=XBB3(SUB2)+.000001
      XBB4(SUB1)=NORM2/XBB3(SUB1)
    150 LIM1=XDCSET(SUB2)-XBB4(SUB2)/2.
      LIM5=XDCSET(SUB1)-XBB4(SUB1)/2.
      IF (LIM1.GT.LIM5) GO TO 160
      XDCSET(SUB1)=XDCSET(SUB1)-LIM5+LIM1-.0000001
      GO TO 170
    160 LIM2=LIM1+XBB4(SUB2)
      LIM6=LIM5+XBB4(SUB1)
      IF (LIM2.LT.LIM6) GO TO 170
      XDCSET(SUB1)=XDCSET(SUB1)+LIM2-LIM6+.0000001
    170 LIM3=XDCSET(SUB2)-XBB3(SUB2)/2.
      LIM7=XDCSET(SUB1)-XBB3(SUB1)/2.
      IF (LIM3.GT.LIM7) GO TO 180
      XDCSET(SUB1)=XDCSET(SUB1)-LIM7+LIM3-.0000001
      GO TO 190
    180 LIM4=LIM3+XBB3(SUB2)
      LIM8=LIM7+XBB3(SUB1)
      IF (LIM4.LT.LIM8) GO TO 190
      XDCSET(SUB1)=XDCSET(SUB1)+LIM4-LIM8+.0000001

```

```

INPUT121 037030
INPUT122 037040
INPUT123 037050
INPUT124 037060
INPUT125 037070
INPUT126 037080
INPUT127 037090
INPUT128 037100
INPUT129 037110
INPUT130 037120
INPUT131 037130
INPUT132 037140
INPUT133 037150
INPUT134 037160
INPUT135 037170
INPUT136 037180
INPUT137 037190
INPUT138 037200
INPUT139 037210
INPUT140 037220
INPUT141 037230
INPUT142 037240
INPUT143 037250
INPUT144 037260
INPUT145 037270
INPUT146 037280
INPUT147 037290
INPUT148 037300
INPUT149 037310
INPUT150 037320
INPUT151 037330
INPUT152 037340
INPUT153 037350
INPUT154 037360
INPUT155 037370
INPUT156 037380
INPUT157 037390
INPUT158 037400
INPUT159 037410
INPUT160 037420
INPUT161 037430
INPUT162 037440
INPUT163 037450
INPUT164 037460
INPUT165 037470
INPUT166 037480
INPUT167 037490
INPUT168 037500
INPUT169 037510
INPUT170 037520
INPUT171 037530
INPUT172 037540
INPUT173 037550
INPUT174 037560
INPUT175 037570
INPUT176 037580
INPUT177 037590
INPUT178 037600
INPUT179 037610
INPUT180 037620

```

```

190 CONTINUE
   IF (JAA(2).NE.10HSYMMETRY ) GO TO 210
   DU 200 J=1,NBS
   SUB1=(J-1)*25+1
   LA(SUB1)=2.*LA(SUB1)
   KA(SUB1)=2.*KA(SUB1)
   XCDS1(SUB1)=0.
   200 XBB4(SUB1)=XBB4(SUB1)*2.
   210 RETURN
C
   220 FORMAT (12F5.1)
   230 FORMAT (/32H THE DAMAGE FUNCTION ON FILE HAS,13,50H REGIONS OF DIF,INPU192 037740
   IFERENT PD. THE DATA CARDS FOR HOB =,F6.2,20H METERS SPECIFY THAT,INPU193 037750
   23,9H BE USED.)
   240 FORMAT (23HOTHIS IS A FATAL ERROR.)
      END

```

```

INPU181 037630
INPU182 037640
INPU183 037650
INPU184 037660
INPU185 037670
INPU186 037680
INPU187 037690
INPU188 037700
INPU189 037710
INPU190 037720
INPU191 037730
INPU192 037740
INPU193 037750
INPU194 037760
INPU195 037770
INPU196- 037780

```

```

C
SUBROUTINE CHBN
COMMON /COM1/COM1(20100)
DIMENSION ZI(25,25,25),SZZ(50,25)
EQUIVALENCE (COM1(1),ZI(1,1,1)),(COM1(15626),SZZ(1,1))

C
COMMON /COM3/COM3(10000)
DIMENSION NN(25),HT(25),DF(25),HOB(25),PK01(25),PK02(25),PK1(25),
1 PK2(25),PK3PL(25),PK2PL(25),PK3PL(25),PKPS(25),
2 PSALL(25),SZBAR(25),SZZ(25),SZZ(25),SZZ(25),SZZ(25),
3 SZZ(25),IFMT(1)
EQUIVALENCE (COM3(1878),NN(1)),(COM3(1916),HT(1))
1 (COM3(3045),DF(1)),(COM3(3070),HOB(1))
2 (COM3(3095),PK01(1)),(COM3(3120),PK02(1))
3 (COM3(3145),PK1(1)),(COM3(3170),PK2(1))
4 (COM3(3195),PK3PL(1)),(COM3(3220),PK2PL(1))
5 (COM3(3245),PK3PL(1)),(COM3(3270),PKPS(1))
6 (COM3(3295),PSALL(1)),(COM3(3320),SZBAR(1))
7 (COM3(3345),SZZ(1)),(COM3(3370),SZZ(1))
8 (COM3(3395),SZZ(1)),(COM3(3420),SZZ(1))
9 (COM3(3445),IFMT(1)),(COM3(3486),NVEH(1))
A (COM3(1000C),NHTS)

C
COMMON /AAA/AAA(8)
COMMON /PAGE/LINES,PAGE

C
EQUIVALENCE (NHOB,FNHOB),(I,FI)

C
DIMENSION FMT2(15),FMT4(17)

C
INTEGER AAA,FMT2,FMT4,PAGE

C
DATA (FMT2(1),I=1,15)/10H(19H ,10HVOLLEY SZ,10HE =,15,911
1 ,10H1/),10H(19H ,10HVOLLEY SZ,10HE =,15,911
2 ,10H1/1H ,16X,,10H1011/),10H(19H ,10HVOLLEY SZ
3 ,10HE =,15,911,10H1/1H ,16X,,10H1011/1H ,10H20X,511/)/
DATA (FMT4(1),I=1,17)/10H(14HOTARGE,10HT NUMBER,1,1CH3,2H =,F9,
1 ,1CH6,9F11.6),10H(14HOTARGE,10HT NUMBER,1,1CH3,2H =,F9,
2 ,10H6,9F11.6/1,10HH ,20X,10F,10H11.6),10H(14HOTARGE
3 ,10HT NUMBER,1,1CH3,2H =,F9,10H6,9F11.6/1,10HH ,20X,10F
4 ,10H11.6/1H ,2,10H4X,5F11.6)/

C
IF (AAA(1).NE.10HCPTIMIZE ) GO TO 20
AAA(6)=AAA(1)
AAA(7)=AAA(2)
10 AAA(8)=10HDONE
GO TO 50
20 IF (AAA(1).NE.10HALL HOB3 ) GO TO 40
DF(1)=1./FLOAT(NHTS)
NHOB=NHTS
DO 3C I=1,NHOB
HOB(I)=HT(I)
30 DF(I)=DF(1)
GO TO 50
40 IF (AAA(1).NE.10HHOB DISTR1) GO TO 50
DECODE (1C,520,AAA(3) )FNHOB
NHOB=FNHOB+1
READ (5,520) (HOB(L),L=1,NHCB)
50 DO 6C K=1,NVEH

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```

DO 6C I=1,NVS
60 SZZ(K,I)=0.
WRITE (6,580)
IF (AAA(6).EQ.1CHOPTIMIZE .AND.AAA(8).EQ.1CHDOONE ) 60 TO 180CMBN 61 C36390
LINES=(PAGE-21-4*((NHQB-1)/10)-(NVEH-1)*((NVS-1)/10+2))/2 CMBN 62 C38400
IF (LINES) 90,70,80 CMBN 63 C38410
70 WRITE (6,590) CMBN 64 C38420
GO TO 90 CMBN 65 C38430
80 ENCODE (10,610,IFMT(1)) LINES CMBN 66 C38440
WRITE (6,IFMT) CMBN 67 C38450
90 WRITE (6,530) CMBN 68 C38460
I1=1 CMBN 69 C38470
I2=NHQB CMBN 70 C38480
IF (I2.GT.10) I2=10 CMBN 71 C38490
100 WRITE (6,540) (HQB(I),I=1,I2) CMBN 72 C38500
WRITE (6,550) (DF(I),I=1,I2) CMBN 73 C38510
IF (I2.EQ.NHQB) 60 TO 110 CMBN 74 C38520
I1=I1+1 CMBN 75 C38530
I2=I2+1 CMBN 76 C38540
IF (I2.GT.10) I2=10 CMBN 77 C38550
110 DO 140 I1=1,NHQB CMBN 78 C38560
DO 130 I2=1,NHTS CMBN 79 C38570
IF (HQB(I1).LT..999*HT(L2).CR.HQB(L1).GT.1.001*HT(L2)) 60 TO 130 CMBN 80 C38580
DO 120 K=1,NVEH CMBN 81 C38590
120 SZZ(K,I)=SZZ(K,I)+DF(L1)*ZZ(K,I,L2) CMBN 82 C38600
GO TO 140 CMBN 83 C38610
130 CONTINUE CMBN 84 C38620
WRITE (6,560) L1,HQB(L1) CMBN 85 C38630
GO TO 510 CMBN 86 C38640
140 CONTINUE CMBN 87 C38650
WRITE (6,570) CMBN 88 C38660
150 IFMT2=1 CMBN 89 C38670
IFMT4=1 CMBN 90 C38680
IF (NVS.LT.11) 60 TO 160 CMBN 91 C38690
IFMT2=5 CMBN 92 C38700
IFMT4=5 CMBN 93 C38710
IF (NVS.LT.21) 60 TO 160 CMBN 94 C38720
IFMT2=10 CMBN 95 C38730
IFMT4=11 CMBN 96 C38740
160 WRITE (6,IFMT2(IFMT2)) (NN(I),I=1,NVS) CMBN 97 C38750
DO 170 K=1,NVEH CMBN 98 C38760
WRITE (6,IFMT4(IFMT4)) K,(SZZ(K,I),I=1,NVS) CMBN 99 C38770
170 CONTINUE CMBN 100 C38780
GO TO 300 CMBN 101 C38790
C CMBN 102 C38800
OPTIMIZATION CMBN 103 C38810
180 DECODE (10,520,AAA(7)) IFI CMBN 104 C38820
I=FI*.1 CMBN 105 C38830
IF (I.EQ.0) 60 TO 200 CMBN 106 C38840
DO 190 I1=1,NVS CMBN 107 C38850
IF (I.EG.NN(I1)) 60 TO 210 CMBN 108 C38860
190 CONTINUE CMBN 109 C38870
200 I1=1 CMBN 110 C38880
210 IF (NVEH-GE.NHQB) 60 TO 230 CMBN 111 C38890
L=NVEH+1 CMBN 112 C38900
DO 220 K=L,NHQB CMBN 113 C38910
DO 220 K=L,NHQB CMBN 114 C38920
DO 220 K=L,NHQB CMBN 115 C38930
DO 220 K=L,NHQB CMBN 116 C38940
DO 220 K=L,NHQB CMBN 117 C38950
DO 220 K=L,NHQB CMBN 118 C38960
DO 220 K=L,NHQB CMBN 119 C38970
220 SZZ(K,I)=C. CMBN 120 C38980

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240 L=1,NHTS
DO 240 K=1,NVEH
C      PREVIOUSLY, WE HAD SZZ(NVEH,NVS) BUT NOW WE TREAT IT AS
C      SZZ(NHOB,NVS)
240 SZZ(L,I)=SZZ(L,I)+ZZ(K,I),L
L=1
DO 250 L=2,NHTS
IF (SZZ(L,I).GT.SZZ(L,I)) L1=L
250 CONTINUE
C      OPTIMUM HOB FOR THE SPECIFIED ATTACK LEVEL HAS BEEN DETERMINED.
C      RETURN TO SZZ(NVEH,NVS)
DO 260 K=1,NVEH
DO 260 I=1,NVS
260 SZZ(K,I)=ZZ(K,I),I
LINES=(PAGE-6-((NVS-1)/(10+2))*(NVEH+1))/2
IF (LINES) 290,270,280
270 WRITE (6,590)
GO TO 290
280 ENCODE (10,610,IFMT(1)) LINES
WRITE (6,IFMT)
290 WRITE (6,600) HT(L1),NN(I1)
GO TO 150
C
300 LINES=(3*NVEH-1)*NVEH+4
IF (AAA(4).NE.10HSYMMETRIC ) GO TO 330
K=2*NVEH
LINES=LINES+3
DO 320 I=1,NVEH
DO 310 J=1,NVS
310 SZZ(K,J)=SZZ(I,J)
320 K=K-1
NVEH=2*NVEH
C
330 IF (LINES.GT.14) LINES=14
DO 360 J=1,NVS
PSALL(J)=1.
SUM=0.
SUM2=0.
DO 340 I=1,NVEH
PS=1.-SZZ(I,J)
PSALL(J)=PSALL(J)*PS
PKPS(I)=999999.
IF (PS.GT..000001) PKPS(I)=SZZ(I,J)/PS
340 SUM=SUM+PKPS(I)
PK1(J)=PSALL(J)*SUM
DO 350 L=1,NVEH
DO 350 M=1,NVEH
IF (M.GT.L) SUM2=SUM2+PKPS(L)*PKPS(M)
350 CONTINUE
PK2(J)=PSALL(J)*SUM2
PK1PL(J)=1.-PSALL(J)
PK2PL(J)=PK1PL(J)-PK1(J)
PK3PL(J)=PK2PL(J)-PK2(J)
PKG1(J)=PSALL(J)+PK1(J)
360 PKG12(J)=PKG1(J)+PK2(J)
C
WRITE (6,580)
LINES=(PAGE-8-((NVS-1)/(10+2))*LINES)/2
IF (LINES) 390,380,370
370 ENCODE (10,610,IFMT(1)) LINES

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CMBN121 038990
CMBN122 039000
CMBN123 039010
CMBN124 039020
CMBN125 039030
CMBN126 039040
CMBN127 039050
CMBN128 039060
CMBN129 039070
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CMBN179 039570
CMBN180 039580

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WRITE (6,IFMT)
GD TO 39C
380 WRITE (6,590)
390 IF ((NVS-11)/10-1) 430,410,400
400 I4=20
I4=I3+1
GD TO 420
410 I3=NVS
420 I1=IC
I2=I1+1
GD TO 440
430 I1=NVS
C
440 IF (AAA(4).EQ.10HSYMMETRIC) WRITE (6,620)
IF (AAA(4).EQ.10HSYMMETRIC) WRITE (6,630)
WRITE (6,640) (NN(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,770) (NN(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,790) (NN(I),I=14,NVS)
WRITE (6,650) (PSALL(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PSALL(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PSALL(I),I=14,NVS)
IF (NVEH.LT.2) GO TO 450
WRITE (6,660) (PK1(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK1(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK1(I),I=14,NVS)
IF (NVEH.LT.3) GO TO 450
WRITE (6,670) (PK2(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK2(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK2(I),I=14,NVS)
450 WRITE (6,680) (PK1PL(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK1PL(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK1PL(I),I=14,NVS)
IF (NVEH.LT.2) GO TO 510
WRITE (6,690) (PK2PL(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK2PL(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK2PL(I),I=14,NVS)
IF (NVEH.LT.3) GO TO 460
WRITE (6,700) (PK3PL(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK3PL(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK3PL(I),I=14,NVS)
460 WRITE (6,710) (PK01(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK01(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK01(I),I=14,NVS)
IF (NVEH.LT.3) GO TO 510
WRITE (6,720) (PK02(I),I=1,I1)
IF (NVS-GT.10) WRITE (6,780) (PK02(I),I=12,I3)
IF (NVS-GT.20) WRITE (6,800) (PK02(I),I=14,NVS)
C
IF (AAA(4).EQ.10HSYMMETRIC) NVEH=NVEH/2
IF (NVEH.LT.2) GO TO 510
DO 46C J=1,NVS
SZBAR(J)=C.
47C I=1,NVEH
SZBAR(J)=SZBAR(J)+SZZ(1,J)
46C SZBAR(J)=SZBAR(J)/FLOAT(NVEH)
WRITE (6,730) (SZBAR(J),J=1,I1)
IF (NVS-GT.10) WRITE (6,750) (SZBAR(J),J=12,I3)
IF (NVS-GT.20) WRITE (6,800) (SZBAR(J),J=14,NVS)
IF (NVEH.LT.3) GO TO 510
DO 46C J=1,NVS

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CMBN235 040130
CMBN236W 040140
CMBN237W 040150
CMBN238W 040160
CMBN239 040170
CMBN240 040180

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S1ZZ(J)=SZZ(I,J)
I1VEH(J)=I
DO 490 I=2,NVEH
IF (SZZ(I,J).GE.S1ZZ(J)) GO TO 490
S1ZZ(J)=SZZ(I,J)
I1VEH(J)=I
490 CONTINUE
DO 500 J=1,NVS
SZZ(J)=SZZ(I,J)
I2VEH(J)=I
DO 500 I=2,NVEH
IF (SZZ(I,J).LE.S2ZZ(J)) GO TO 500
S2ZZ(J)=SZZ(I,J)
I2VEH(J)=I
500 CONTINUE
WRITE (6,740) (I1VEH(J),J=1,I1)
IF (NVS.GT.10) WRITE (6,770) (I1VEH(J),J=12,I3)
IF (NVS.GT.20) WRITE (6,790) (I1VEH(J),J=14,NVS)
WRITE (6,760) (S1ZZ(J),J=1,I1)
IF (NVS.GT.10) WRITE (6,780) (S1ZZ(J),J=12,I3)
IF (NVS.GT.20) WRITE (6,800) (S1ZZ(J),J=14,NVS)
WRITE (6,750) (I2VEH(J),J=1,I1)
IF (NVS.GT.10) WRITE (6,770) (I2VEH(J),J=12,I3)
IF (NVS.GT.20) WRITE (6,790) (I2VEH(J),J=14,NVS)
WRITE (6,760) (S2ZZ(J),J=1,I1)
IF (NVS.GT.10) WRITE (6,780) (S2ZZ(J),J=12,I3)
IF (NVS.GT.20) WRITE (6,800) (S2ZZ(J),J=14,NVS)
510 IF (AAA(6).NE.1)CHOPTIMIZE .OR.AAA(6).EQ.1)HODONE
GO TO 10
C
520 FORMAT (8F10.4)
530 FORMAT (1H,51X,28H THE HOB DISTRIBUTION FOLLOWS////)
540 FORMAT (1H0,24X,6H08 =,10F10.2)
550 FORMAT (1H0,5X,25H FRACTION OF POPULATION =,10F10.3)
560 FORMAT (////5H0+08,12,2H)=,F6.2,112H METERS, OF THIS DISTRIBUTION
IN, DOES NOT COME WITHIN .1 PER CENT OF ANY HOB FOR WHICH PROBABILITIES
2TIES OF DAMAGE ARE/68H CURRENTLY AVAILABLE. THEREFOR, THIS HOB DISC
3TRIBUTION IS TERMINATED.)
570 FORMAT (////1H0,25X,81H PROBABILITIES OF DAMAGE AVERAGED OVER THE
1HOB DISTRIBUTION FOR EACH TARGET FOLLOW////)
580 FORMAT (1H1)
590 FORMAT (1H)
600 FORMAT (1H,18X,40H PD'S FOR EACH TARGET WITH OPTIMUM FUZING (HOB=,
1F6.2,22H METERS, ATTACK LEVEL=,13,19H ROUNDS PER CANNON)////)
610 FORMAT (1H,12,7H(//))
620 FORMAT (1H,46X,38H THE SYSTEM DAMAGE PROBABILITIES FOLLOW,6(//))
630 FORMAT (1H,16X,55H THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO
1 SYMPETRY) DAMAGE PROBABILITIES FOLLOW,6(//))
VOLLEY SIZE =,17,91,0)
640 FORMAT (26H
ALL SURVIVE =,10F10.5)
650 FORMAT (126H
EXACTLY ONE DAMAGED =,10F10.5)
660 FORMAT (26H
EXACTLY TWO DAMAGED =,10F10.5)
670 FORMAT (26H
AT LEAST ONE DAMAGED =,10F10.5)
680 FORMAT (26H
AT LEAST TWO DAMAGED =,10F10.5)
690 FORMAT (26H
AT LEAST THREE DAMAGED =,10F10.5)
700 FORMAT (26H
LESS THAN TWO DAMAGED =,10F10.5)
710 FORMAT (26H
LESS THAN THREE DAMAGED =,10F10.5)
720 FORMAT (26H
AVERAGE PER TARGET =,10F10.5)
730 FORMAT (26H
LEAST PROBABLE TARGET =,10F10.5)
740

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CMBN241 040190
CMBN242 040200
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CMBN293 040710
CMBN294 040720
CMBN295 040730
CMBN296 040740
CMBN297 040750
CMBN298 040760
CMBN299 040770
CMBN300 040780

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750 FORMAT (2GH0 MOST PROBABLE TARGET =,10110)
760 FORMAT (2GH0 PROBABILITY =,1CF10.5)
770 FORMAT (1H ,25X,10110)
780 FORMAT (1H ,48X,1CF10.5)
790 FORMAT (1H ,26X,1C110)
800 FORMAT (1H ,31X,9F10.5)
END

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CHBN301 040790
CHBN302 040800
CHBN303 040810
CHBN304 040820
CHBN305 040830
CHBN306 040840
CHBN307- 040850

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C
SUBROUTINE SEXUN4
COMMON /COM3/COM3(10000)
DIMENSION VDYN(92),NSP(46),M(40,46),Q(4,46),SGST(46),PLATE(20)
1 T(20),THETA(20),CV(20),ALFAV(20),BETAV(20)
2 GAMAV(20),LMDAV(20),KFCFTRV(20),CM(20),ALFAM(20)
3 BETAM(20),GAMAM(20),LMDAM(20),KFCFTRM(20),EXPVR(20)
4 EXPVR(20),QVR(20),QMR(20),LMDAV(20),LMDAM(20),GMAV(20)
5 GMA(20)
EQUIVALENCE (COM3(231),VDYN(1)),(COM3(323),NSP(1))
1 (COM3(369),M(1,1)),(COM3(2209),Q(1,1))
2 (COM3(4049),SGST(1)),(COM3(4187),PLATE(1))
3 (COM3(4207),T(1)),(COM3(4227),THETA(1))
4 (COM3(4247),METAL(1)),(COM3(4267),CV(1))
5 (COM3(4287),ALFAV(1)),(COM3(4307),BETAV(1))
6 (COM3(4327),GAMAV(1)),(COM3(4347),LMDAV(1))
7 (COM3(4367),KFCFTRV(1)),(COM3(4387),CH(1))
8 (COM3(4407),ALFAM(1)),(COM3(4427),BETAM(1))
9 (COM3(4447),GAMAM(1)),(COM3(4467),LMDAM(1))
A (COM3(4487),KFCFTRM(1)),(COM3(4507),EXPVR(1))
B (COM3(4527),EXPVR(1)),(COM3(4547),QVR(1))
C (COM3(4567),QMR(1)),(COM3(4587),LMDAV(1))
D (COM3(4607),LMDAM(1)),(COM3(4627),GMAV(1))
E (COM3(4647),GMA(1)),(COM3(4667),RAT(1))
EQUIVALENCE (COM3(4668),RAT(1)),(COM3(4669),RAT(1))
1 (COM3(4670),RAT(1)),(COM3(9910),PHK)
2 (COM3(9911),MMR1), (COM3(9912),VVVR1)
3 (COM3(9913),MMR1), (COM3(9914),VVVR1), (COM3(9915),K1)
4 (COM3(9916),L1), (COM3(9917),K2), (COM3(9918),KEY)
5 (COM3(9919),SECANT), (COM3(9920),SGSTBR)
6 (COM3(9921),PHKBR), (COM3(9922),ITHETA)
7 (COM3(9923),NTHETA,FNTHET), (COM3(9924),QQQ)
8 (COM3(9925),NTHOR), (COM3(9926),NTHOR,FNTHOR)
9 (COM3(9927),IPLATE), (COM3(9928),NPLATE,FNPLAT)
A (COM3(9934),VCTFLG), (COM3(9937),FRGFLG)
B (COM3(9940),SHAPE), (COM3(9941),AA), (COM3(9942),NNSP)
C (COM3(9961),VTERH), (COM3(9983),K22), (COM3(9984),K22)
COMMON /AAA/AAA(8)
COMMON /CONST/CONST(6)
EQUIVALENCE (CONST(3),UGTOR)
COMMON /PAGE/LINES,PAGE
C
DIMENSION IFMT1(23),WORD(2)
EQUIVALENCE (CUMY,IDUMYV)
C
INTEGER AAA,FRGFLG,PAGE,PLATE,VCTFLG,WORD
REAL KFCFTRM,KFCFTRV,LMDAM,LMDAV,LMDAM,LMDAV,M,MMR1,MMHRI
C
DATA (WCRO(I),I=1,2) /1CH (MED) ,1CH (MAX) /
DATA (IFMT1(I),I=1,23)/1CH(1H),31(//),1CH,1H,42X,4,10H6H1HE THOR
1 1CH CONSTANTS,10H FOR THE F,10HOLLOWING C,10HASES ARE,5
2 1CH(//),1H,55,4CH,1HC,7X,5,1CHMALPHA,5X,10H4HBETA,6X,
3 10H5HGAMMA,4X,1CH,CHLAMBDA,1CH5X,PHKFCFTR,10H(//1H),23X
4 1CH,ALC,5X,1,10HCHV RESIDU,10HAL,6FL0,3,10H1HC,38X,1H
5 1CHMM RESIDUA,10HL,6FL0,5),10H( 1H1/ ,10H 1H,42X,4/
C
10 READ (5,2E0) (AAA(I),I=1,8)
IF (AAA(1),EQ,1CH) COMPUTE .OR. AAA(1),EQ,1CH COMPUTE .OF. AAA(1),ESEXUN4,9
10.1CH COMPUTE .OF. AAA(1),EQ,1CH COMPUTE) GU TO 100
SEXUN4 2 040860
SEXUN4 3 040870
SEXUN4 4 040880
SEXUN4 5 040890
SEXUN4 6 040900
SEXUN4 7 040910
SEXUN4 8 040920
SEXUN4 9 040930
SEXUN4 10 040940
SEXUN4 11 040950
SEXUN4 12 040960
SEXUN4 13 040970
SEXUN4 14 040980
SEXUN4 15 040990
SEXUN4 16 041000
SEXUN4 17 041010
SEXUN4 18 041020
SEXUN4 19 041030
SEXUN4 20 041040
SEXUN4 21 041050
SEXUN4 22 041060
SEXUN4 23 041070
SEXUN4 24 041080
SEXUN4 25 041090
SEXUN4 26 041100
SEXUN4 27 041110
SEXUN4 28 041120
SEXUN4 29 041130
SEXUN4 30 041140
SEXUN4 31 041150
SEXUN4 32 041160
SEXUN4 33 041170
SEXUN4 34 041180
SEXUN4 35 041190
SEXUN4 36 041200
SEXUN4 37 041210
SEXUN4 38 041220
SEXUN4 39 041230
SEXUN4 40 041240
SEXUN4 41 041250
SEXUN4 42 041260
SEXUN4 43 041270
SEXUN4 44 041280
SEXUN4 45 041290
SEXUN4 46 041300
SEXUN4 47 041310
SEXUN4 48 041320
SEXUN4 49 041330
SEXUN4 50 041340
SEXUN4 51 041350
SEXUN4 52 041360
SEXUN4 53 041370
SEXUN4 54 041380
SEXUN4 55 041390
SEXUN4 56 041400
SEXUN4 57 041410
SEXUN4 58 041420
SEXUN4 59 041430
SEXUN4 60 041440
SEXUN4 61 041450

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C
IF (AAA(1),NE,1CHFRAGMENTAT) GO TO 20
FRGFLG=1
VCTFLG=1
CALL FRAG1 (1HO)
WRITE (6,320) SHAPE,AA
CALL FRAG2 (1HO)
GO TO 1C

C
20 IF (AAA(1),NE,1CHTERMINAL V) GO TO 30
VCTFLG=1
DECODE (1C,290,AAA(3)) JVTIRM
GO TO 1C

C
30 IF (AAA(1),NE,1CHTHOR DATA .AND. AAA(1),NE,1CH THOR DATA) GO TO 60
DECODE (1C,290,AAA(2)) IFNTHOR
NTHOR=FNTHOR+.1
READ (5,310) (METAL(1),CV(1),ALFAV(1),BETAV(1),GAMAV(1),LANDAV(1),
1 KFCTRV(1),CM(1),ALFAM(1),BETAM(1),GAMAM(1),LANDAM(1),KFCTRM(1),
2 I=1,NTHOR)
LINES=PAGE-7-5*NTHOR
IF (LINES.LT.0) GO TO 40
LINES=LINES/2+2
ENCODE (2C,33C,IFMT1(1)) LINES
GO TO 50

40 IFMT1(1)=IFMT1(22)
IFMT1(2)=IFMT1(23)

50 WRITE (6,1FMT1) (METAL(1),CV(1),ALFAV(1),BETAV(1),GAMAV(1),
1 LANDAV(1),KFCTRV(1),CM(1),ALFAM(1),BETAM(1),GAMAM(1),LANDAM(1),
2 KFCTRM(1),I=1,NTHOR)
GO TO 1C

C
60 IF (AAA(1),NE,1CHANGLES .AND. AAA(1),NE,1CH ANGLES .AND. AAA(1),NE,1CH
1.NE,1CH ANGLES .AND. AAA(1),NE,1CH ANGLES .AND. AAA(1),NE,1CH
2 ANGLES) GO TO 70
DECODE (7C,29C,AAA(2)) IFNTHET,(THETA(1),I=1,6)
NTHETA=FNTHET+.1
IF (NTHETA.GT.6) READ (5,29C) (THETA(1),I=7,NTHETA)
GO TO 1C

C
70 IF (AAA(1),NE,1CHARMOR .AND. AAA(1),NE,1CH ARMOR .AND. AAA(1),NE,1CH
1.NE,1CH ARMOR .AND. AAA(1),NE,1CH ARMOR .AND. AAA(1),NE,1CH
2 ARMOR .AND. AAA(1),NE,1CH ARMOR) GO TO 80
DECODE (1C,29C,AAA(2)) IFNPLAT
NPLATE=FNPLAT+.1
READ (5,30C) (PLATE(1),I=1,NPLATE)
GO TO 1C

C
80 IF (AAA(1),NE,1CHINCAPACITAT) GO TO 90
DUMMY=INCAP(DUMMY,DUMMY,AAA(4))
GO TO 1C

C
90 IF (AAA(1),EG,1CHSECTION IV) GO TO 10
RETURN

C
END OF INPUT DATA

C
100 IF (FRGFLG.EQ.1) GO TO 130
FRGFLG=1
DL 12C K2=K22,K222

```

```

SEXU461 C4146C
SEXU462 041470
SEXU463 041480
SEXU464 041490
SEXU465 041500
SEXU466W 041510
SEXU467 041520
SEXU468 04153C
SEXU469 041540
SEXU470 04155C
SEXU471 041560
SEXU472* 041570
SEXU473 041580
SEXU474 041590
SEXU475 041600
SEXU476* 041610
SEXU477 04162C
SEXU478R 04163C
SEXU479R 04164C
SEXU480R 041650
SEXU481 041660
SEXU482 041670
SEXU483 041680
SEXU484* 041690
SEXU485 04170C
SEXU486 04171C
SEXU487 041720
SEXU488W 041730
SEXU489W 041740
SEXU490W 041750
SEXU491 041760
SEXU492 041770
SEXU493 041780
SEXU494 041790
SEXU495 041800
SEXU496* 041810
SEXU497 041820
SEXU498R 04183C
SEXU499 04184C
SEXU500 041850
SEXU501 041860
SEXU502 04187C
SEXU503 041880
SEXU504* 041890
SEXU505 04190C
SEXU506R 041910
SEXU507 04192C
SEXU508 04193C
SEXU509 04194C
SEXU510 041950
SEXU511 041960
SEXU512 04197C
SEXU513 04198C
SEXU514 041990
SEXU515 04200C
SEXU516 04201C
SEXU517 04202C
SEXU518 04203C
SEXU519 04204C
SEXU520 04205C

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```

IF (SGST(K2).EQ.0.) GO TO 120
NNSP=NSP(K2)
DO 110 K1=1,NNSP
110 M(K1,K2)=10.**M(K1,K2)
120 CONTINUE
130 IF (VCTFLG.NE.1) GO TO 140
CALL VECTR
VCTFLG=0
140 QQC=((.0610234*SHAPE)**(-2./3.))
DUMMY=PPKFCN(QCG,DUMMY,IDUMMY)
IPLATE=0
150 IPLATE=IPLATE+1
DO 160 ITHOR=1,INTHOR
IF (METAL(ITHOR).EQ.PLATE(IPLATE)) GO TO 190
160 CONTINUE
WRITE (6,380) IPLATE,PLATE(IPLATE)
IF (IPLATE.EQ.NPLATE) GO TO 180
IPLATE=IPLATE+1
DO 170 JPLATE=IPLATE,NPLATE
PLATE(JPLATE-1)=PLATE(JPLATE)
170 I(JPLATE-1)=I(JPLATE)
IPLATE=IPLATE-1
180 NPLATE=NPLATE-1
GO TO 200
190 EXPVR(IPLATE)=2.*ALFAM(ITHOR)/3.+8ETAV(ITHOR)
EXPVR(IPLATE)=2.*ALFAM(ITHOR)/3.+8ETAM(ITHOR)
QQC=I(IPLATE)*SHAPE**(-2./3.)
QVR(IPLATE)=10.**CV(ITHOR)*QQC**ALFAM(ITHOR)
QMR(IPLATE)=10.**CM(ITHOR)*QQC**ALFAM(ITHOR)
LMDAV(IPLATE)=LMDAV(ITHOR)
LMDAM(IPLATE)=LMDAM(ITHOR)
GMAV(IPLATE)=GMAV(ITHOR)
GMAM(IPLATE)=GMAM(ITHOR)
FROM THOR 70, KFCTRM(2024)=-.964 AND KFCTRV(2024)=-.965
RATGM=1.
RATIOV=1.
IF (KFCTRM(IPLATE).NE.0.) RATIOV=KFCTRM(IPLATE)/.964
IF (KFCTRV(IPLATE).NE.0.) RATIOV=KFCTRV(IPLATE)/.965
RATOM1=1.-RATIOV
RATOV1=1.-RATIOV
200 IF (IPLATE.LT.NPLATE) GO TO 150
DO 270 IPLATE=1,NPLATE
DO 260 ITHETA=1,INTHETA
WRITE (6,34C) PLATE(IPLATE),I(ITHETA),THETA(ITHETA),VTERM
PHKBAR=C.
SGSTR=C.
SECANT=1000000000.
IF (ABS(THETA(ITHETA)).LE.89.) SECANT=1./COS(THETA(ITHETA)*DGTOR)
GVR(IPLATE)=GVR(IPLATE)*SECANT**GMAV(IPLATE)
QMR(IPLATE)=QMR(IPLATE)*SECANT**GMAM(IPLATE)
DO 240 K2=K22,K222
IF (SGST(K2).EQ.0.) GO TO 24C
NNSP=NSP(K2)
DO 230 L=1,NNSP
KEY=2
K1=NNSP-L+1
VVVR=VDYN(K2+(KEY-1)*46)
MMR=MI(K1,K2)
VVVR1=VVVR-QVR(IPLATE)*MMR**EXPVR(IPLATE)*VVVR**LMDAV(IPLATE)
VVVR1=VVVR1+RATEV1+VVVR1*QATICV

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SEXU121 042060
SEXU122 04207C
SEXU123 042080
SEXU124 042090
SEXU125 04210C
SEXU126 042110
SEXU127 042120
SEXU128 042130
SEXU129 042140
SEXU130 042150
SEXU131 042160
SEXU132 042170
SEXU133 042180
SEXU134 042190
SEXU135 042200
SEXU136M 042210
SEXU137 042220
SEXU138 042230
SEXU139 04224C
SEXU140 042250
SEXU141 042260
SEXU142 042270
SEXU143 042280
SEXU144 042290
SEXU145 042300
SEXU146 042310
SEXU147 042320
SEXU148 042330
SEXU149 042340
SEXU150 042350
SEXU151 042360
SEXU152 042370
SEXU153 042380
SEXU154 042390
SEXU155 042400
SEXU156 042410
SEXU157 04242C
SEXU158 042430
SEXU159 04244C
SEXU160 042450
SEXU161 042460
SEXU162 04247C
SEXU163 042480
SEXU164M 042490
SEXU165 042500
SEXU166 042510
SEXU167 042520
SEXU168 042530
SEXU169 042540
SEXU170 042550
SEXU171 042560
SEXU172 04257C
SEXU173 042580
SEXU174 042590
SEXU175 042600
SEXU176 042610
SEXU177 042620
SEXU178 04263C
SEXU179 04264C
SEXU15C 042650

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IF (VVVR1.LE.C.) GO TO (230,240), KEY
MMR1=MMR-OMR(IPLATE)*MMR**EXP(K(IPLATE)*VVVR**LMDAM(IPLATE))
MMR1=MMR+RATOR1+MMR1*RAT10M
IF (MMR1.LE.C.) GO TO (240,220), KEY
MMR=MMR1
VVVR=VVVR1
IF (SGSTR.EQ.C.) WRITE (6,350)
PKH=PKFCN(MMR,VVVR,JDUMY)
WRITE (6,360) K2,VDYN(K2*(KEY-1)*46),WORD(KEY),MK1,K2),VVVR,MMR,
1 PKH
PKBAR=PKBAR+PKH*SGST(K2)*Q(K1,K2)
SGSTR=SGSTR+SGST(K2)*Q(K1,K2)
220 KEY=KEY-1
230 CONTINUE
240 CONTINUE
IF (SGSTR.NE.0.) GO TO 250
WRITE (6,390)
GO TO 270
250 PKBAR=PKBAR/SGSTR
WRITE (6,370) PKBAR
QVR(IPLATE)=QVR(IPLATE)*SECANT**(-GMV(IPLATE))
OMR(IPLATE)=OMR(IPLATE)*SECANT**(-GMH(IPLATE))
260 CONTINUE
270 CONTINUE
GO TO 1C

C
280 FORMAT (8A10)
290 FORMAT (8E10.4)
300 FORMAT (4A10,4F10.4)
310 FORMAT (A10,6F10.4,10X,6F10.4)
320 FORMAT (1H,15H SHAPE FACTOR =,F6.1,5H A =,F5.3/)
330 FORMAT (5H(1H,12,13H(,1H,42X,4)
340 FORMAT (1H,12X,A10,F7.2,25H INCHES THICK THETA =,F6.2,34H DEG
1REES PROJECTILE VELOCITY =,F8.2,16H FEET PER SECOND)
350 FORMAT (/1H0,28X,5HSPRAY,8X,6HV IMPACT,9X,8HM IMPACT,5X,10HV RESID
1UAL,4X,10CM RESIDUAL,5X,4HPI/H)
360 FORMAT (1H0,28X,13,E16.4,6,3E14.4,F9.4)
370 FORMAT (15H0 MEAN PI/H =,F12.4)
380 FORMAT (1H,24(,1H,35X,12HPLATE NUMBER,13,4H IS ,A10,1H,71H0,35
1X,61H10R CONSTANTS FOR THIS MATERIAL ARE NOT CURRENTLY AVAILABLE.
21H0,35X,35HTHEREFOR, THIS PLATE IS TERMINATED.)
390 FORMAT (1H,10(,1H0,43X,45HTHIS PLATE ASSEMBLY SUSTAINED NO PERF
1GATIONS)
END
SEXU181 042660
SEXU182 042670
SEXU183 042680
SEXU184 042690
SEXU185 042700
SEXU186 042710
SEXU187 042720
SEXU188 042730
SEXU189 042740
SEXU190 042750
SEXU191 042760
SEXU192 042770
SEXU193 042780
SEXU194 042790
SEXU195 042800
SEXU196 042810
SEXU197 042820
SEXU198 042830
SEXU199 042840
SEXU200 042850
SEXU201 042860
SEXU202 042870
SEXU203 042880
SEXU204 042890
SEXU205 042900
SEXU206 042910
SEXU207 042920
SEXU208 042930
SEXU209 042940
SEXU210 042950
SEXU211 042960
SEXU212 042970
SEXU213 042980
SEXU214 042990
SEXU215 043000
SEXU216 043010
SEXU217 043020
SEXU218 043030
SEXU219 043040
SEXU220 043050
SEXU221 043060
SEXU222 043070
SEXU223 043080
SEXU224 043090
SEXU225- 043100

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```

C      FUNCTION PKFCN (AA,BB,II)
      A=AA
      B=BB
      PKFCN=0.
      V50=
      IF (B.LT.V50) GO TO 1C
      C=
      IF (C.GT.CDEF2) PKFCN=
      10 RETURN

C      ENTRY INCAP
      DECODE (40,30,II) KEY,CDEF1,CDEF2,CDEF3
      WRITE (6,40) KEY,CDEF1,CDEF2,CDEF3
      GO TO 1C

C      ENTRY PPKFCN
      D=AA
      IF (KEY.EQ.10HSUMMER ) GO TO 20
      COEF4=14630000.*D
      COEF5=-1666300.*D
      GO TO 10
      20 COEF4=7543000.*D
      COEF5=-1794200.*D
      GO TO 1C

C      30 FORMAT (A10,7E10.4)
      40 FORMAT (1H1,29I1,1H ,37X,57HTHE INCAPACITATION PARAMETERS FOR THE
      1 FOLLOWING CASES ARE//1H0,37X,A10,3E17.5)
      END

```

```

*4301*27 043110
PKFCN 2 043120
PKFCN 3 043130
PKFCN 4 043140
PKFCN 5 043150
PKFCN 6 043160
PKFCN 7 043170
PKFCN 8 043180
PKFCN 9 043190
PKFCN10 043200
PKFCN11 043210
PKFCN12 043220
PKFCN13* 043230
PKFCN14W 043240
PKFCN15 043250
PKFCN16 043260
PKFCN17E 043270
PKFCN18 043280
PKFCN19 043290
PKFCN20 043300
PKFCN21 043310
PKFCN22 043320
PKFCN23 043330
PKFCN24 043340
PKFCN25 043350
PKFCN26 043360
PKFCN27 043370
PKFCN28 043380
PKFCN29 043390
PKFCN30- 043400

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APPENDIX B

PROBABILITY OF INCAPACITATION EQUATIONS

This appendix presents sufficient information concerning the probability of incapacitation equations for soldiers (references 5 and 8) to allow those equations to be encoded in a manner compatible with the LASVEM computer program. The equations themselves have been deleted from this report in order to keep it unclassified.

Cards PKFCN 6 with cards PKFCN 20, PKFCN 21, PKFCN 23, and PKFCN 24 compute a V_{50} level as described in paragraph 1 of reference 8. That reference uses a factor, 'A', the mean presented area in centimeters squared. Centimeters must be converted to inches and the presented area must be eliminated:

$$A = \left(\frac{M}{.0610234 \cdot \text{SHAPE}} \right)^{2/3} \quad \text{Equation B-1}$$

Note that card SEXU129 incorporates the factor, .0610234, and that card SEXU188, which is the call to function PKFCN, defines AA, BB and, in turn A, B, as fragment mass and speed, respectively.

Cards PKFCN 8 and PKFCN 9 compute the probability of incapacitating a soldier with a fragment of mass A (in grains) and velocity B (in fps). Reference 6 uses the three variables a, b, and n which are encoded as COEF1, COEF2, and COEF3, respectively.

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APPENDIX C

AN ILLUSTRATIVE EXAMPLE

This appendix provides an example of the use of this methodology from start to finish. Although the example is typical, it is very simple. None of the data necessarily represent actual or developmental systems. Not all the options of the program are exercised, nor is all of the output shown.

We wish to determine measures of the damage sustained by a force of four APC's when the force is fired upon by artillery firing HE shell fuzed for air burst. The APC's are oriented in the direction of fire. A scenario such as this might be useful for determining the protection provided to the occupants by the APC armor against friendly supporting fires. The scenario is depicted in Figure C-1.

Various numbers of rounds will be fired by one howitzer battery consisting of six cannon. The aiming policy is battery parallel sheaf with a hypothetical cannon at the battery's geometrical center aiming at the center of the APC force. Ballistic data and fuze data are shown in Table C-1. APC structure is indicated by a shop diagram at Figure C-2. Data for the individual APC armor plates are in Table C-2. We use one perforation as the damage criterion.

First, program section IV will be used to determine which plates have any chance of sustaining perforations. There are two reasons for using section IV:

1. Plates identified as not sustaining any perforations can be eliminated from consideration, thus conserving both machine time and user effort.
2. An estimate of the average probability of incapacitation of soldiers hit by residual fragments will be produced.

The input data deck is at Figures C-3 and C-4. Plates D and E are not considered at all because they are shielded from fragmentation by suspension and mobility components and from direct hits by the rest of the APC. Data from other sources indicates that the spaced armor will not sustain perforations. Results of this first step are summarized in Table C-3. A sample of the output is at Figure C-5.

Plates C, F, and H sustain no damage from fragmentation; however, they may sustain massive damage from direct hits and very near misses (see paragraph 4.1). Although we may process all three of these plates for direct hits and very near misses without error, we need process only plate F, because the hits and very near misses on plate C

Text continues on page 170.

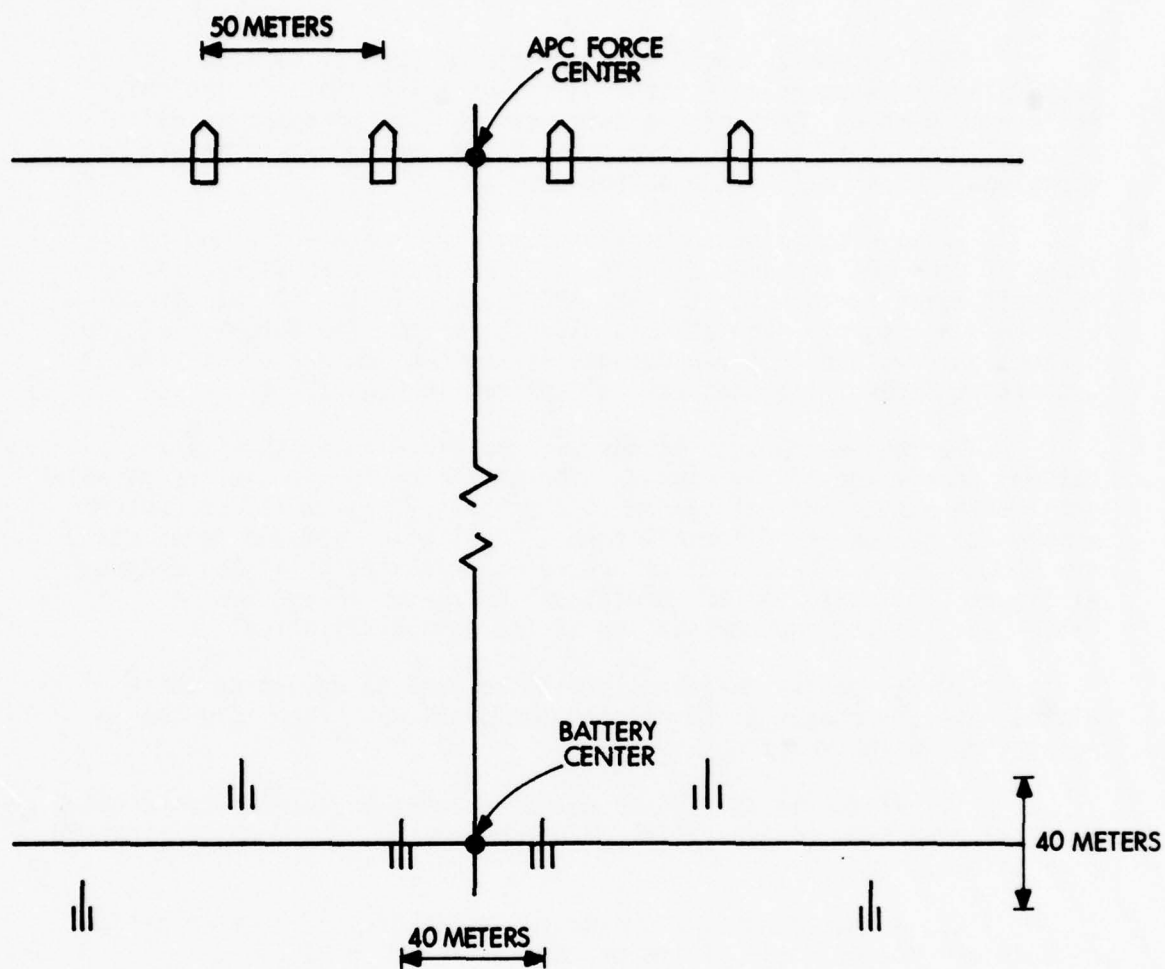


Figure C-1. (U) Geometry of the Firing Battery and APC Force.

TABLE C-1. BALLISTIC AND FUZE DATA

Projectile Terminal Velocity	850. Ft/Sec			
Projectile Angle of Fall	30.°			
Fuze Reliability	.95			
Fuze HOB Distribution:				
HOB (Meters):	.3	5.	12.	
Fraction of Population:	.03	.80	.17	
Precision Error Standard Deviation, Range	36. meters			
Precision Error Standard Deviation, Deflection	6. meters			
MPI Error Standard Deviation, Range	45. meters			
MPI Error Standard Deviation, Deflection	27. meters			

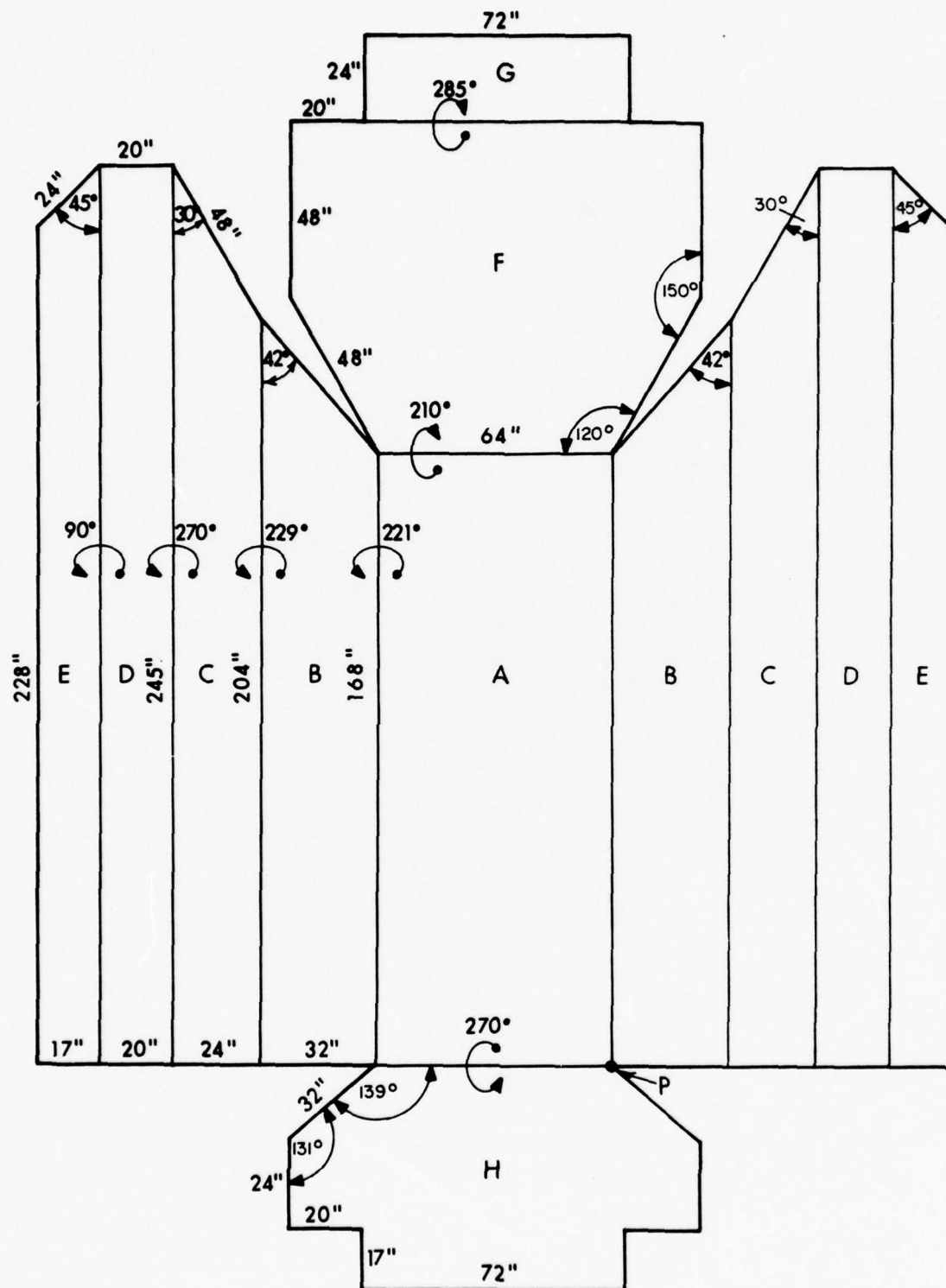


Figure C-2. (U) APC Structure, Shop Diagram.

TABLE C-2. PLATE DATA

Plate or Plate Pair	Material	Thickness in Inches	Inclination to Horizontal	Surface Area in Inches ²	Height of Top Edge or Surface above Ground in Inches
A	7039 Aluminum	1.5	0.°	10752.	78.
B	2024 Aluminum	1.6	41.°	2X5948.	78.
C	Spaced Armor	*	90.°	2X5389.	57.
D } E }	Shielded from fragmentation by tracks, roadwheels, skirts, etc.				
F	Hard Homo- geneous Steel	2.0	30.°	9034.	78.
G	7039 Aluminum	2.0	135.°	1728.	33.
H	Hard Homo- geneous Steel	2.0	90.°	5772.	78.

*The spaced armor consists of 3 plates. From outermost to innermost, they are:

.25 inches hard homogeneous steel
.20 inches hard homogeneous steel
1.12 inches 7039 aluminum

FRAGMENTATION DATA

	19.	15.	640.	0.032	4.	1.	3.	5.
	7.	16.	13.	5.	14.	7.	6.	7.
	10.	13.	21.	26.				
	1.	0.0645	22.	24.				
5.2600	1.	0.0645	0.6800	0.0968	1.4900	0.2581	3.4680	0.0323
132.6670	5.2600	0.0323	9.9500	0.0968	10.5330	0.0323	21.0200	0.0968
309.0000	132.6670	0.0645	157.0000	0.0323	245.0000	0.0323	259.0000	0.0323
	309.0000	0.0323	493.0000	0.0323	622.0000	0.0645	5250.0000	
2.	2.	0.2857	0.4210	0.2381	1.5540	0.0952	2.9150	0.0238
5.8900	5.8900	0.0238	9.2300	0.0238	11.7700	0.0476	18.5900	0.0238
22.2200	22.2200	0.0238	25.4700	0.0714	40.6730	0.0476	66.5000	0.0476
480.0000	480.0000	0.0476	735.5000	0.1667	1.5000	0.1667	20.7000	0.3333
3.	3.	0.1667	0.4500	0.1667	2.9000	0.0833	9.7400	0.0833
39.5300	39.5300	0.1667	112.0000	0.0833				
4.	4.	0.7500	0.2730					
27.2500	27.2500							
5.	5.	1.0000	0.0000					
6.	6.	0.3333	2.5900	0.3333	7.3600	0.3333	637.0000	0.1000
7.	7.	0.4000	0.3120	0.2000	2.8250	0.2000	6.3200	
65.2000	65.2000	0.1000	72.4000	0.1667	1.4450	0.2500	17.5000	0.1667
8.	8.	0.1667	0.6100	0.0833	492.0000	0.0833	1649.0000	0.0345
39.3000	39.3000	0.0833	56.5200	0.1034	1.5800	0.1379	2.6350	0.0690
9.	9.	0.1379	0.6750	0.0345	31.4400	0.0345	64.8000	0.1034
8.7200	8.7200	0.0345	12.7000	0.0345	128.0000	0.0345	295.0000	0.0345
76.0000	76.0000	0.0690	93.0000	0.0690	666.5000	0.0690	969.0000	
364.0000	364.0000	0.0345	424.0000	0.0488	1.3900	0.0488	2.9600	0.0488
1352.0000	1352.0000			0.0488	17.2300	0.0488	22.3000	0.0488
10.	10.	0.0976	0.7280	0.0976	64.0000	0.0244	79.3400	0.0488
6.4750	6.4750	0.0732	12.7200	0.0244	101.0000	0.0244	197.0000	0.0244
26.6000	26.6000	0.0244	51.5000	0.0488	441.5000	0.0732	543.6670	0.0488
83.5000	83.5000	0.0244	98.9000	0.0137				
221.0000	221.0000	0.0488	357.5000	0.0137				
952.0000	952.0000	0.0244	1535.0000	0.0137				
11.	11.	0.0274	0.6300	0.0137	1.1900	0.0685	3.2860	0.0548
6.4350	6.4350	0.0137	8.1700	0.0411	12.4330	0.0822	16.8620	0.0137
20.1500	20.1500	0.0411	32.2670	0.0548	44.6200	0.0274	55.0000	0.0411
76.3330	76.3330	0.0137	84.7200	0.0822	112.0000	0.0137	128.0000	0.0822
175.3330	175.3330	0.0548	274.5000	0.0548	333.2500	0.0411	426.0000	0.0411
651.3330	651.3330	0.0685	844.4000	0.0137	1525.0000	0.0137	1634.0000	0.0137
2135.0000	2135.0000	0.0137	2634.0000	0.0137	3050.0000			
12.	12.	0.1250	0.7000	0.0625	1.7100	0.0625	6.8400	0.0625
9.8400	9.8400	0.0625	11.9600	0.0625	19.1400	0.0625	28.3700	0.0625
66.0000	66.0000	0.0625	75.8000	0.0625	96.8000	0.1250	175.5000	0.0625
1200.0000	1200.0000	0.0625	1470.0000	0.0625	2760.0000			
13.	13.	0.3636	3.5850	0.1818	14.2700	0.0909	16.7900	0.0909
32.7200	32.7200	0.0909	64.2200	0.0909	71.4000	0.0909	128.0000	0.0909
14.	14.	0.4091	0.4440	0.3636	1.1390	0.0909	3.2900	0.0455
52.0000	52.0000	0.0455	85.0000	0.0455	149.0000			
15.	15.	0.7000	0.3730	0.1000	1.4470	0.1000	2.6120	0.0167
5.1400	5.1400	0.0167	11.0400	0.0333	21.6350	0.0333	32.3200	0.0417
16.	16.	0.4167	0.2000	0.0833	1.4500	0.0833	3.0950	0.0417
				0.0417	22.8000	0.1667	46.1000	0.0417

5.1400	0.0167	11.0400	0.0333	21.6350	0.0333	32.3200	0.0417
16.	0.4167	0.2000	0.0833	1.4500	0.0833	3.0950	0.0417
9.9700	0.0417	16.5700	0.0417	22.8000	0.1667	46.1000	
56.8000	0.0417	73.6600	0.0417	84.4400			
17.	0.5000	0.2600	0.0526	1.8000	0.1053	3.3920	0.0526
12.3100	0.0263	40.8000	0.0526	64.4000	0.0263	88.2600	0.0526
128.5000	0.0263	159.0000	0.0263	17.0000	0.0263	603.0000	0.0263
1200.0000	0.1274	0.4920	0.1863	1.3780	0.1765	3.4610	0.0686
18.	0.0098	8.4200	0.0392	13.2150	0.0196	15.3600	0.0294
6.2430	0.0392	27.5380	0.0490	42.2500	0.0294	59.7270	0.0098
21.1600	0.0098	74.9530	0.0098	113.4000	0.0098	141.5000	0.0686
65.6000	0.0098	210.0000	0.0098	351.0000	0.0098	427.0000	0.0098
173.7140	0.0534	0.5000	0.0840	1.4360	0.1374	3.5540	0.0667
539.0000	0.0382	9.3120	0.0840	11.8020	0.0382	17.0320	0.0076
19.	0.0687	30.9840	0.0611	40.3350	0.0534	55.5170	0.0153
6.4190	0.0229	75.4070	0.0382	83.5440	0.0229	94.5400	0.0305
20.9000	0.0153	132.0000	0.0305	159.7500	0.0153	270.0000	0.0153
62.7000	0.0153	450.5000	0.0153	656.0000	0.0305	814.0000	0.0382
110.5000							
346.5000							
1871.0000							
1.	0.0	5.0	2300.0	2452.0	0.0	0.0	
2.	5.0	15.0	2550.0	3014.0	0.0	0.0	
3.	15.0	25.0	2730.0	3088.0	0.0	0.0	
4.	25.0	35.0	2900.0	3163.0	0.0	0.0	
5.	35.0	45.0	3038.0	3238.0	0.0	0.0	
6.	45.0	55.0	3250.0	3950.0	35.6	40.0	
7.	55.0	65.0	2900.0	3550.0	111.0	117.0	
8.	65.0	75.0	3650.0	4200.0	132.8	129.0	
9.	75.0	85.0	3950.0	4500.0	322.5	299.0	
10.	85.0	95.0	4200.0	4700.0	455.6	416.0	
11.	95.0	105.0	3150.0	4450.0	811.1	752.0	
12.	105.0	115.0	1850.0	2250.0	177.0	172.0	
13.	115.0	125.0	1950.0	2050.0	121.4	128.0	
14.	125.0	135.0	2400.0	3250.0	243.3	290.0	
15.	135.0	145.0	2350.0	2950.0	545.6	775.0	
16.	145.0	155.0	2050.0	2400.0	150.6	275.0	
17.	155.0	165.0	2200.0	2550.0	147.6	394.0	
18.	165.0	175.0	2250.0	2800.0	135.2	711.0	
19.	175.0	180.0	2550.0	2900.0	65.5	2740.0	

FIGURE C-3. INPUT DATA, FRAGMENTATION

The Following Page is Blank.

SECTION IV
 *** THE FRAGMENTATION DATA DECK OF FIGURE C-3 IS INSERTED HERE ***
 TERMINAL VELOCITY 850.
 THOP DATA 3.
 AL 7039 7.047 1.029 -1.072 1.251 -1.139 1.016
 -6.663 .227 .694 -.361 1.901 1.021
 AL 2024 7.047 1.029 -1.072 1.251 -1.139 1.985
 -6.663 .227 .694 -.361 1.901 .964
 HHS 6.475 .889 -.945 1.262 .019
 -2.264 .346 .629 .880
 ANGLES 1.
 INCAPACITATION PARAMETERS WINTER .0616454 31000. .48781
 ARMOR 4.
 AL 7039 1.5 AL 7039 2.0 AL 2024 1.6 HHS 2.0
 COMPUTE
 END OF DATA

FIGURE C-4. INPUT DATA DECK FOR PROGRAM SECTION IV

TABLE C-3. RESULTS OF PROGRAM SECTION IV

<u>PLATE</u>	<u>PERFORATED</u>	<u>P_{I/H}</u>
A	yes	.83
B	yes	.62
C	no	-
D	no	-
E	no	-
F	no	-
G	yes	.65
H	no	-

AL 7039 1.50 INCHES THICK THETA = 0.00 DEGREES PROJECTILE VELOCITY = 850.00 FEET PER SECOND

SPRAY	V IMPACT	M IMPACT	V RESIDUAL	M RESIDUAL	PI/H
8	.4561E+04 (MAX)	.1649E+04	.9909E+03	.1225E+04	.9946
8	.4021E+04 (MED)	.1649E+04	.3875E+03	.1315E+04	.9339
9	.4722E+04 (MAX)	.1352E+04	.8863E+03	.9686E+03	.9863
9	.4182E+04 (MED)	.1352E+04	.2808E+03	.1048E+04	0.0000
9	.4722E+04 (MAX)	.9690E+03	.3599E+03	.6797E+03	.8446
10	.4776E+04 (MAX)	.1535E+04	.1129E+04	.1099E+04	.9957
10	.4285E+04 (MED)	.1535E+04	.5628E+03	.1180E+04	.9690
10	.4776E+04 (MAX)	.5520E+03	.3908E+03	.6608E+03	.8579
11	.4383E+04 (MAX)	.3050E+04	.1552E+04	.2388E+04	1.0000
11	.3117E+04 (MED)	.3050E+04	.1480E+03	.2704E+04	0.0000
11	.4383E+04 (MAX)	.2634E+04	.1387E+04	.2649E+04	.9998
11	.4383E+04 (MAX)	.2135E+04	.1134E+04	.1645E+04	.9987
11	.4363E+04 (MAX)	.1634E+04	.7803E+03	.1244E+04	.9879
11	.4383E+04 (MAX)	.1525E+04	.6830E+03	.1157E+04	.9791

MEAN PI/H = .8274E+00

FIGURE C-5. OUTPUT OF PROGRAM SECTION IV FOR ONE OF THE ARMOR PLATES.

and on plate H will be accounted for on plates B and F and on plate A, respectively. Thus, for HOB = .3 meters, (HOB assumed to be half the projectile length for impact functioning rounds) we consider plates A, B, F, and G, and for HOB = 5. and 12. meters, we consider plates A, B, and G. It should be obvious that plate G will sustain little damage.

For the computations of program sections I and II, we use a four inch cell at HOB = .3 meters and an eight inch cell otherwise. We assign a value of four feet to the blast effects sphere radius. We define plate A to be the reference plate to which the other plates will be assembled; therefore, the offsets of the various plates' central cells are defined with respect to the central cell of plate A (central cells and their offsets are discussed in paragraphs 4.1 and 5.1). Data for the individual plates of the structure serving as the model of our APC are at Table C-4. The input data deck for this second stage of the computations is at Figure C-6.

Samples of the output from program section I are at Figures C-7 through C-9. Table C-5 contains the important parameters computed by program section I.

We note that our intuition concerning plate G was correct; it has sustained no damage. We note further that for HOB's greater than 473. inches (55 eight inch cells plus 33 inches height of the top edge of plate G above the ground), plate G would present zero surface area to the burst and so could not sustain any perforations. Considerations such as these can be important when machine time becomes large. The source of the uncertainty in the values for plate B at HOB = 12. meters is clear from examination of Figure C-9; perforations might be sustained beyond the left deflection limit of the matrix used. Any error, however, is quite small. Finally, all these values refer to a half-infinite ground plane.

The output of program section II is at Figures C-10 through C-12. We note that, due to the possible error in the values for plate B at HOB = 12. meters, the 12 meter values for the complete structure may incorporate a small error. Again these values refer to a half-infinite ground plane.

Figures C-13 and C-14 present an index of the expected perforations file and a tabulation of the damage function file, respectively. Although not produced by program section II, these are presented here because the input data card which caused them to be produced was a part of the data deck shown in Figure C-6. The first several logical records (which are not shown) of the damage function file pertain to the individual plates with non-zero probability of damage (Table C-5). Damage function file logical records 8, 9, and 10 refer to the complete structure at HOB = .3, 5., and 12. meters, respectively. Had the data deck of Figure C-6 been split up into two parts, one for program section I and the other for program section II, then an examination of the section I

Text continues on page 193.

TABLE C-4. DATA FOR STRUCTURE APPROXIMATING APC OF FIGURE C-2.

Plate	Dimensions in No. of Cells		Inclination to Horizontal in Degrees	Height of Top Surface or Edge Above Ground	Surface Area Scale Factor	Central Cell Offset		
	Along Range Axis	Along Deflection Axis				Along Range Axis	Along Deflection Axis	
<u>4-inch cells</u>								
A	42	16	0	78	1.000	22 ⁺	9 ⁺	
B	46	16*	41	78	.9899	2	0	
F		26	30	78	1.013	21	0	
G		18	135	33	1.000	40	0	
<u>8-inch cells</u>								
A	21	8	0	78	1.000	11 ⁺	5 ⁺	
B	23	8*	41	78	.9899	1	0	
G		9	135	33	1.000	21	0	

*Separation between top edges of two halves of plate pair.

⁺Location of central cell, rather than offset, with respect to point P of Figure C-2.

BASIC DATA
 1. .3
 1. 1.5
 1. 1.
 42. 16.
 1. 1.
 THOR DATA
 AL 7039 7.047 1.029 -1.072 1.251 -.139 1.016
 -6.663 .227 .694 -.361 1.901 1.021
 850. 48.
 30. *** THE FRAGMENTATION DATA DECK OF FIGURE C-3 IS INSERTED HERE ***
 CONTOUR
 NO PROBABILITY MATRIX
 BASIC DATA
 1. .3
 1. 2.
 1. 1.
 18. 1. 135. 33.
 1. 1.
 30. 850.
 CONTOUR
 NO PROBABILITY MATRIX
 BASIC DATA
 1. .3
 1. 1.6
 1. 1.
 46. 16.
 1. 1.
 8. 2. 41. 78. .9899
 THOR DATA
 AL 2024 7.047 1.029 -1.072 1.251 -.139 .965
 -6.663 .227 .694 -.361 1.901 .964
 850. 48.
 30. CONTOUR
 NO PROBABILITY MATRIX
 BASIC DATA
 1. .3
 1. 2.
 1. 1.
 26. 1. 30. 78. 1.013
 1. THOR DATA
 HHS 6.475 .889 -.945 1.262 .019
 -2.264 .346 .629 .327 .880
 850. 48.
 30. CONTOUR
 NO PROBABILITY MATRIX
 BASIC DATA
 2. 5.
 1. 1.5
 1. 1.
 21. 8.
 1. 1. 78.

```

1. 78.
21.
1.
THOR DATA
AL 7039 7.047 1.029 -1.072 1.251 1.016
-6.663 .227 .694 -.361 1.901 1.021
850. 48.
NO PROBABILITY MATRIX
BASIC DATA 8. 100. 55. 0.
2. 12.
1.
1.
3. 1. 135. 33.
1.
30. 48.
NO PROBABILITY MATRIX
BASIC DATA 8. 100. 55. 0.
2. 12.
1. 1.6
1.
23. 8. 4. 2. 41. 78. .9899
1.
THOR DATA
AL 2024 7.047 1.029 -1.072 1.251 .965
-6.663 .227 .694 -.361 1.901 .964
850. 48.
NO PROBABILITY MATRIX
CONTOUR 3.
CONTOUR ASSEMBLE 1. 3. 4. 2.
4. 1. 2. 40.
SHIFT X = 3. 2. 21.
5. 9. 7.
SHIFT X = 1. 21.
3. 10. 6.
EXPECTED PERFORATIONS FILE
END OF DATA
DAMAGE FUNCTION FILE

```

FIGURE C-6. INPUT DATA DECK FOR PROGRAM SECTIONS I AND II

The following page is blank.

HOB# = .30 METERS THICKNESS=1.50 INCHES CELL = 4.00 INCHES NX= 42 CELLS NY= 16 CELLS NZ= 0 CELLS T= 76.0 INCHES
SCALE FACTOR APPLIED TO INPUT PLATE = 1./1.000

NXX=10C CELLS	NYN=100 CELLS	PROJECTILE LOCATION WAS (55.5, .5)
---------------	---------------	-------------------------------------

THE EXPECTED PERFORATIONS MATRIX FOR THIS CASE IS ON THE EXPECTED PERFORATIONS FILE (PMAT348) AS RECORD NUMBER 1

LETHAL AREA=	13.626	SQAUPE METERS	AVERAGE PROBABILITY OF DAMAGE =1.000	OVER	13.626	SQAUPE METERS
--------------	--------	---------------	--------------------------------------	------	--------	---------------

OUTPUT OF THE PROBABILITY OF DAMAGE MATRIX HAS BEEN SUPPRESSED

THE PROBABILITY CONTOURS FOR THIS TARGET, HQ8, AND DAMAGE CRITERION FOLLOW. THE NUMBERS ARE PD*10. (TRUNCATED), AND E=CJC5, *1.0

[illegible]

2C	*
19	*
18	*
17	*
16	*
15	*
14	*
13	*
12	*
11	*
10	*
9	*
8	*
7	*
6	*
5	*
4	*
3	*
2	*
1	*

[illegible]

THESE DATA ARE ON THE DAMAGE FUNCTION FILE (DFCN348) AS RECORD NUMBER 1

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2	DAMAGE AREA IN METERS**2
	PER REGION	CUMULATIVE

THESE DATA ARE ON THE DAMAGE FUNCTION FILE (DFCN348) AS RECORD NUMBER 1

AVERAGE PD WITHIN LETHAL AREA IN METERS**2 DAMAGE AREA IN METERS**2
EACH REGION PER REGION CUMULATIVE PER REGION CUMULATIVE

1.000 13.626 13.626 13.626

AVERAGE PD WITHIN RECTANGULARIZED, UNNORMALIZED RANGE DATA RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA
EACH REGION

EXTENT OF REGION LOCATION OF REGION CENTER WRT PROJECTILE EXTENT OF REGION LOCATION OF REGION CENTER WRT PROJECTILE

METERS CELLS METERS CELLS METERS CELLS METERS CELLS

6.706 66.0 0.000 0.0 2.032 20.0 1.016 10.0

FIGURE C-7. SOME OUTPUT OF PROGRAM SECTION I FOR HOB = .3 METERS.

The following page is blank.

HOB= 5.00 METERS THICKNESS=1.60 INCHES CELL= 8.00 INCHES NX= 23 CELLS NY= 8 CELLS NZ= 4 CELLS T= 78.0 INCHES

SCALE FACTOR APPLIED TO INPUT PLATE = 1./ .990

ALPHA= 0.0 DEGREES BETA= 41.0 DEGREES 2 SIDES

NXX=100 CELLS NYY=100 CELLS PROJECTILE LOCATION WAS (55.5, .5)

THE EXPECTED PERFORATIONS MATRIX FOR THIS CASE IS ON THE EXPECTED PERFORATIONS FILE (PMAT348) AS RECORD NUMBER 9

LETHAL AREA= 21.695 SQUARE METERS AVERAGE PROBABILITY OF DAMAGE = .226 OVER 95.835 SQUARE METERS

OUTPUT OF THE PROBABILITY OF DAMAGE MATRIX HAS BEEN SUPPRESSED

THE PROBABILITY CONTOURS FOR THIS TARGET, HOB, AND DAMAGE CRITERION FOLLOW. THE NUMBERS ARE PD*10. (TRUNCATED), AND E=.0005, *=-1.0

333334444444555555566666677777777
5678901234567890123456789012345678901234567

[illegible]

333333444444555555666666777777

THESE DATA ARE ON THE DAMAGE FUNCTION FILE (DFCN348') AS RECORD NUMBER 6

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
	PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
.720	2.110	2.110	2.932	2.932
.653	4.126	6.236	6.317	9.249
.549	2.720	8.956	4.955	14.204
.448	3.055	12.012	6.813	21.017
.348	3.175	15.186	9.125	30.142
.251	2.472	17.659	9.868	40.010
.143	2.410	20.069	16.888	56.898
.042	1.627	21.695	38.937	95.835

WAVELENGTH PD WITHIN EACH REGION	RECTANGULARIZED, UNNORMALIZED RANGE DATA			RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA		
	EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE
	METERS	CELLS	METERS	METERS	CELLS	METERS
.720	2.438	12.0	- .610	1.422	7.0	3.962
.653	3.658	18.0	-1.016	3.048	15.0	3.962
.549	4.267	21.0	-1.118	4.064	20.0	4.267
.448	5.486	27.0	-1.118	4.877	24.0	4.674
.348	5.893	29.0	- .914	6.096	30.0	5.080
.248	5.904	29.0	- .914	7.112	35.0	5.080
.148	5.904	29.0	- .914	7.112	35.0	5.080

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9.868
16.888
38.937
40.010
56.898
95.835

17.859
20.069
21.695

2.472
2.410
1.627

.251
.143
.042

AVERAGE PD WITHIN EACH REGION	RECTANGULARIZED, UNNORMALIZED RANGE DATA				RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
	EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	
	METERS	CELLS	METERS	CELLS	METERS	CELLS	METERS	CELLS
.720	2.438	12.0	-.610	-3.0	1.422	7.0	3.962	19.5
.653	3.658	18.0	-1.016	-5.0	3.048	15.0	3.962	19.5
.549	4.267	21.0	-1.118	-5.5	4.064	20.0	4.267	21.0
.448	5.486	27.0	-1.118	-5.5	4.877	24.0	4.674	23.0
.348	5.893	29.0	-.914	-4.5	6.096	30.0	5.080	25.0
.251	6.706	33.0	-.711	-3.5	7.112	35.0	5.385	26.5
.143	7.518	37.0	-.305	-1.5	9.754	48.0	6.706	33.0
.042	8.738	43.0	.102	.5	14.021	69.0	8.433	41.5

FIGURE C-8. SOME OUTPUT OF PROGRAM SECTION I FOR HDB = 5 METERS.

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[illegible]

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
	PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
.134	4.787	4.787	35.675	35.675
.046	6.229	11.016	135.846	171.521

[illegible]

AVERAGE PD WITHIN EACH REGION		LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
		PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
.134		4.787	4.787	35.675	35.675
.046		6.229	11.016	135.846	171.521

AVERAGE PD WITHIN EACH REGION		RECTANGULARIZED, UNNORMALIZED RANGE DATA		RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	
		METERS	CELLS	METERS	CELLS	METERS	CELLS
.134		4.674	23.0	-4.775	-23.5	8.941	44.0
.046		14.021	69.0	-1.321	-6.5	17.069	84.0
							50.0
							58.0

FIGURE C-9. SOME OUTPUT OF PROGRAM SECTION 1 FOR HOB = 12 METERS.

TABLE C-5. TABULATED RESULTS FROM PROGRAM SECTION I

<u>Plate</u>	<u>HOB in Meters</u>	<u>Lethal Area in Meters²</u>	<u>Damage Area in Meters²</u>	<u>Average Probability of Damage</u>
A	.3	13.626	13.626	1.
	5.	9.323	18.127	.514
	12.	8.930	62.431	.143
B	.3	20.232	20.232	1.
	5.	21.535	95.835	.225
	12.	10.910+	171.521+	.064+
F	.3	11.613	11.613	1.
	5. }	Not computed; known to be 0. from section IV output		
	12. }			
G	.3	0.	0.	0.
	5.	0.	0.	0.
	12.	0.	0.	0.

The following page is blank.

OUTPUT OF THE PROBABILITY OF DAMAGE MATRIX HAS BEEN SUPPRESSED

THE PROBABILITY CONTOURS FOR THIS TARGET, HOB, AND DAMAGE CRITERION FOLLOW. THE NUMBERS ARE PD*10. (TRUNCATED), AND E=.0005, *=1.0

G00C0001111111112222222233333344444444555555556666666777777778888888899999999

[illegible]

0000000111111122222222333333334444444455555555666666667777777788888888
345678901234567890123456789012345678901234567890123456789012345678

[illegible]

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2 PER REGION	CUMULATIVE	DAMAGE AREA IN METERS**2 PER REGION	CUMULATIVE
----------------------------------	--	------------	--	------------

1.00C	24.361	24.361	24.361
-------	--------	--------	--------

AVERAGE PD WITHIN EACH REGION	RECTANGULARIZED, UNNORMALIZED RANGE DATA				RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
	EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	
	METERS	CELLS	METERS	CELLS	METERS	CELLS	METERS	CELLS
1.000	8.738	86.0	-1.016	-10.0	2.845	28.0	1.422	14.0

FIGURE C-10. OUTPUT OF PROGRAM SECTION II FOR HOB = .3 METERS.

The following page is blank.

3333333344444444555555556666666677777777
4567890123456789012345678901234567890123456

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
	PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
.936	2.512	2.512	2.684	2.684
.848	1.856	4.367	2.188	4.872
.732	3.508	7.876	4.790	9.662
.656	6.393	14.268	9.745	19.407
.552	3.371	17.639	6.111	25.518
.450	3.341	20.981	7.432	32.950
.346	3.187	24.166	9.208	42.158
.251	2.457	26.624	9.786	51.943
.142	2.384	29.009	16.805	68.749
.041	1.514	30.522	36.790	105.538

RECTANGULARIZED, UNNORMALIZED RANGE DATA	EXTENT OF REGION	LOCATION OF REGION CENTER WRT PROJECTILE	METERS	CELLS	METERS	CELLS
1	1	1	1	1	1	1
2	2	2	2	2	2	2
3	3	3	3	3	3	3
4	4	4	4	4	4	4
5	5	5	5	5	5	5
6	6	6	6	6	6	6
7	7	7	7	7	7	7
8	8	8	8	8	8	8
9	9	9	9	9	9	9
10	10	10	10	10	10	10
11	11	11	11	11	11	11
12	12	12	12	12	12	12
13	13	13	13	13	13	13
14	14	14	14	14	14	14
15	15	15	15	15	15	15
16	16	16	16	16	16	16
17	17	17	17	17	17	17
18	18	18	18	18	18	18
19	19	19	19	19	19	19
20	20	20	20	20	20	20
21	21	21	21	21	21	21
22	22	22	22	22	22	22
23	23	23	23	23	23	23
24	24	24	24	24	24	24
25	25	25	25	25	25	25
26	26	26	26	26	26	26
27	27	27	27	27	27	27
28	28	28	28	28	28	28
29	29	29	29	29	29	29
30	30	30	30	30	30	30
31	31	31	31	31	31	31
32	32	32	32	32	32	32
33	33	33	33	33	33	33
34	34	34	34	34	34	34
35	35	35	35	35	35	35
36	36	36	36	36	36	36
37	37	37	37	37	37	37
38	38	38	38	38	38	38
39	39	39	39	39	39	39
40	40	40	40	40	40	40
41	41	41	41	41	41	41
42	42	42	42	42	42	42
43	43	43	43	43	43	43
44	44	44	44	44	44	44
45	45	45	45	45	45	45
46	46	46	46	46	46	46
47	47	47	47	47	47	47
48	48	48	48	48	48	48
49	49	49	49	49	49	49
50	50	50	50	50	50	50
51	51	51	51	51	51	51
52	52	52	52	52	52	52
53	53	53	53	53	53	53
54	54	54	54	54	54	54
55	55	55	55	55	55	55
56	56	56	56	56	56	56
57	57	57	57	57	57	57
58	58	58	58	58	58	58
59	59	59	59	59	59	59
60	60	60	60	60	60	60
61	61	61	61	61	61	61
62	62	62	62	62	62	62
63	63	63	63	63	63	63
64	64	64	64	64	64	64
65	65	65	65			

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AVERAGE PD WITHIN EACH REGION	RECTANGULARIZED, UNNORMALIZED RANGE DATA				RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
	EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	
	METERS	CELLS	METERS	CELLS	METERS	CELLS	METERS	CELLS
.936	2.845	14.0	-.813	-4.0	1.016	5.0	.508	2.5
.848	4.064	20.0	-1.016	-5.0	1.422	7.0	.711	3.5
.732	5.080	25.0	-1.118	-5.5	4.674	23.0	2.337	11.5
.656	5.486	27.0	-.914	-4.5	5.486	27.0	2.743	13.5
.552	5.690	28.0	-.813	-4.0	6.299	31.0	3.150	15.5
.450	6.096	30.0	-1.016	-5.0	7.112	35.0	3.556	17.5
.346	6.299	31.0	-.914	-4.5	8.128	40.0	4.064	20.0
.251	6.706	33.0	-.914	-4.5	7.925	39.0	4.978	24.5
.142	7.518	37.0	-.506	-2.5	11.582	57.0	5.791	28.5
.041	8.738	43.0	-.102	-.5	14.021	69.0	8.433	41.5

FIGURE C-11. OUTPUT OF PROGRAM SECTION II FOR HOB = 5 METERS.

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THESE DATA ARE ON THE DAMAGE FUNCTION FILE (DFCN348) AS RECORD NUMBER 10

AVERAGE PD WITHIN EACH REGION	LETHAL AREA IN METERS**2 PER REGION	CUMULATIVE PER REGION	DAMAGE AREA IN METERS**2 PER REGION	CUMULATIVE PER REGION
1	1	1	1	1
2	4	5	4	5
3	9	14	9	14
4	16	30	16	30
5	25	55	25	55
6	36	91	36	91
7	49	140	49	140
8	64	204	64	204
9	81	285	81	285
10	100	385	100	385
11	121	506	121	506
12	144	650	144	650
13	169	819	169	819
14	196	1015	196	1015
15	225	1240	225	1240
16	256	1496	256	1496
17	289	1785	289	1785
18	324	2109	324	2109
19	361	2470	361	2470
20	400	2870	400	2870
21	441	3311	441	3311
22	484	3795	484	3795
23	529	4324	529	4324
24	576	4900	576	4900
25	625	5525	625	5525
26	676	6201	676	6201
27	729	6930	729	6930
28	784	7714	784	7714
29	841	8555	841	8555
30	900	9455	900	9455
31	961	10416	961	10416
32	1024	11440	1024	11440
33	1089	12529	1089	12529
34	1156	13685	1156	13685
35	1225	14910	1225	14910
36	1296	16206	1296	16206
37	1369	17575	1369	17575
38	1444	19019	1444	19019
39	1521	20540	1521	20540
40	1600	22140	1600	22140
41	1681	23821	1681	23821
42	1764	25585	1764	25585
43	1849	27434	1849	27434
44	1936	29370	1936	29370
45	2025	31395	2025	31395
46	2116	33511	2116	33511
47	2209	35720	2209	35720
48	2304	38024	2304	38024
49	2401	40425	2401	40425
50	2500	42925	2500	42925
51	2601	45526	2601	45526
52	2704	48230	2704	48230
53	2809	51039	2809	51039
54	2916	53955	2916	53955
55	3025	56980	3025	56980
56	3136	60116	3136	60116
57	3249	63365	3249	63365
58	3364	66729	3364	66729
59	3481	70210	3481	70210
60	3600	73810	3600	73810
61	3721	77531	3721	77531
62	3844	81375	3844	81375
63	3969	85344	3969	85344
64	4096	89440	4096	89440
65	4225	93665	4225	93665
66	4356	98021	4356	98021
67	4489	102510	4489	102510
68	4624	107134	4624	107134
69	4761	111895	4761	111895
70	4900	116805	4900	116805
71	5041	121866	5041	121866
72	5184	127080	5184	127080
73	5329	132449	5329	132449
74	5476</			

4.748 4.748

AVERAGE PD WITHIN EACH REGION		LETHAL AREA IN METERS**2		DAMAGE AREA IN METERS**2	
		PER REGION	CUMULATIVE	PER REGION	CUMULATIVE
.335	1.591	4.748	4.748		
.249	3.818	15.360	20.108		
.141	8.121	57.435	77.544		
.046	6.365	137.415	214.958		

RECTANGULARIZED, UNNORMALIZED RANGE DATA				RECTANGULARIZED, UNNORMALIZED DEFLECTION DATA			
EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE		EXTENT OF REGION		LOCATION OF REGION CENTER WRT PROJECTILE	
METERS	CELLS	METERS	CELLS	METERS	CELLS	METERS	CELLS
3.048	15.0	-4.166	-20.5	2.032	10.0	1.016	5.0
7.518	37.0	-3.150	-15.5	3.658	18.0	1.829	9.0
9.550	47.0	-2.743	-13.5	14.630	72.0	7.315	36.0
14.021	69.0	-1.524	-7.5	20.320	100.0	10.160	50.0

FIGURE C-12. OUTPUT OF PROGRAM SECTION II FOR HOB = 12 METERS.

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AN INDEX OF THE EXPECTED PERFORMATIONS FILE (PMAT348) FOLLOWS

RECORD	NXX	NYI	CELL	HOB	IRGL	ICOL	LYMYB	LYMYT	LYMXL	LYMXR	A	B	NSIDE	NX	NY	NZ	T	THCK
1	100	100	4.00	.30	C	55	1	20	23	88	6.0	0.0	0	42	16	0	78.0	1.50
2	100	100	4.00	.30	C	55	1	20	23	56	135.0	0.0	1	0	18	6	33.0	2.00
3	100	100	4.00	.30	C	55	1	28	21	90	0.0	41.0	2	42	16	8	78.0	1.60
4	100	100	4.00	.30	C	55	1	25	24	66	30.0	0.0	1	0	26	22	78.0	2.00
5	100	100	6.00	5.00	C	55	1	15	37	67	0.0	0.0	0	21	6	0	78.0	1.50
6	100	100	6.00	12.00	C	55	1	34	17	72	0.0	0.0	0	21	8	0	78.0	1.50
7	100	100	6.00	5.00	C	55	1	2	25	56	135.0	0.0	1	0	9	3	33.0	2.00
8	100	100	6.00	12.00	C	55	1	2	25	56	135.0	0.0	1	0	9	3	33.0	2.00
9	100	100	6.00	5.00	C	55	8	76	35	77	0.0	41.0	2	23	6	4	78.0	1.60
10	100	100	6.00	12.00	C	55	17	100	15	83	0.0	41.0	2	23	8	4	76.0	1.60

FIGURE C-13. INDEX OF THE EXPECTED PERFORMATIONS MATRIX FILE.

A TABULATION OF THE DAMAGE FUNCTION FILE (DFCN348) FOLLOWS

RECORD NUMBER	POINT NUMBER	SYMMETRY CHARACTER	DAMAGE CRITERION	LYMXL	LYMYR	LYMYB	LYMYT	PROJECTILE LOCATION	HOB (METERS)	CELL (INCHES)	NUMBER OF REGIONS
8	1	C	1	3	68	1	28	(55.5, .5)	.30	4.00	1

DAMAGE FUNCTION REGIONS

POBAR	LETHAL AREA	DAMAGE AREA	DIMENSIONS IN METERS (UNNORMALIZED)	RANGE	DEFLECTION	OFFSET OF MIDPOINT WRT PROJECTILE IN METERS	..ANGE	DEFLECTION
1.000	8.738	2.845	-1.016	1.422		24.361	24.361	

RECORD NUMBER	POINT NUMBER	SYMMETRY CHARACTER	DAMAGE CRITERION	LYMXL	LYMYR	LYMYB	LYMYT	PROJECTILE LOCATION	HOB (METERS)	CELL (INCHES)	NUMBER OF REGIONS
9	2	C	1	34	76	1	76	(55.5, .5)	5.00	8.00	10

DAMAGE FUNCTION REGIONS

POBAR	LETHAL AREA	DAMAGE AREA	DIMENSIONS IN METERS (UNNORMALIZED)	RANGE	DEFLECTION	OFFSET OF MIDPOINT WRT PROJECTILE IN METERS	RANGE	DEFLECTION
.041	8.738	14.021	-1.02	8.433		1.514	36.790	
7.518	11.582	-50F	5.791	2.384		16.805	.251	
7.925	-914	4.978	2.457	9.786		.346	6.299	
-914	4.064	3.187	9.208	.450		6.096	7.112	
3.556	3.341	7.432	.552	5.690		6.299	-813	
3.371	6.111	.656	5.486	-1.118		-914	2.743	
9.745	.732	5.080	4.674	.711		2.337	3.506	
.848	4.064	1.422	-1.016	.508		1.856	2.188	
2.845	1.016	-813	.508	2.512		2.684	.038	
.024	.017	.010	.003	0.000		0.000	0.000	

RECORD NUMBER	POINT NUMBER	SYMMETRY CHARACTER	DAMAGE CRITERION	LYMXL	LYMYR	LYMYB	LYMYT	PROJECTILE LOCATION	HOB (METERS)	CELL (INCHES)	NUMBER OF REGIONS
10	3	C	1	14	62	1	100	(55.5, .5)	12.00	8.00	4

DAMAGE FUNCTION REGIONS

POBAR	LETHAL AREA	DAMAGE AREA	DIMENSIONS IN METERS (UNNORMALIZED)	OFFSET OF MIDPOINT WRT PROJECTILE IN METERS

10 3 C 1 14 62 1 100 (55.5, .5) 12.00 8.00 4

DAMAGE FUNCTION REGIONS					OFFSET OF MIDPOINT WRT PROJECTILE IN METERS	
PDBAR	LETHAL AREA	DAMAGE AREA	DIMENSIONS IN METERS (UNNORMALIZED) RANGE DEFLECTION		RANGE	DEFLECTION
.046	14.021	20.320	-1.524	10.160	6.365	137.415
9.550	14.630	-2.743	7.315	8.121	57.435	.249
3.658	-3.150	1.829	3.818	15.360	.335	3.048
-4.166	1.016	1.591	4.746	.450	6.096	7.112

2
FIGURE C-14. A TABULATION OF THE DAMAGE FUNCTION FILE. RECORDS NUMBERED 1 THRU 7 HAVE BEEN DELETED BY THE AUTHOR.

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results would have shown that plate G could have been eliminated from the section II deck, since it contributed nothing. Although very little would have been gained in this example, in some cases this sort of "one-step-at-a-time" analysis can save significant amounts of machine time.

We have already obtained some results of value for our APC model: lethal areas, average damage probabilities, probability of vulnerability of a single APC. Now we will use program section III to obtain measures of the damage sustained by the APC force fired upon by the howitzer battery (Figure C-1). Figures C-10 through C-12 provide contour plots for the damage functions, and we see that in each case, the damage function is "fully nested" (see paragraph 6.1). The damage functions input to program section III are constructed from those output by program section II using judgement and experience.

In this example, we make two different approximations to the damage functions output by program section II in order to give some rough idea of how results for program section III might depend upon the input damage function. The input data deck is at Figure C-15. The first approximation results in "cookie cutter" damage functions; that is, all the different probability of damage regions are combined to obtain one region with a constant probability of damage. For the second approximation, we rectangularize (maintaining normalization) the various probability of damage regions, without combining any of them.

Results of program section III for these approximations to the damage functions are at Figures C-16 and C-17. One should not assume that the differences in results for different approximations to the damage functions will always be as small as they are in this example.

ENCOUNTER 6.	2.	6.	3.	12.	
-20.	0.	0.	20.	-20.	
100.	60.	-20.	-60.	-100.	
0.	0.				
75.	25.				
1.	3.	4.	5.	10.	20.
2.	45.	27.	.95	15.	
36.	6.				
DFCN348	SYMMETRY 8.				
DFCN34F	SYMMETRY 9.				
DFCN346	SYMMETRY 10.				
HOB DISTRIBUTION	3.	SYMMETRIC ARRAY		OPTIMIZE 5.	
.3	12.				
.63	.80	6.	3.	12.	
ENCOUNTER 6.	.17				
SAME CANNON	2.				
SAME TARGETS					
SAME VOLLEYS					
SAME ERRORS					
DFCN348	SYMMETRY 8.				
DFCN346	SYMMETRY 9.				
DFCN348	SYMMETRY 10.				
SAME HOB DISTRIBUTION		SYMMETRIC ARRAY		OPTIMIZE 5.	
END OF DATA					

FIGURE C-15. INPUT DATA DECK FOR PROGRAM SECTION III

AD-A068 976

ARMY MATERIEL SYSTEMS ANALYSIS ACTIVITY ABERDEEN PROV--ETC F/G 19/3
LIGHTLY ARMORED STRUCTURE VULNERABILITY ESTIMATION METHODOLOGY --ETC(U)
JAN 79 C J LAPOINTE
AMSAA-TR-254

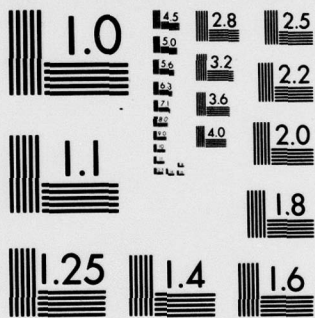
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

DAMAGE FUNCTION NUMBER 8 FROM FILE DFCN348 FOR H08 = .30 HAS 1 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS	OFFSET OF MIDPOINT FROM TARGET CENTER
	RANGE DEFLECTION	RANGE DEFLECTION
1.000	8.65 5.63	-1.02 0.00

DAMAGE FUNCTION NUMBER 9 FROM FILE DFCN348 FOR H08 = 5.00 HAS 1 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS	OFFSET OF MIDPOINT FROM TARGET CENTER
	RANGE DEFLECTION	RANGE DEFLECTION
.289	7.73 27.32	-.10 0.00

DAMAGE FUNCTION NUMBER 10 FROM FILE DFCN348 FOR H08 = 12.00 HAS 1 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS	OFFSET OF MIDPOINT FROM TARGET CENTER
	RANGE DEFLECTION	RANGE DEFLECTION
.093	12.18 35.30	-1.52 0.00

TARGET NUMBER 1 LOCATED AT (0.00, 75.00)

VOLLEY SIZE =	1	2	3	4	5	10	15	20
PD(H08 = .30) =	.007267	.014403	.021410	.028293	.035053	.067108	.096481	.123453
PD(H08 = 5.00) =	.009055	.017983	.026786	.035466	.044024	.085072	.123379	.159161
PD(H08 = 12.00) =	.005862	.011678	.017446	.023168	.028843	.056547	.083160	.108731

TARGET NUMBER 2 LOCATED AT (0.00, 25.00)

VOLLEY SIZE =	1	2	3	4	5	10	15	20
PD(H08 = .30) =	.007841	.015540	.023098	.030519	.037807	.072347	.103975	.133005
PD(H08 = 5.00) =	.009331	.019522	.029076	.038495	.047781	.092297	.133808	.172552
PD(H08 = 12.00) =	.006380	.012768	.018983	.025207	.031380	.061489	.090384	.118119

PD(HOB= 5.00) = .009831 .019522 .029076 .038495 .047781 .092297 .133808 .172552
 PD(HOB= 12.00) = .006380 .012768 .018983 .025207 .031380 .061489 .090384 .118119

THE HOB DISTRIBUTION FOLLOWS

HOB = .30 5.00 12.00
 FRACTION OF POPULATION = .030 .600 .170

PROBABILITIES OF DAMAGE AVERAGED OVER THE HOB DISTRIBUTION FOR EACH TARGET FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20
 TARGET NUMBER 1 = .008459 .016804 .025037 .033160 .041174 .079684 .115735 .149516
 TARGET NUMBER 2 = .009184 .018244 .027181 .035997 .044694 .086461 .125531 .162112

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20
 ALL SURVIVE = .96518 .93172 .89958 .86869 .83900 .70685 .59793 .50781
 EXACTLY ONE DAMAGED = .03436 .06648 .09647 .12446 .15056 .25620 .32819 .37505
 EXACTLY TWO DAMAGED = .00046 .00178 .00388 .00668 .01013 .03480 .06750 .10379
 AT LEAST ONE DAMAGED = .03482 .06828 .10042 .13131 .16100 .29315 .40207 .49219
 AT LEAST TWO DAMAGED = .00046 .00180 .00395 .00684 .01043 .03695 .07388 .11714
 AT LEAST THREE DAMAGED = .00000 .00002 .00007 .00016 .00031 .00215 .00638 .01334
 LESS THAN TWO DAMAGED = .99954 .99820 .99605 .99316 .98957 .96305 .92612 .88286
 LESS THAN THREE DAMAGED = 1.00000 .99998 .99993 .99984 .99969 .99785 .99362 .98666
 AVERAGE PER TARGET = .00882 .01752 .02611 .03458 .04293 .08307 .12063 .15581

PD'S FOR EACH TARGET WITH OPTIMUM FUZING (HOB= 5.00 METERS, ATTACK LEVEL= 5 ROUNDS PER CANNON)

VOLLEY SIZE = 1 2 3 4 5 10 15 20
 TARGET NUMBER 1 = .009055 .017983 .026786 .035466 .044024 .085072 .123379 .159161
 TARGET NUMBER 2 = .009831 .019522 .029076 .038495 .047781 .092297 .133808 .172552

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20

VOLLEY SIZE =	1	2	3	4	5	10	15	20
TARGET NUMBER 1 =	.009055	.017983	.026786	.035466	.044024	.085072	.123379	.159161
TARGET NUMBER 2 =	.009831	.019522	.029076	.038495	.047781	.092297	.133808	.172552

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE =	1	2	3	4	5	10	15	20
ALL SURVIVE =	.96276	.92707	.89287	.86008	.82864	.68970	.57657	.48407
EXACTLY ONE DAMAGED =	.03671	.07087	.10263	.13212	.15948	.26852	.34043	.38515
EXACTLY TWO DAMAGED =	.00052	.00203	.00442	.00761	.01150	.03918	.07532	.11483
AT LEAST ONE DAMAGED =	.03724	.07293	.10713	.13992	.17136	.31030	.42343	.51593
AT LEAST TWO DAMAGED =	.00053	.00206	.00451	.00780	.01188	.04178	.08300	.13078
AT LEAST THREE DAMAGED =	.00000	.00003	.00009	.00020	.00037	.00260	.00767	.01596
LESS THAN TWO DAMAGED =	.99947	.99794	.99549	.99220	.98812	.95822	.91700	.86922
LESS THAN THREE DAMAGED =	1.00000	.99997	.99991	.99980	.99963	.99740	.99233	.98404
AVERAGE PER TARGET =	.00944	.01875	.02793	.03698	.04590	.08868	.12859	.16586

FIGURE C-16. RESULTS OF PROGRAM SECTION III FOR THE COOKIE CUTTER APPROXIMATIONS TO THE DAMAGE FUNCTIONS.

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DAMAGE FUNCTION NUMBER 8 FROM FILE DFCN348 FOR HOB = .30 HAS 1 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS RANGE DEFLECTION	OFFSET OF MIDPOINT FROM TARGET CENTER RANGE DEFLECTION
1.000	8.65 5.63	-1.02 0.00

DAMAGE FUNCTION NUMBER 9 FROM FILE DFCN348 FOR HOB = 5.00 HAS 10 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS RANGE DEFLECTION	OFFSET OF MIDPOINT FROM TARGET CENTER RANGE DEFLECTION
.936	2.74 1.96	-1.81 0.00
.848	3.73 2.61	-1.02 0.00
.732	3.73 5.18	-1.02 0.00
.656	4.41 8.81	-1.02 0.00
.552	4.80 10.63	-1.02 0.00
.450	5.31 12.40	-1.02 0.00
.346	5.72 14.75	-1.02 0.00
.251	6.63 15.67	-1.02 0.00
.142	6.68 20.58	-1.02 0.00
.041	8.11 26.03	-1.02 0.00

DAMAGE FUNCTION NUMBER 10 FROM FILE DFCN348 FOR HOB = 12.00 HAS 4 REGIONS, OF WHICH 0 ARE UNNESTED

PD	REGION DIMENSIONS RANGE DEFLECTION	OFFSET OF MIDPOINT FROM TARGET CENTER RANGE DEFLECTION
.335	2.67 3.56	-4.17 0.00
.249	6.43 6.26	-3.15 0.00
.141	7.11 21.80	-2.81 0.00
.046	12.18 35.30	-1.52 0.00

TARGET NUMBER 1 LOCATED AT (0.00, 75.00)

VOLLEY SIZE =	1	2	3	4	5	10	15	20
PD(HOB = .30) =	.007267	.014403	.021410	.028293	.035053	.067108	.096481	.123453
PD(HOB = 5.00) =	.009017	.017874	.026574	.035120	.043515	.063352	.119896	.153487
PD(HOB = 12.00) =	.005866	.011679	.017439	.023147	.028803	.056324	.082632	.107792

TARGET NUMBER 2 LOCATED AT (0.00, 25.00)

VOLLEY SIZE =	1	2	3	4	5	10	15	20
PD(HOB = .30) =	.007841	.015540	.023098	.030519	.037807	.072347	.103975	.133005

VOLLEY SIZE = 1 2 3 4 5 10 15 20

PO(HOB = .30) = .007841 .015540 .023098 .030519 .037807 .072347 .103975 .133005

PO(HOB = 5.00) = .009751 .019328 .028733 .037971 .047645 .090087 .129545 .165792

PO(HOB = 12.00) = .006360 .012662 .018905 .025092 .031221 .061036 .089521 .116745

THE HOB DISTRIBUTION FOLLOWS

HOB = .30 5.00 12.00

FRACTION OF POPULATION = .030 .800 .170

PROBABILITIES OF DAMAGE AVERAGED OVER THE HOB DISTRIBUTION FOR EACH TARGET FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20

TARGET NUMBER 1 = .008429 .016717 .024866 .032879 .040760 .078270 .112859 .144617

TARGET NUMBER 2 = .009118 .018081 .026893 .035558 .044078 .084616 .121974 .156470

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20

ALL SURVIVE = .96537 .93220 .90043 .86999 .84081 .71189 .60674 .52038

EXACTLY ONE DAMAGED = .03418 .06603 .09569 .12331 .14900 .25251 .32295 .36930

EXACTLY TWO DAMAGED = .00045 .00175 .00381 .00655 .00990 .03357 .06442 .09821

AT LEAST ONE DAMAGED = .03463 .06780 .09957 .13001 .15919 .28811 .39326 .47962

AT LEAST TWO DAMAGED = .00046 .00177 .00388 .00671 .01019 .03559 .07032 .11033

AT LEAST THREE DAMAGED = .00000 .00002 .00007 .00016 .00030 .00203 .00590 .01211

LESS THAN TWO DAMAGED = .99954 .99823 .99612 .99329 .98981 .96441 .92968 .88967

LESS THAN THREE DAMAGED = 1.00000 .99998 .99993 .99984 .99970 .99797 .99410 .98789

AVERAGE PER TARGET = .00877 .01740 .02588 .03422 .04242 .08144 .11742 .15064

PD'S FOR EACH TARGET WITH OPTIMUM FUZING (HOB = 5.00 METERS, ATTACK LEVEL = 5 ROUNDS PER CANNON)

VOLLEY SIZE = 1 2 3 4 5 10 15 20

TARGET NUMBER 1 = .009017 .017874 .026574 .035120 .043515 .083352 .119896 .153487

TARGET NUMBER 2 = .009751 .019328 .028733 .037971 .047045 .090087 .129545 .165792

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE = 1 2 3 4 5 10 15 20

ALL SURVIVE = .96299 .92765 .89389 .86164 .83081 .69567 .58690 .49867

VOLLEY SIZE = 1 2 3 4 5 10 15 20
 TARGET NUMBER 1 = .009017 .017874 .026574 .035120 .043515 .083352 .119896 .153487
 TARGET NUMBER 2 = .009751 .019328 .028733 .037971 .047045 .090087 .129545 .165792

THE SYSTEM (INCLUDING TARGET REFLECTIONS DUE TO SYMMETRY) DAMAGE PROBABILITIES FOLLOW

VOLLEY SIZE =	1	2	3	4	5	10	15	20
ALL SURVIVE =	.96259	.92765	.89389	.86164	.83031	.69567	.58690	.49867
EXACTLY ONE DAMAGED =	.03649	.07033	.10169	.13074	.15763	.26427	.33459	.37905
EXACTLY TWO DAMAGED =	.00052	.00200	.00434	.00744	.01121	.03762	.07149	.10797
AT LEAST ONE DAMAGED =	.03701	.07235	.10611	.13836	.16919	.30433	.41310	.50133
AT LEAST TWO DAMAGED =	.00052	.00202	.00442	.00762	.01157	.04006	.07951	.12228
AT LEAST THREE DAMAGED =	.00000	.00003	.00008	.00019	.00036	.00244	.00702	.01431
LESS THAN TWO DAMAGED =	.99948	.99798	.99558	.99238	.98843	.95994	.92149	.87772
LESS THAN THREE DAMAGED =	1.00000	.99997	.99992	.99981	.99964	.99756	.99298	.98569
AVERAGE PER TARGET =	.00938	.01860	.02765	.03655	.04528	.08672	.12472	.15964

FIGURE C-17. RESULTS OF PROGRAM SECTION III FOR THE APPROXIMATIONS OF GREATEST DETAIL TO THE DAMAGE FUNCTIONS.

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APPENDIX D

CONTROL DECK FOR THE EXAMPLE OF APPENDIX C

This appendix presents and explains the control deck used to execute the program in the example of Appendix C. Detailed explanations of the commands and their parameters may be found in CDC system literature.

Figure D-1 presents the control deck used to obtain the first set of results, the program section IV output. Card 3 attaches the permanent file on which the program is maintained in relocatable form. Cards 4 and 5 make accessible the permanent file on which the data deck of Figures C-3 and C-4 is maintained. These data could be read in on cards, but they are maintained as a file for convenience. Card 7 causes the program to be loaded and executed with file S4 replacing the system input file.

Figure D-2 presents the control deck used to obtain the second set of results, the output of program sections I and II.

Cards 4 and 5 make accessible the permanent file on which the data deck of Figures C-3 and C-6 is maintained. Again, cards could be used. Card 9 causes the program to be loaded and executed with files S12, PMAT348, and DFCN348 replacing the system input, perforation matrix, and damage function files, respectively. Card 10 causes the perforation matrix file to be catalogued (made permanent) as file PMAT348 with a password whose future absence will prevent all access to the file except for reading it. Card 11 performs the same function for the damage function file, under the name DFCN348. If an additional run of program sections I and/or II were desired, with additional perforation matrices and damage functions being written on these same files, appropriate ATTACH or GETPF commands would be required between cards 7 and 9.

Figure D-3 presents the control deck used to obtain the third set of results, the output of program section III.

[illegible]

```

JOBNAME,STMF.
ACCOUNT,XXXX.
ATTACH,LASREL,LASVENRELOCATABLE,LD=LAPOLITE.
FILE,S4,FL=100,RT=2,BT=C.
GETPE,S4,SECTION4DATA,LD=LAPOLITE,ST=MFA.
MAP,OFF.
LASREL,S4.
RETURN,S4,LASREL.
RT69 (MULTIPUNCHED IN COLUMN 1)
RT69 (MULTIPUNCHED IN COLUMN 1)

```

FIGURE D-1. CONTROL DECK FOR PROGRAM SECTION IV

11111111112222222222333333333344444444445555555555666666666677777777778
 1.34567890123456789012345678901234567890123456789012345678901234567890

COLUMN
 NUMBER
 CARD
 NUMBER

1
 2
 3
 4
 5
 6
 7
 8
 9
 10
 11
 12
 13
 14

JOBNAME,STMFZ.
 ACCOUNT,XXXX.
 ATTACH,LASREL,LASVENRELOCATABLE,ID=LAPDINTE.
 FILE,S12,FL=100,RT=Z,BT=C.
 GETPF,S12,SECTIONS1AND2DATA,ID=LAPDINTE,ST=MFA.
 REQUEST,PHAT348,*PF.
 REQUEST,DFCN346,*PF.
 MAP,OFF.
 LASREL,S12,PHAT348,DFCN346.
 CATALOG,PHAT346,PHAT346,ID=LAPDINTE,XR=XXXXXXXXXX.
 CATALOG,DFCN348,DFCN348,ID=LAPDINTE,XR=XXXXXXXXXX.
 RETURN,S12,PHAT346,DFCN346,LASREL.
 789 (MULTIPUNCHED IN COLUMN 1)
 6789 (MULTIPUNCHED IN COLUMN 1)

FIGURE D-2. CONTROL DECK FOR PROGRAM SECTIONS 1 AND 11

COLUMN NUMBER	CARD NUMBER
1	
2	
3	
4	
5	
6	
7	
8	
9	
10	
11	
12	

FIGURE D-3. CONTROL DECK FOR PROGRAM SECTION III

ADDENDUM

Paragraph 4.1.1, page 8, addresses the use of different linear combinations of the perforations sustained assuming:

- a. All fragments within a spray leave the source point with that spray's median velocity.
- b. All fragments within a spray leave the source point with that spray's maximum velocity.

Subsequent to the completion of this report, the program code was modified to allow the linear combination to be varied routinely, as input data. The coding which effects this is shown in Figure ADD-1. The sequence numbers (columns 82-87) indicate placement of the cards within the program shown in Appendix A.

The variable linear combination coefficients are F(1) and F(2). F(1) pertains to the perforations obtained with median velocities and F(2), to those obtained with maximum velocities. F(1) and F(2) are read in as real numbers with explicit decimal points on card number 1 of the BASIC DATA subdeck (see Figure 4-9), F(1) in columns 71 thru 75 and F(2) in columns 76 thru 80.

```

C      COMMON /LINCOM/ F(2),P(2)
      DECODE(70,1115,AAA(2))FFILES,CELLI,FNXX,FNYY,FICOL,FIRG,F(1),F(2)LASV197*
      1 SCALE2,F(1),F(2)
      1115 FORMAT(6E10,4,2F5,1)
      4 TO INPUT PLATE = 1./F5,3,10X,3*LINEAR COMBINATION COEFFICIENTS
      5 = F5,3,10X,F6,3/1)
      COMMON /LINCOM/ FF(2),P(2)
C
      30 PERF(11,JJ)=FF(1)*P(1)+FF(2)*P(2)
      110 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      120 PERF(11,JJ)=PERK
      270 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      280 PERF(11,JJ)=PERK
      420 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      430 PERF(11,JJ)=PERK
      460 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      490 PERF(11,JJ)=PERK
      510 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      520 PERF(11,JJ)=PERK
      660 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      670 PERF(11,JJ)=PERK
      PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      720 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      730 PERF(11,JJ)=PERK
      750 PERK=PERK+FF(1)*P(1)+FF(2)*P(2)
      760 PERF(11,JJ)=PERK
      COMMON /LINCOM/ F(2),P(2)
C
      P(1)=C.
      P(2)=C.
      I=1
      IF(3-OT-4C)I=2
      P(1)=P(1)*SGOIN(K2)*STERG(K1,K2)

```

FIGURE A00-1. PROGRAM MODIFICATION.

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